

Common borders. Common solutions.

# Landslide Hazard Assessment on Regional Scales: Pilot Implementation in Greece



SciNet NatHaz  
Prevention



Black Sea  
CROSS BORDER  
COOPERATION

## Acknowledgments:

The **SciNetNatHaz** Project  
is partially funded by the **EU** and National funds  
within the context of the

**Black Sea Basin Joint Operational Programme 2007-2013**

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**Nikolaos Klimis**, Democritus University of Thrace

*SciNetNatHaz project Open Seminars, September-October 2015*

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## Landslide Hazard Assessment in the Blaxi area. The...Gaps!

- **Usable Data are lacking.** Inventories of past landslides do not exist or are not accessible.
- **Metadata** are not supplied so it's very difficult to assess **reliability and accuracy** of available data (if found!).
- **Different LHA methodologies** are used even in the same country, making comparison of outputs, **impossible**.
- **Hazard identification & Risk assessment on regional and on local scales** (that could provide the essential information for planning typical preventive measures) has only been **sparsely implemented**.

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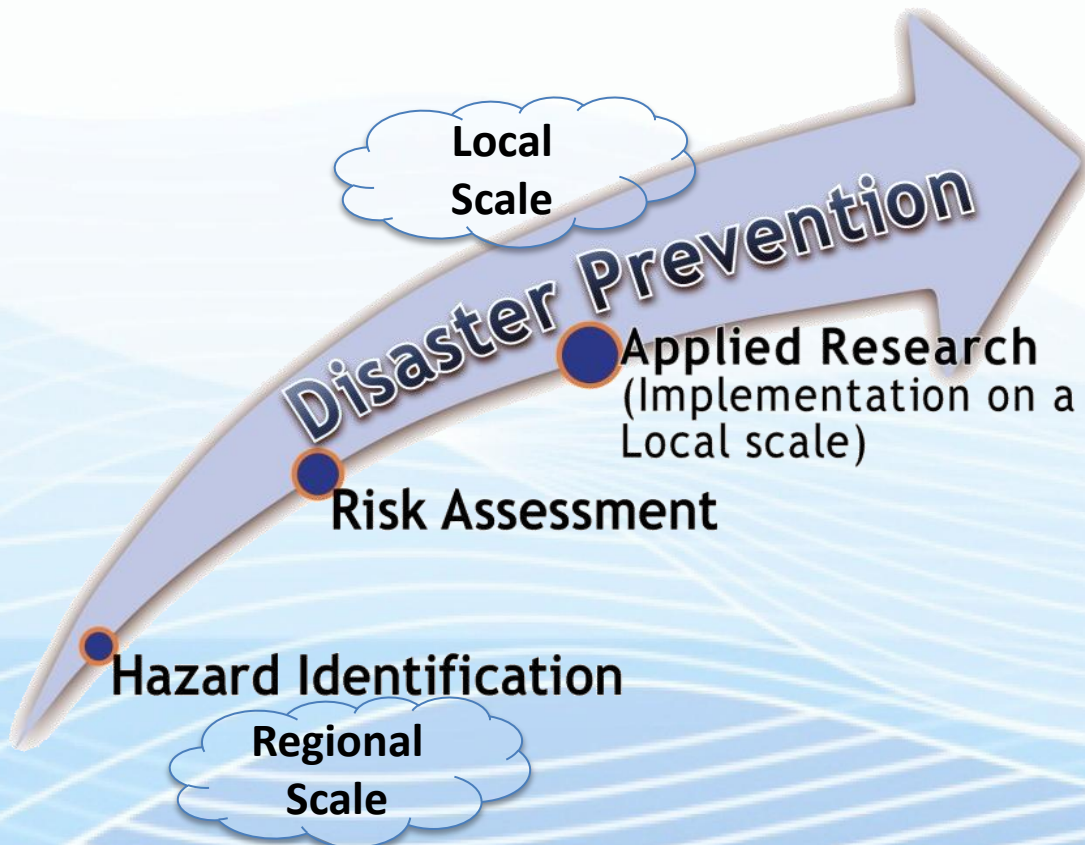
## SciNetNatHaz Landslide Hazard Assessment (LHA) related actions

The SciNetNatHaz project actions taken include:

- Select **worldwide accepted methodologies, applicable** in the wider area of the Black Sea basin, given the restrictions regarding data availability
- **Adapt** to “local” conditions and **implement LHA on regional scales** and in **pilot implementation areas**
- **Compare** selected methodologies in terms of **feasibility to implement** and **accuracy & reliability** of outputs
- Provide **free access to data** produced and processed with **Metadata** according to the INSPIRE directive provisions
- Indicatively **assess the Risk on regional scale** and **implement analysis on a local scale** which could provide the essential information for **planning typical preventive measures**.

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## Regional and Local scale LH Assessment to promote Prevention



- Landslide Hazard Assessment on **Regional Scale** to promote strategic planning & development
- Stability analysis on a **local scale** to assess typical preventive measures

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## Selected, Adapted to local conditions and Applied Methodologies

- A. Mora & Vahrson methodology** (Sergio Mora C., & Wilhelm-Gunther Vahrson (1994): Macrozonation Methodology for Landslide Hazard determination. Bulletin of the Association of Engineering Geologists, Vol. XXXI No.1, 1994, pp.49-58.
- B. Federal Emergency Management Agency (FEMA, USA) methodology – HazUS** (<https://www.fema.gov/hazus>)
- C. Factor of Safety calculation (Infinite Slope Model)**

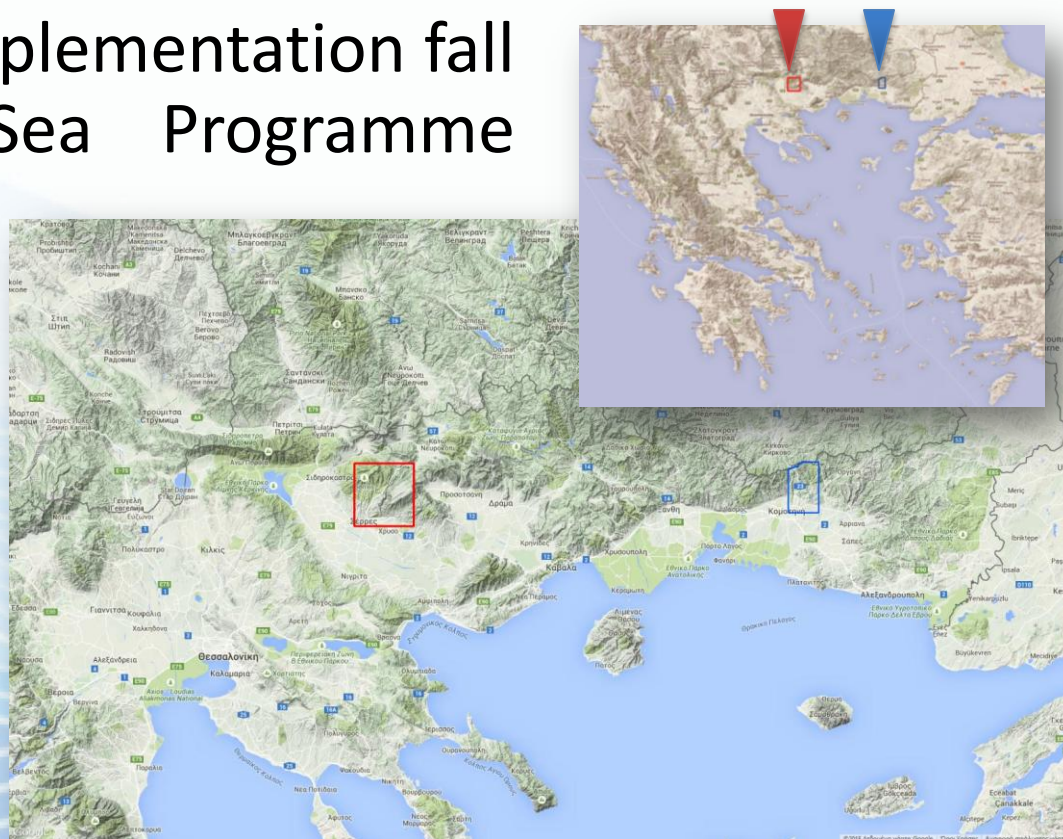
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## Implementation areas - Hellas

Both areas of pilot implementation fall inside the Black Sea Programme eligible area:

**A. Serres**

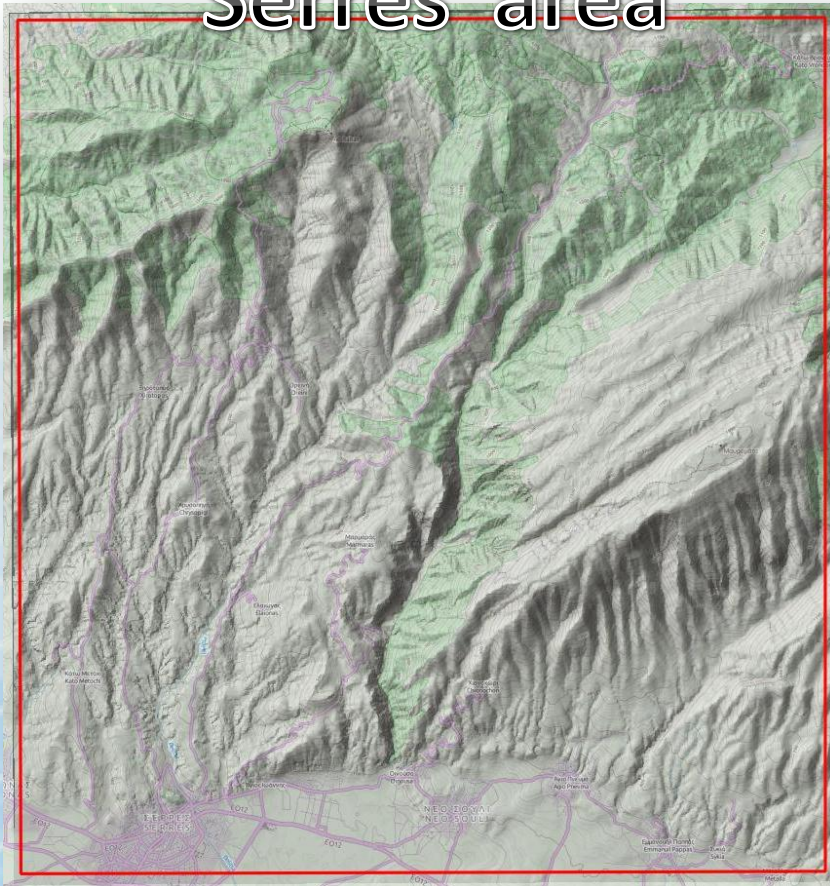
**B. Komotini-Nymfaia**



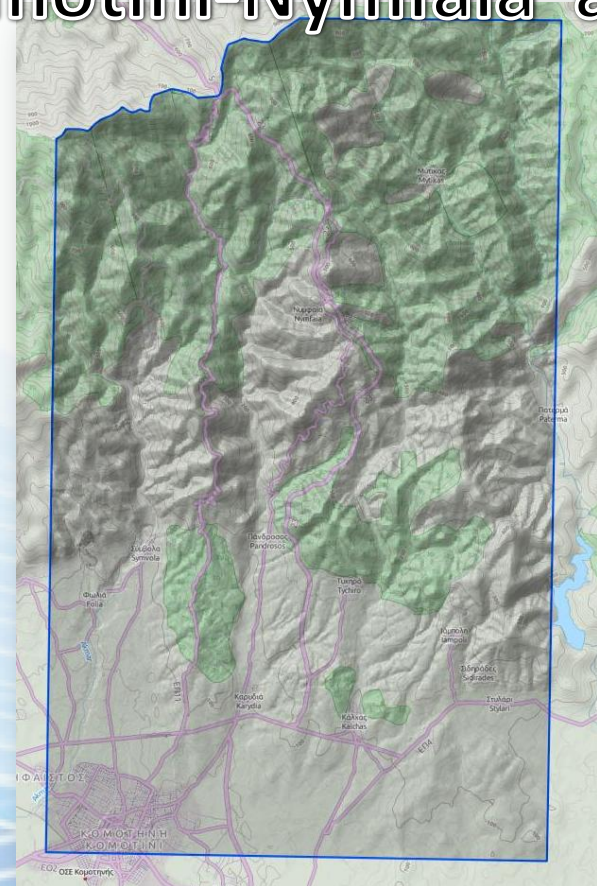
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# Implementation areas - Hellas

Serres area



Komotini-Nymfaia area



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## A. Mora & Vahrson Methodology

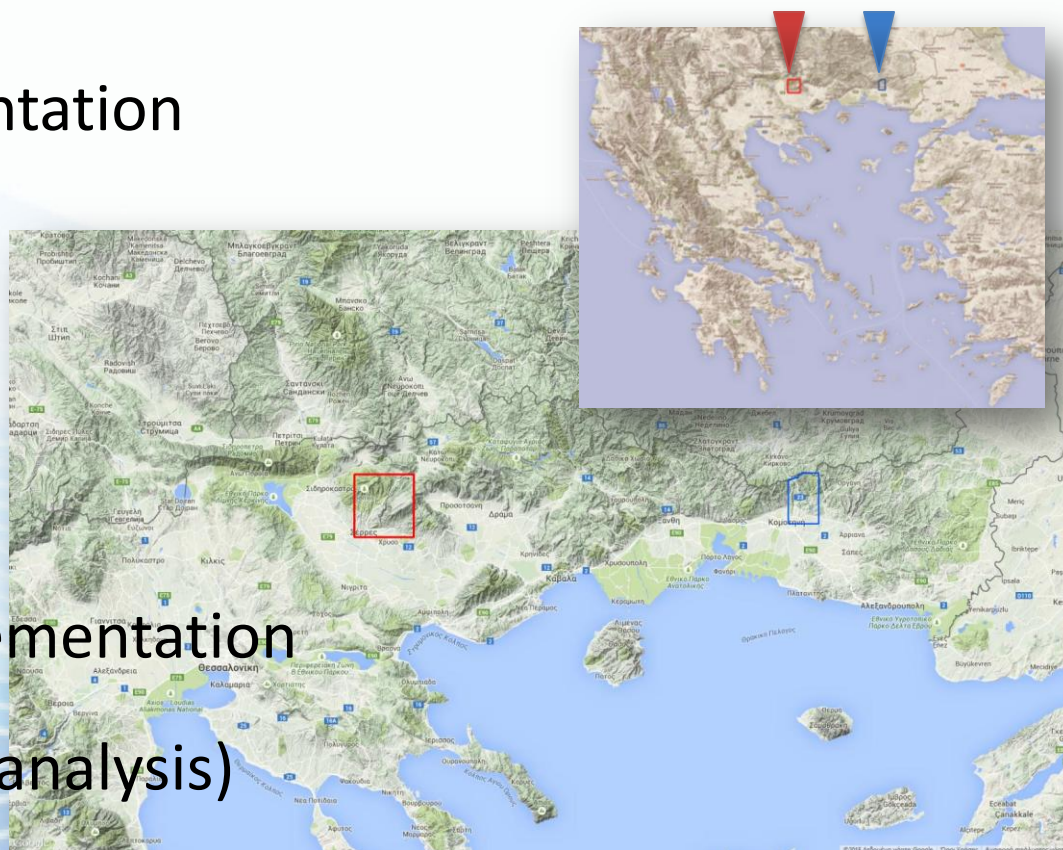
Areas of pilot implementation

**A.** Serres

**B.** Komotini-Nymfaia

Scale of Regional Implementation

1:50.000 (input data & analysis)



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## A. Mora & Vahrson Methodology

**Calculates the “Intrinsic Landslide Susceptibility” (SUSC)**

Taking into account the:

Slope Factor (**Sr**)

Lithology Factor (**SI**)

Soil Humidity Conditions (**Sh**)

$$\begin{aligned} HI &= SUSC * TRIG = \\ &= (Sr * SI * Sh) * (Ts + Tp) \end{aligned}$$

**And the Triggering Factor (TRIG)**

Deriver from the combination of

Seismic factor (**Ts**)

Precipitation factor (**Tp**)

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## A. Mora & Vahrson Methodology

The landslide **Hazard indicator (HI)**

$$\begin{aligned} \text{HI} &= \text{SUSC} * \text{TRIG} \\ &= (\text{Sr} * \text{Sl} * \text{Sh}) * (\text{Ts} + \text{Tp}) \end{aligned}$$

Where:

**Sr** : “Slope” factor

**Sl** : **Geology** factor

**Sh**: **Humidity** factor

**Ts**: (Earthquake) **Seismic** triggering factor

**Tp**: **Precipitation** triggering factor

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## A. M&V Methodology-Data requirements

- Scale of Implementation 1:50.000
- Topographic data (topographic Maps, elevation data, lattice points etc). In case topographic data at a 1:50000 scale are not available, ASTER DEMs can be used at the expense of accuracy.
- Geologic Maps
- Ground Motion data (PGA values)
- Mean Monthly Rainfall (mm) and MAX daily precipitations

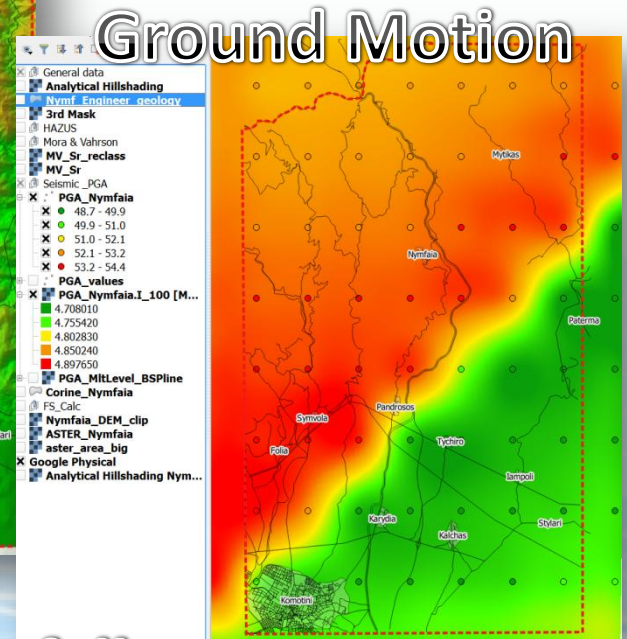
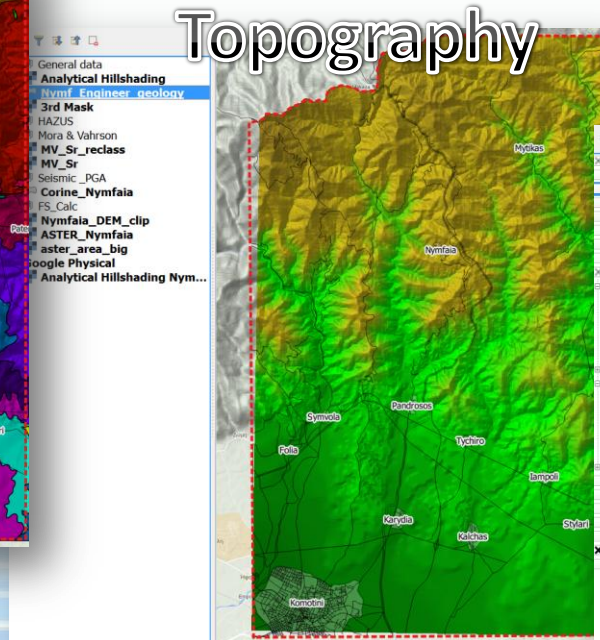
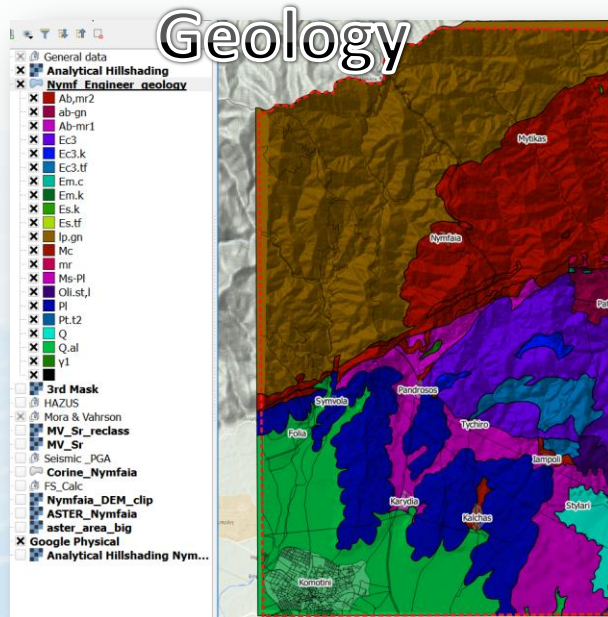


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# A. M&V Methodology-Data requirements



...and some basic data regarding rainfall

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## Susceptibility Indicator **SUSC**

$$HI = \mathbf{SUSC} * \text{TRIG} = (\mathbf{Sr} * \mathbf{SI} * \mathbf{Sh}) * (\text{Ts} + \text{Tp})$$

Includes the intrinsic properties of the landscape, the mechanical quality and its “passive” behavior. The parameters are the following:

- Slope Factor (**Sr**=Relative Relief),
- Lithology Factor (**SI**),
- Soil Humidity Conditions (**Sh**)

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## Susceptibility Indicator SUSC – Slope Factor

$$HI = SUSC * TRIG = (Sr * SI * Sh) * (Ts + Tp)$$

The Slope Factor is defined by the maximum difference in elevation per unit area **Rr = Relative Relief per grid unit (square km)** **Rr = (Hmax-Hmin)/km<sup>2</sup>**

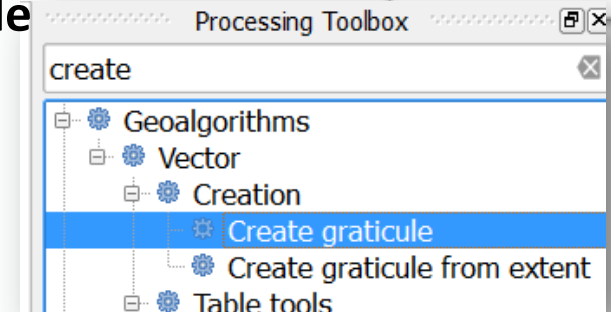
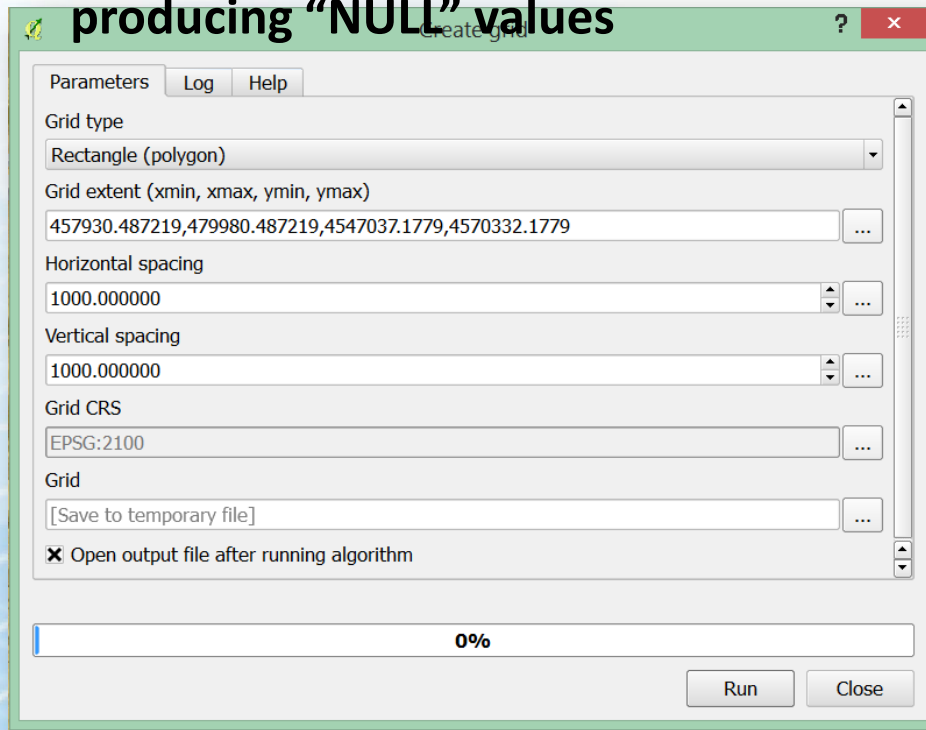
Relative Relief Rr (m/km <sup>2</sup> )	Classification	Slope Factor Sr
0-75	Very Low	0
76-175	Low	1
176-300	Moderate	2
301-500	Medium	3
501-800	High	4
>800	Very High	5

**Table 1.** Slope factor classification

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# Relative Slope Factor(Sr) Calculation step 1/3

- **QGIS** / Toolbox / Vector / Creation / Create graticule
- SET as GRID EXTENT the DEM file in order to avoid producing “NULL” values



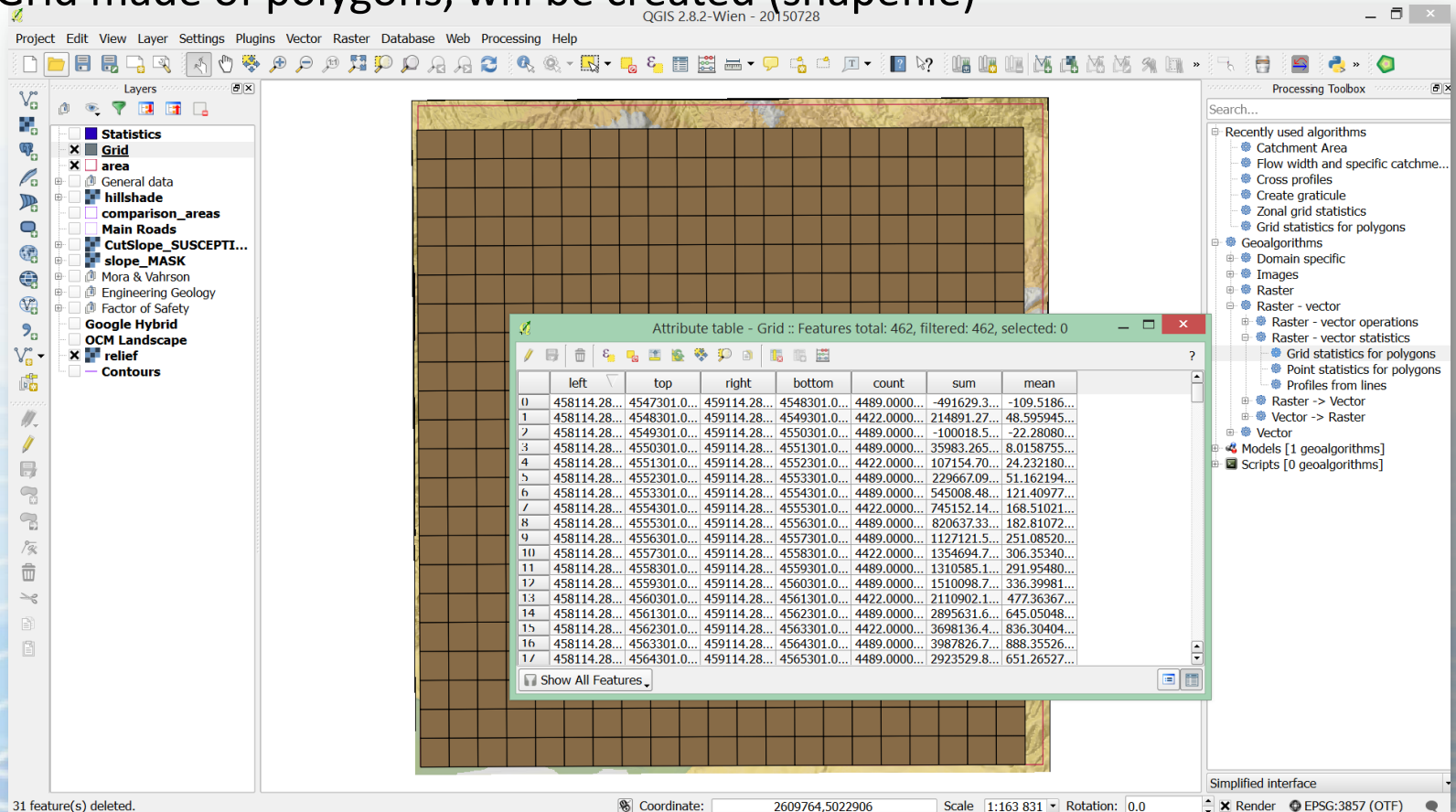
- Grid Type: **polygon**
- Grid Extend: **Select a layer** which covers the implementation area (the DEM will be fine)
- Horizontal and Vertical spacing: **1000m**
- Grid CRS: Insert the **Geodetic Reference System** of your choice
- Grid: grid **name**

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# Relative Slope Factor(Sr) Calculation step 1/3

- A Grid made of polygons, will be created (shapefile)

QGIS 2.8.2-Wien - 20150728



Project Edit View Layer Settings Plugins Vector Raster Database Web Processing Help

Layers

- Statistics
- ☒ Grid
- ☒ area
- General data
- hillshade
- comparison\_areas
- Main Roads
- CutSlope\_SUSCEPTI...
- slope\_MASK
- Mora & Vahrson
- Engineering Geology
- Factor of Safety
- Google Hybrid
- OCM Landscape
- ☒ relief
- Contours

Processing Toolbox

Search...

- Recently used algorithms
  - Catchment Area
  - Flow width and specific catchme...
  - Cross profiles
  - Create graticule
  - Zonal grid statistics
  - Grid statistics for polygons
- Geographical
  - Domain specific
  - Images
  - Raster
  - Raster - vector
  - Raster - vector operations
  - Raster - vector statistics
  - Grid statistics for polygons
  - Point statistics for polygons
  - Profiles from lines
  - Raster -> Vector
  - Vector -> Raster
  - Vector
- Models [1 geographical]
- Scripts [0 geographical]

Attribute table - Grid :: Features total: 462, filtered: 462, selected: 0

	left	top	right	bottom	count	sum	mean
0	458114.28...	4547301.0...	459114.28...	4548301.0...	4489.0000...	-491629.3...	-109.5186...
1	458114.28...	4548301.0...	459114.28...	4549301.0...	4422.0000...	214891.27...	48.595945...
2	458114.28...	4549301.0...	459114.28...	4550301.0...	4489.0000...	-100018.5...	-22.28080...
3	458114.28...	4550301.0...	459114.28...	4551301.0...	4489.0000...	35983.265...	8.0158755...
4	458114.28...	4551301.0...	459114.28...	4552301.0...	4422.0000...	107154.70...	24.232180...
5	458114.28...	4552301.0...	459114.28...	4553301.0...	4489.0000...	229667.09...	51.162194...
6	458114.28...	4553301.0...	459114.28...	4554301.0...	4489.0000...	545008.48...	121.40977...
7	458114.28...	4554301.0...	459114.28...	4555301.0...	4422.0000...	745152.14...	168.51021...
8	458114.28...	4555301.0...	459114.28...	4556301.0...	4489.0000...	820637.33...	182.81072...
9	458114.28...	4556301.0...	459114.28...	4557301.0...	4489.0000...	1127121.5...	251.08520...
10	458114.28...	4557301.0...	459114.28...	4558301.0...	4422.0000...	1354694.7...	306.35340...
11	458114.28...	4558301.0...	459114.28...	4559301.0...	4489.0000...	1310585.1...	291.95480...
12	458114.28...	4559301.0...	459114.28...	4560301.0...	4489.0000...	1510098.7...	336.39981...
13	458114.28...	4560301.0...	459114.28...	4561301.0...	4422.0000...	2110902.1...	477.36367...
14	458114.28...	4561301.0...	459114.28...	4562301.0...	4489.0000...	2895631.6...	645.05048...
15	458114.28...	4562301.0...	459114.28...	4563301.0...	4422.0000...	3698136.4...	836.30404...
16	458114.28...	4563301.0...	459114.28...	4564301.0...	4489.0000...	3987826.7...	888.35526...
17	458114.28...	4564301.0...	459114.28...	4565301.0...	4489.0000...	2923529.8...	651.26527...

Show All Features

31 feature(s) deleted.

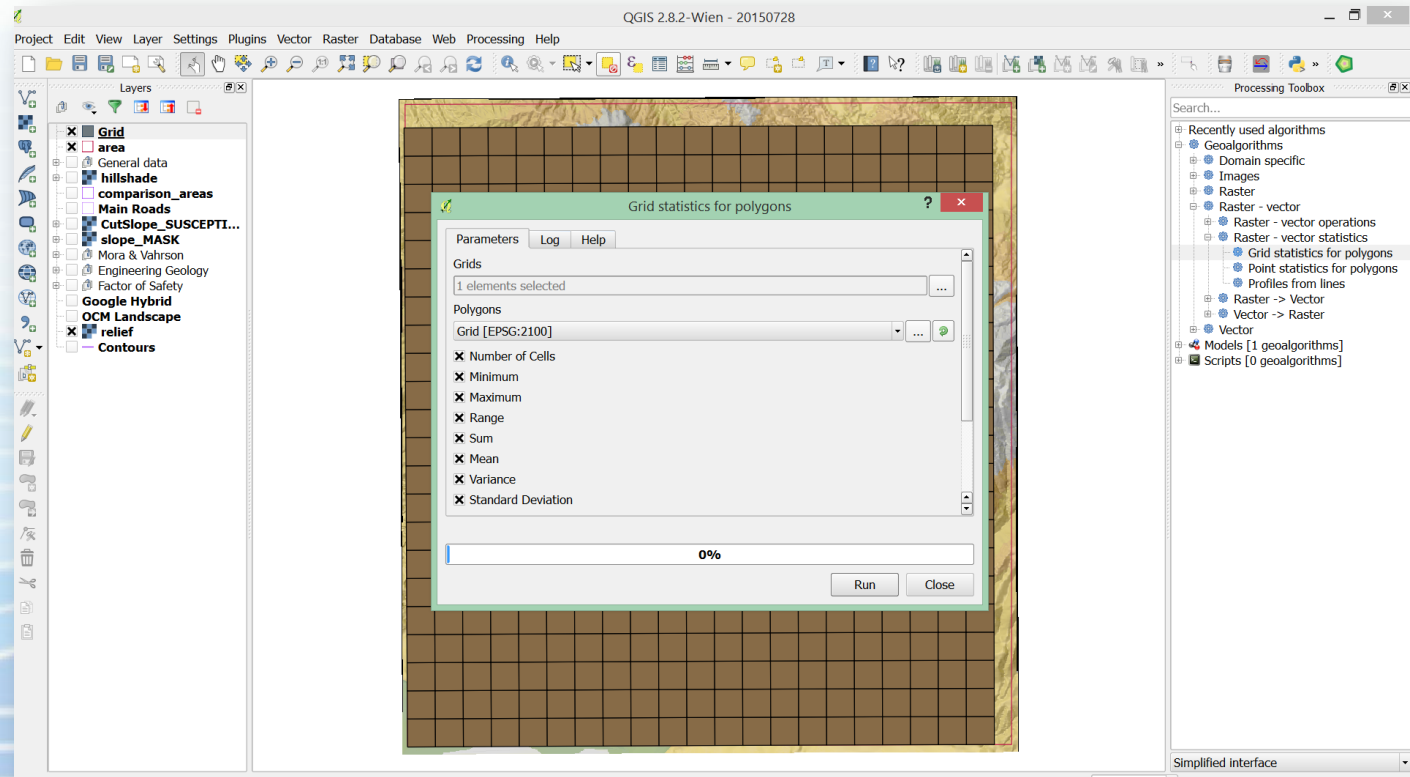
Coordinate: 2609764,5022906 Scale: 1:163 831 Rotation: 0.0

Render EPSG:3857 (OTF)

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# Relative Slope Factor(Sr) Calculation step 2/3

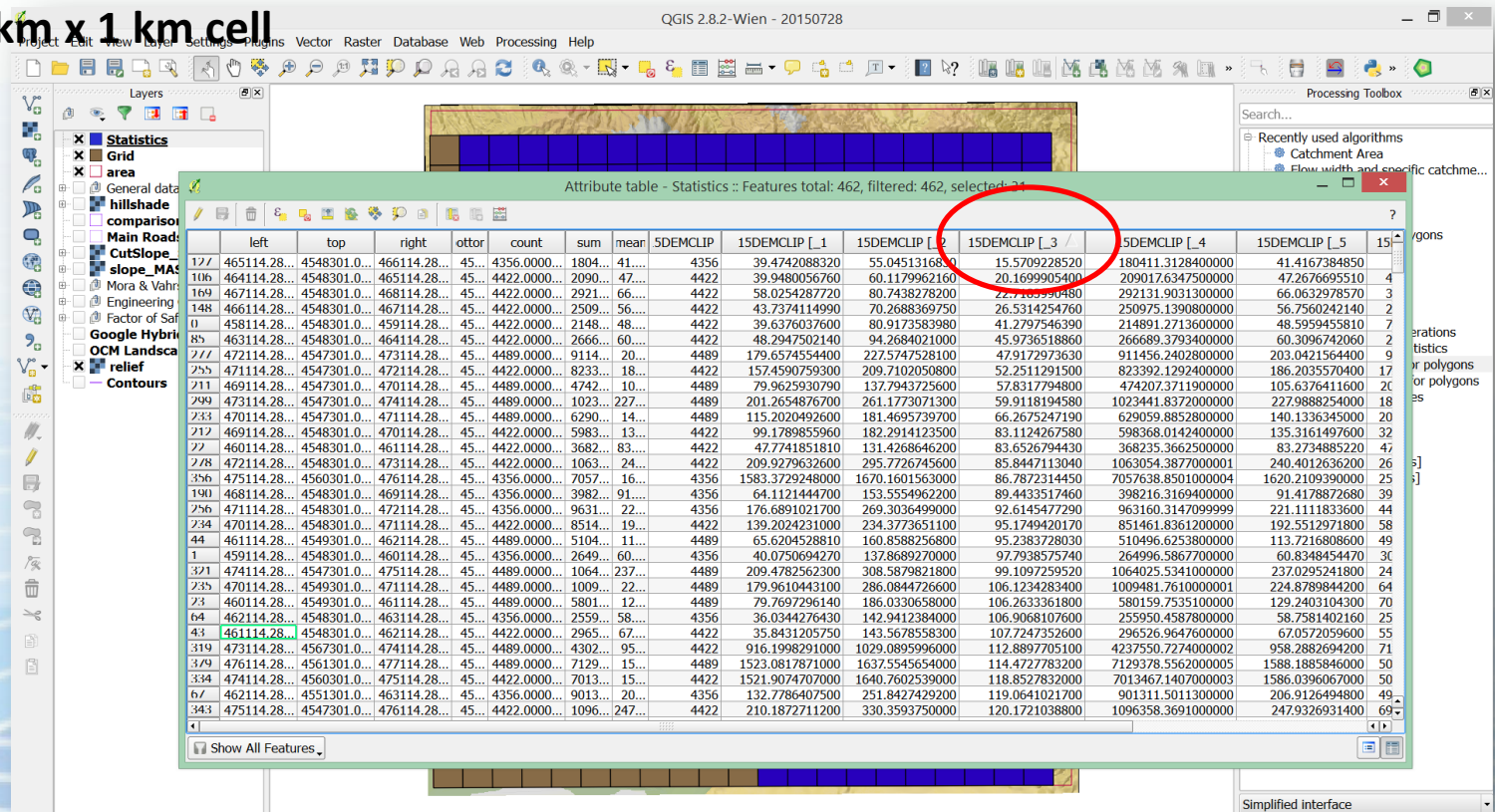
- Toolbox/ Raster-Vector / **Grid Statistics from polygons**
- Insert the requested statistical parameters (especially “RANGE”) and...*Run*



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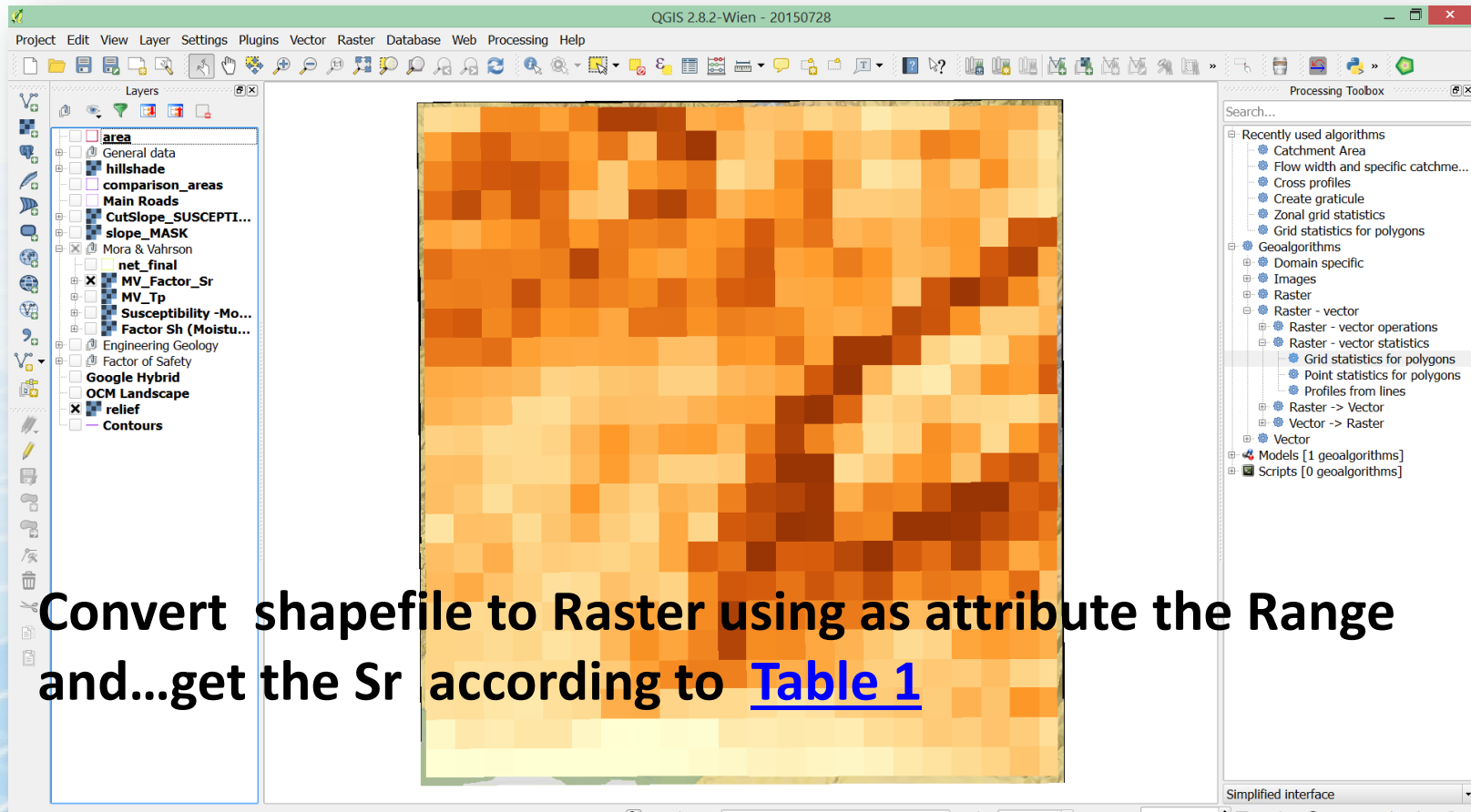
# Relative Slope Factor(Sr) Calculation step 2/3

- A NEW shapefile will be created having as additional attributes the requested parameters including the “Range” which corresponds to the **elevation difference in each 1km x 1 km cell**



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# Relative Slope Factor(Sr) Calculation step 3/3



The screenshot shows the QGIS 2.8.2-Wien interface. The main canvas displays a raster map with a color gradient from light yellow to dark brown, representing the Relative Slope Factor (Sr). The left sidebar shows the 'Layers' panel with a list of layers including 'area', 'hillshade', 'comparison\_areas', 'Main Roads', 'CutSlope\_SUSCEPTI...', 'slope\_MASK', 'Mora & Vahrson', 'net\_final', 'MV\_Factor\_Sr', 'MV\_Tp', 'Susceptibility -Mo...', 'Factor Sh (Moistu...', 'Engineering Geology', 'Factor of Safety', 'Google Hybrid', 'OCM Landscape', 'relief', and 'Contours'. The right sidebar shows the 'Processing Toolbox' with a search bar and a list of algorithms under 'Recently used algorithms' and 'Geographical algorithms'. The 'Processing Toolbox' list includes 'Catchment Area', 'Flow width and specific catchme...', 'Cross profiles', 'Create graticule', 'Zonal grid statistics', 'Grid statistics for polygons', 'Domain specific', 'Images', 'Raster', 'Raster - vector', 'Raster - vector operations', 'Raster - vector statistics', 'Grid statistics for polygons', 'Point statistics for polygons', 'Profiles from lines', 'Raster -> Vector', 'Vector -> Raster', 'Vector', 'Models [1 geographicals]', and 'Scripts [0 geographicals]'. The status bar at the bottom shows 'Simplified interface' and 'Coordinates: EPSG:3857 (UTM)'.

- Convert shapefile to Raster using as attribute the Range and...get the Sr according to [Table 1](#)

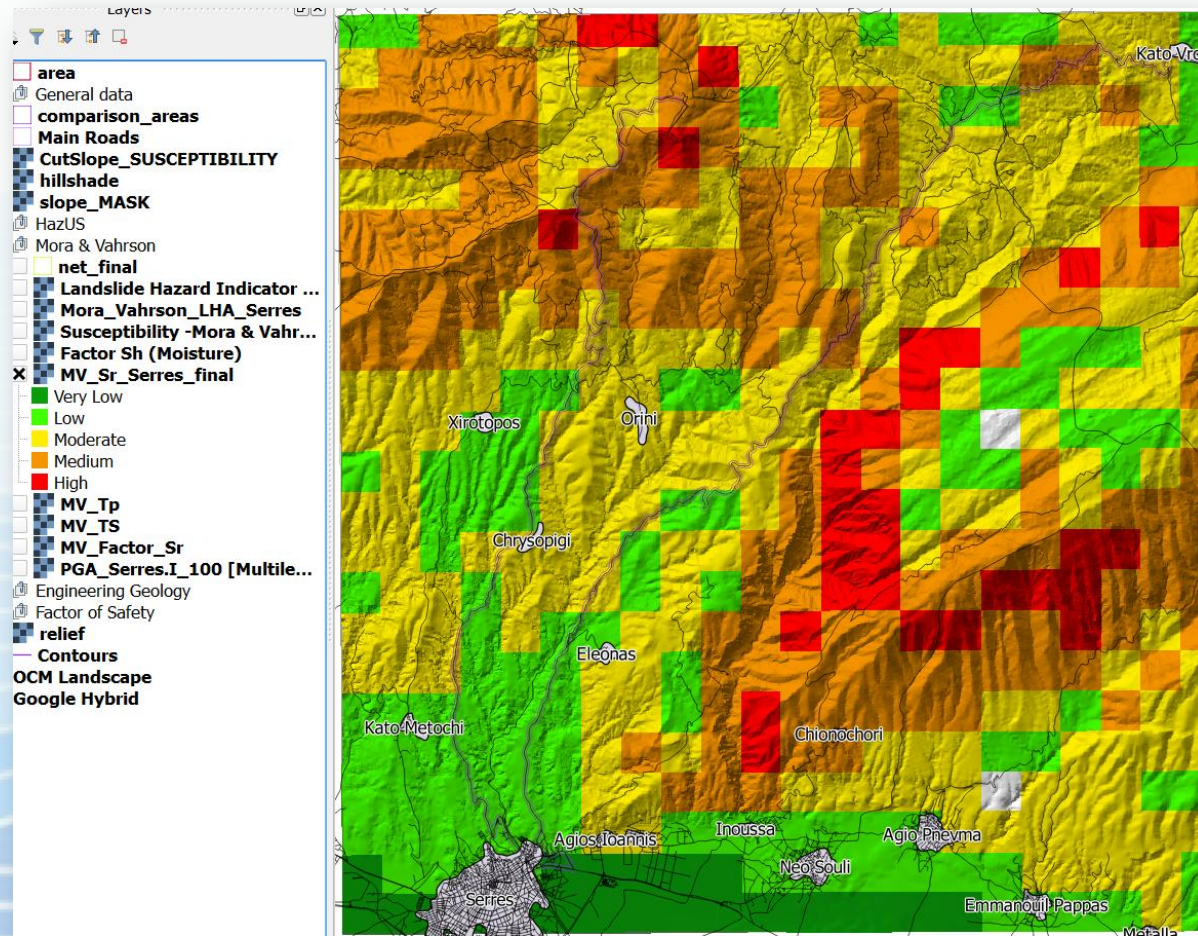


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# Relative Slope Factor(Sr) Calculation



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## Susceptibility Indicator **SUSC** – Lithology Factor 1/2

$$HI = \mathbf{SUSC} * TRIG = (Sr * \mathbf{SI} * Sh) * (Ts + Tp)$$

Includes the intrinsic properties of the landscape, the mechanical quality and its “passive” behavior. The parameters are the following:

The Lithology Factor (**SI**), is assessed from the **description of the geologic formations** and ideally, **geotechnical parameters** should be taken into account. There should be an, as close as possible to real conditions, estimation of the geotechnical behavior of the geologic formations.

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## Susceptibility Indicator **SUSC** – Lithology Factor 2/2

$$HI = \mathbf{SUSC} * TRIG = (Sr * \mathbf{SI} * Sh) * (Ts + Tp)$$

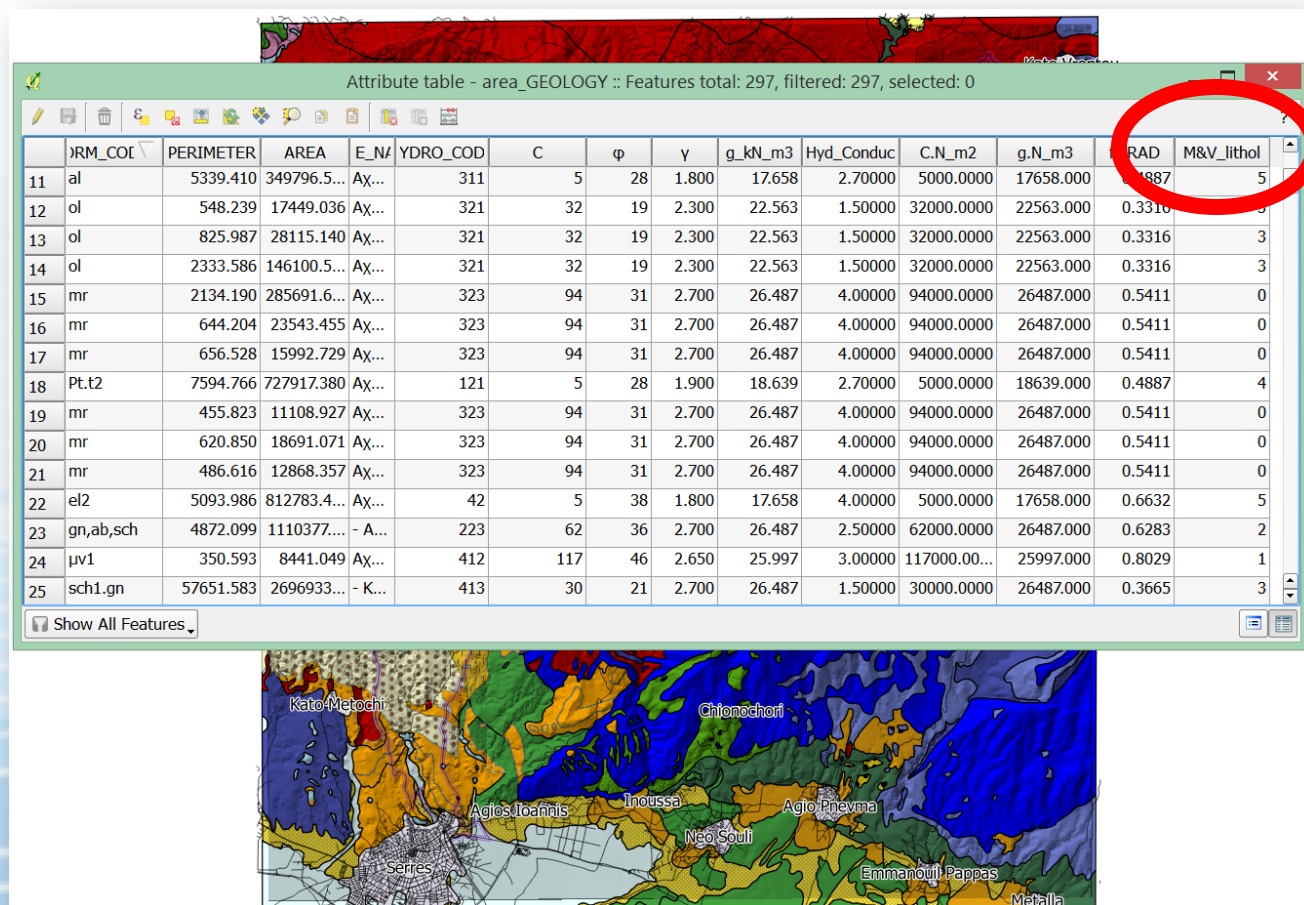
Parameters to be considered: volumetric weight, shear strength, weathering, discontinuities and their spatial distribution and orientation, their relation to slope geometry, drainage and pore pressure conditions, water table etc

**Lithology** can be used to **evaluate susceptibility** as very low (0), low (1), moderate (2), medium (3), high (4) and very high (5) (the highest the number the highest the susceptibility)

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## Susceptibility Indicator SUSC – Geology Factor 2/2

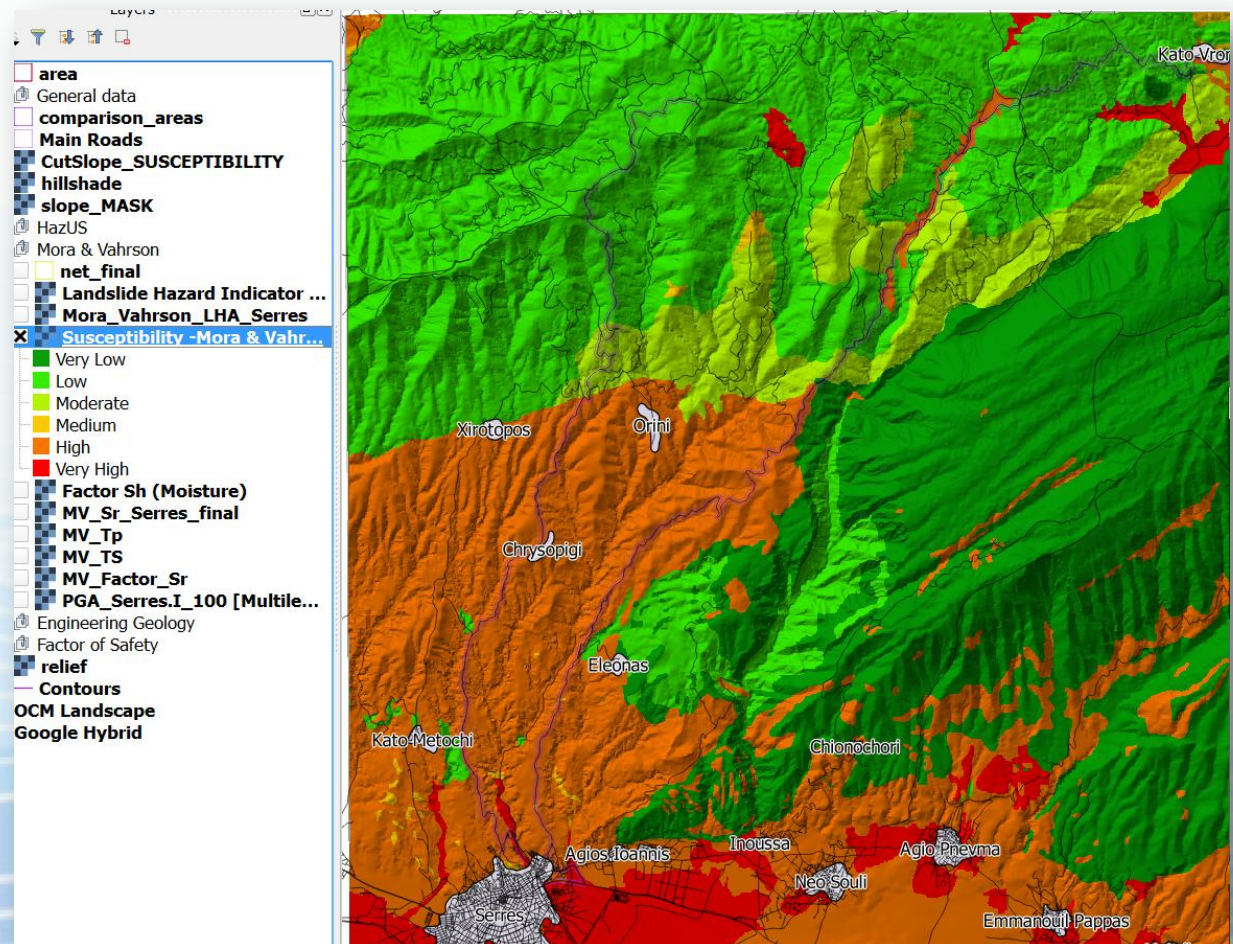
Lithology factor  
according to  
Parameters  
considered  
(volumetric  
weight, shear  
strength,  
weathering etc)



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## Susceptibility Indicator SUSC – Lithology Factor 2/2

Lithology factor  
according to  
Parameters  
considered  
(volumetric  
weight, shear  
strength,  
weathering etc)



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## Susceptibility Indicator SUSC – Soil Moisture

$$HI = \text{SUSC} * \text{TRIG} = (S_r * S_l * S_h) * (T_s + T_p)$$

Takes into account the average conditions of soil moisture. Quantifies the influence of **accumulated humidity throughout the year**.

Best measured in situ, but usually a simple methodology of soil-water balance can be used requiring only the average monthly precipitations.

Steps to follow:

1. Calculate the AVERAGE Monthly potential evapotranspiration (PET) for the implementation area
2. Each monthly average precipitation is assigned an index value according to **Table 3**
3. The TOTAL of all 12 month assigned values are calculated for each analyzed rain gage station. These values range from 0 to 24.
4. The total is classified into 5 groups according to **Table 4**

# Relative Soil Moisture

Average Monthly Precipitation AMP (mm/month)	Assigned Value
<125*	0
126-250	1
>250	2

\* 125 is the proposed value for South America. We must use a value around the average monthly potential evapotranspiration...which may have been correlated to elevation.

**Table 3.** Average monthly rainfall values classification

Accumulated value of Precipitation Indices	Qualification	Factor Sh
0-4	Very Low	1
5-9	Low	2
10-14	Medium	3
15-19	High	4
20-24	Very High	5

**Table 4.** Moisture factor (Sh) from accumulated AMP values

Both Serres and Nymfaia areas present average monthly precipitations below 125mm, so they fall into the "Very low" category

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## Triggering Indicator **TRIG**

$$HI = SUSC * \mathbf{TRIG} = (Sr * SI * Sh) * (Ts + Tp)$$

Represents the EXTERNAL driving forces which trigger the event.

Combines two factors:

- i) the 100 year earthquake and
- ii) The 100 year intense rainfall events

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## Triggering Indicator TRIG - Earthquakes

$$HI = SUSC * TRIG = (Sr * SI * Sh) * (Ts + Tp)$$

**Seismic intensity factor Ts** is determined by analyzing landslides triggered by earthquakes to assess the influence of seismic intensities on the group of lithologic, climatic and morphologic conditions.

Intensity (MM) Tr=100yr	Qualification	Factor Ts
III	Slight	1
IV	Very Low	2
V	Low	3
VI	Moderate	4
VII	Medium	5
VIII	Considerable	6
IX	Important	7
X	Strong	8
XI	Very Strong	9
XII	Extremely Strong	10

**Table 5.** Seismic Intensity factor **BASED ON OBSERVATIONS** in Costa Rica and Central America

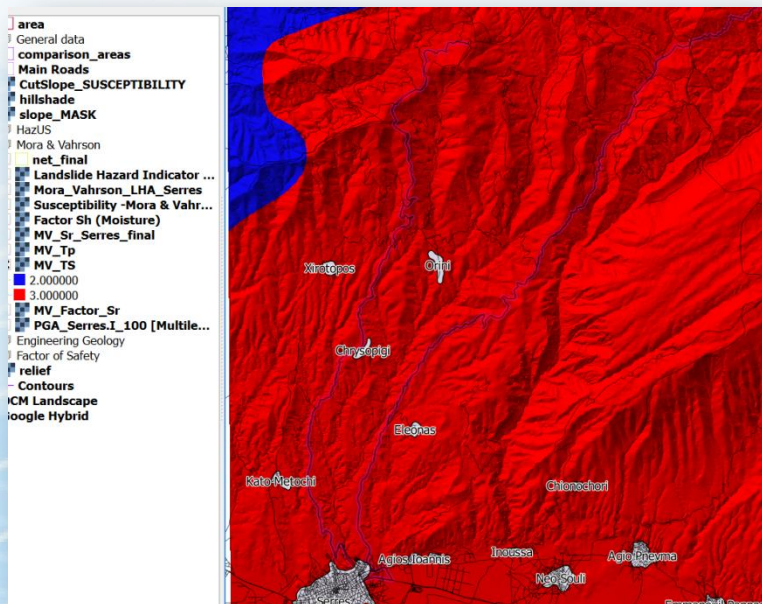
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## Triggering Indicator TRIG - Earthquakes

$$HI = SUSC * TRIG = (Sr * SI * Sh) * (Ts + Tp)$$

The Seismic Intensity for 100yrs return period needs to be calculated

*In PGA = 0.55 \* Imm + 1.30 (R<sup>2</sup>=0.88), PGA in cm/sec<sup>2</sup>  
(Koliopoulos et al., 1998, JEE)*



Attribute table - PGA\_Serres :: Features total: 42, filtered: 42, selected: 0

	-----Y	TR-----10	-----25	-----50	-----100	-----200	-----475	-----950	-----1000	I_100
000...	41.076099...	22.920000...	34.859999...	47.869999...	65.750000...	90.290000...	196.68999...	234.37999...	279.00000...	5.25
000...	41.076099...	22.149999...	34.359999...	47.890000...	66.739999...	93.030000...	216.12999...	291.57999...	294.00999...	5.27
000...	41.076099...	18.440000...	30.690000...	45.119999...	66.340000...	98.340000...	277.75000...	345.06000...	360.89999...	5.26
99...	41.076099...	15.630000...	27.840000...	43.079999...	66.670000...	105.53000...	291.33999...	346.99000...	360.93000...	5.27
000...	41.076099...	13.100000...	25.140000...	41.170000...	67.430000...	113.34999...	294.06999...	350.16000...	360.99000...	5.29
000...	41.076099...	11.039999...	22.859999...	39.659999...	68.790000...	120.48000...	296.56000...	351.87000...	361.01999...	5.33
000...	41.076099...	8.970000...	20.399999...	37.979999...	70.689999...	127.68000...	298.00999...	346.62999...	360.87999...	5.38
000...	41.116100...	16.579999...	27.989999...	41.600000...	61.829999...	91.890000...	182.74000...	205.09999...	217.25000...	5.14
000...	41.116100...	15.029999...	26.660000...	41.140000...	63.479999...	98.620000...	203.68999...	244.47999...	290.72000...	5.18
000...	41.116100...	12.850000...	24.399999...	39.630000...	64.379999...	107.03000...	220.58000...	292.19999...	309.75999...	5.21
99...	41.116100...	11.050000...	22.500000...	38.520000...	65.930000...	116.07999...	231.28000...	295.94999...	318.00000...	5.25
000...	41.116100...	9.070000...	20.140000...	36.829999...	67.370000...	127.64000...	243.52000...	302.80000...	332.01999...	5.29
000...	41.116100...	6.860000...	17.320000...	34.890000...	70.280000...	141.90000...	256.91000...	310.43000...	345.18000...	5.37
000...	41.116100...	5.470000...	15.380000...	33.609999...	73.480000...	155.31000...	268.85000...	316.86000...	354.77999...	5.45

Show All Features

# Precipitation Intensity factor $T_p$

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## Triggering Indicator TRIG - Precipitation

$$HI = SUSC * TRIG = (S_r * S_l * S_h) * (T_s + T_p)$$

Maximum Rainfall $n > 10$ yrs, $T_r = 100$ yrs	Rainfall $n < 10$ yrs; Average	Qualification	$T_p$ Factor
$< 100$ mm	$< 50$ mm	Very Low	1
101-200 mm	51-90 mm	Low	2
201-300 mm	91-130 mm	Medium	3
301-400 mm	131-175 mm	High	4
$> 400$ mm	$> 175$ mm	Very High	5

**Table 6. Precipitation factor ( $T_p$ )** originating from the classification of maximum daily precipitations over a return period of 100 yrs. An auxiliary classification based on the average yearly maximum values per day is given in column 2.

*Both Serres and Nymfaia areas present average maximum DAILY precipitations in the range of 51-90 mm, so they fall into the “Low” category ( $T_p=2$ )*

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## Classification of Landslide Hazard Indicator (HI)

$$\text{HI} = \text{SUSC} * \text{TRIG} = (\text{Sr} * \text{SI} * \text{Sh}) * (\text{Ts} + \text{Tp})$$

HI values range  
from 0 to 1250 or  
more

These values are  
indicative of the  
landslide hazard  
according to Table  
7

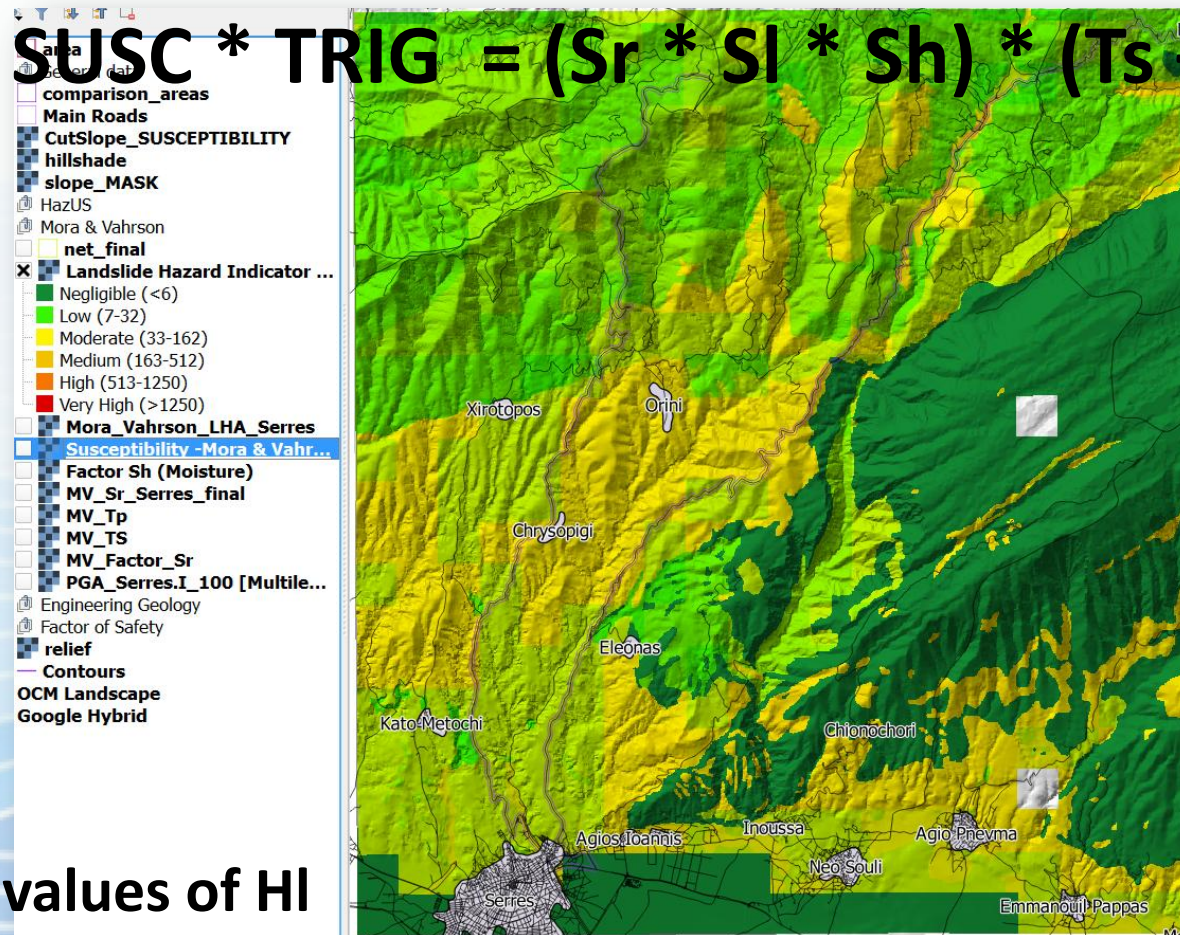
Value of HI	Class	Classification of Hazard of Landslide Potential
<6	I	Negligible
7-32	II	Low
33-162	III	Moderate
163-512	IV	Medium
513-1250	V	High
>1250	VI	Very High

**Table 7.** Classification of the Landslide Hazard HI parametric values.

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# Classification of Landslide Hazard Indicator (HI)

$$HI = SUSC * TRIG = (Sr * SI * Sh) * (Ts + Tp)$$



Classified values of HI

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# END of the 1<sup>st</sup> cycle

Areas of pilot implementation

**A.** Serres

**B.** Komotini

# Thank you!



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## B. FEMA methodology (Hazard US)

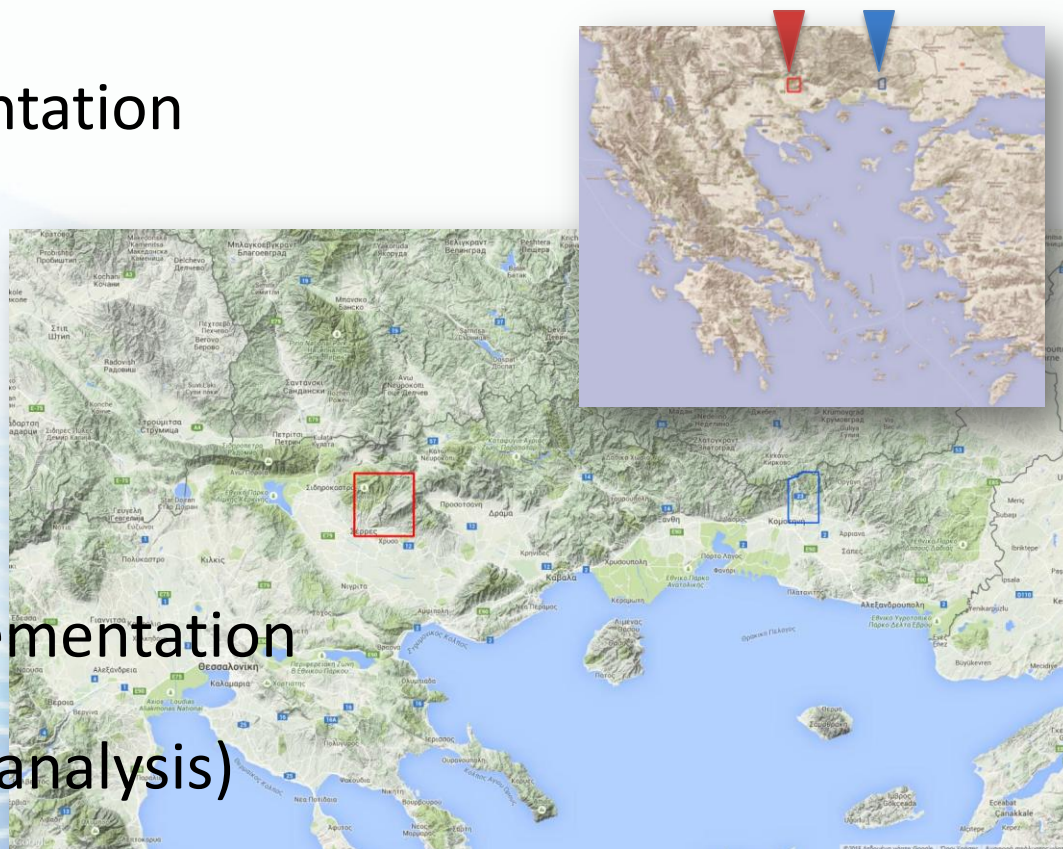
Areas of pilot implementation

**A.** Serres

**B.** Komotini-Nymfaia

Scale of Regional Implementation

1:50.000 (input data & analysis)



Common borders. Common solutions.

# Landslide Hazard Assessment (FEMA)

1. Assess Landslide **Susceptibility** (under static conditions)
2. Assess the **Critical Acceleration** ( $A_c$ )
3. Compare ( $A_c/PGA$ ) the Critical Acceleration ( $A_c$ ) with the actual Peak Ground Acceleration (PGA)

All the above parameters are calculated for two different moisture/ groundwater conditions: “DRY” and “WET” whereas “**DRY**” corresponds to groundwater level **BELOW** surface of failure and “**WET**” corresponds to groundwater **ON** ground surface.

Common borders. Common solutions.

# 1. Landslide Susceptibility under static conditions

**Step 1: Geology** (need to classify the formations in one of the 3 categories in Table 1)

**Step 2: Slope angle** (need to classify the formations in one of the six categories in Table 1)

**Step 3: Underground Water Table** (need to distinguish between “DRY” (when ground water below of level of sliding) and “WET” (when ground water at ground surface)).

Common borders. Common solutions.

# Landslide Susceptibility under static conditions

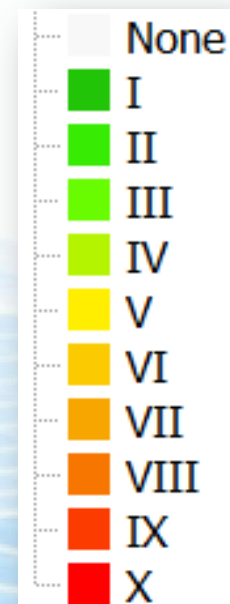
**Table 8. Landslide susceptibility under static conditions**

(HazUS MH, Chapter 4 – PESH)

Geologic Group		Slope Angle, degrees					
		0-10	10-15	15-20	20-30	30-40	>40
<b>(a) DRY (groundwater below level of sliding)</b>							
A	Strongly Cemented Rocks (crystalline rocks and well-cemented sandstone, $c' = 300$ psf, $\phi' = 35^\circ$ )	None	None	I	II	IV	VI
B	Weakly Cemented Rocks and Soils (sandy soils and poorly cemented sandstone, $c' = 0$ , $\phi' = 35^\circ$ )	None	III	IV	V	VI	VII
C	Argillaceous Rocks (shales, clayey soil, existing landslides, poorly compacted fills, $c' = 0$ , $\phi' = 20^\circ$ )	V	VI	VII	IX	IX	IX
<b>(b) WET (groundwater level at ground surface)</b>							
A	Strongly Cemented Rocks (crystalline rocks and well-cemented sandstone, $c' = 300$ psf, $\phi' = 35^\circ$ )	None	III	VI	VII	VIII	VIII
B	Weakly Cemented Rocks and Soils (sandy soils and poorly cemented sandstone, $c' = 0$ , $\phi' = 35^\circ$ )	V	VIII	IX	IX	IX	X
C	Argillaceous Rocks (shales, clayey soil, existing landslides, poorly compacted fills, $c' = 0$ , $\phi' = 20^\circ$ )	VII	IX	X	X	X	X

scale I: less susceptible

scale X: most susceptible



# How to...1/4

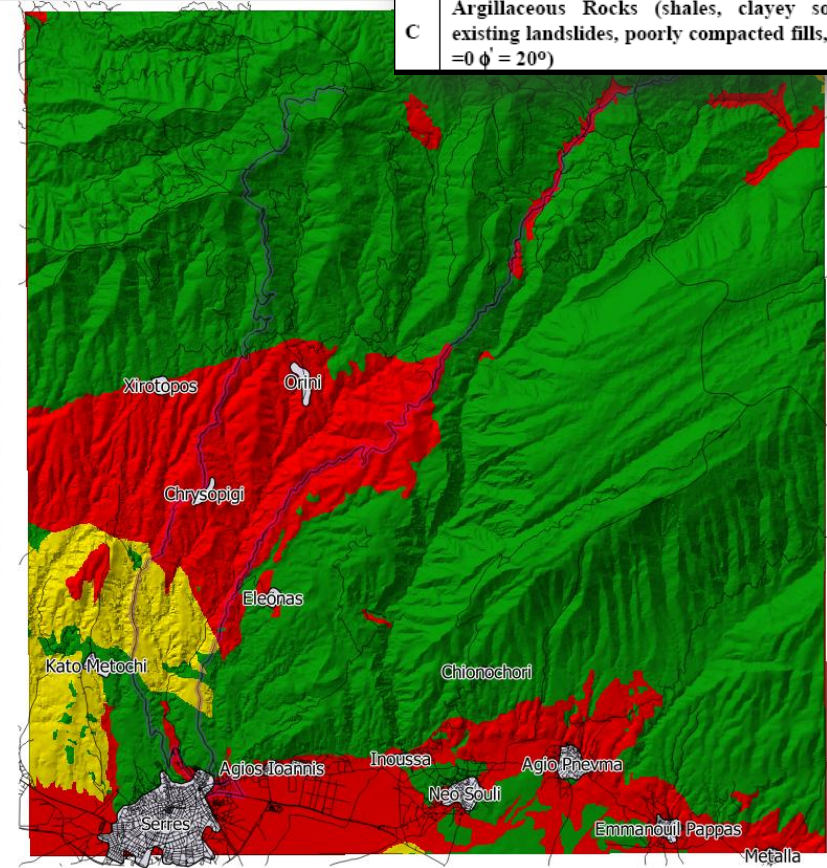
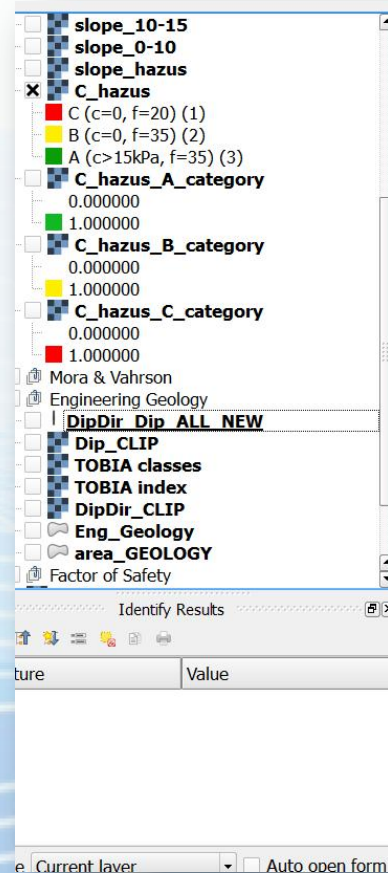
Common borders. Common solutions.

1. Create a NEW column in "geology.shp" and classify the geologic formations according to **Table 8** in **A , B & C Categories**

2. Create a NEW raster with all three categories (as the C\_Hazus shown)

3. Create for **EACH** category, a **SEPARATE file to be used as MASK** (C\_Hazus\_A\_category etc)

4. The classes made will cover the entire area as shown on the map



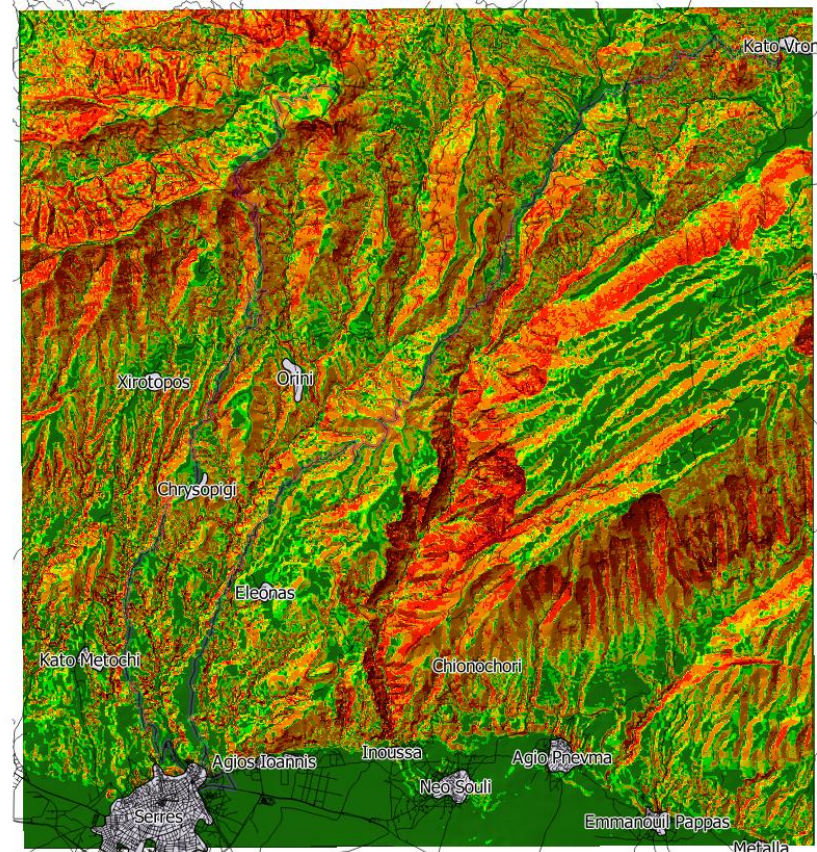
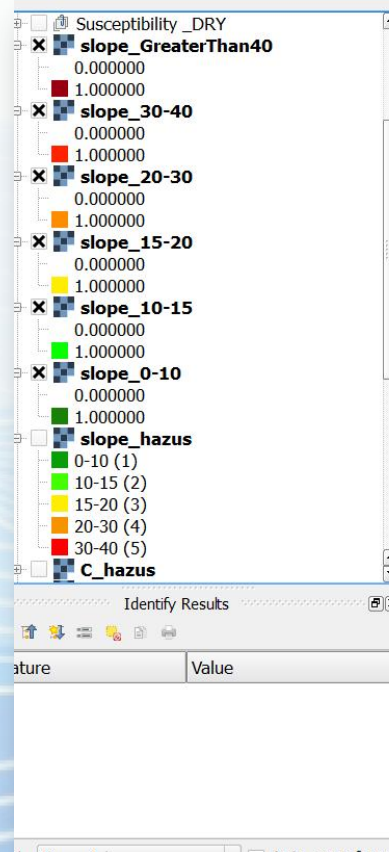
Geologic Group	
(a) DRY (groundwater)	
A	Strongly Cemented Rocks (crystalline rocks and well-cemented sandstone, $c' = 300 \text{ psf}, \phi' = 35^\circ$ )
B	Weakly Cemented Rocks and Soils (sandy soils and poorly cemented sandstone, $c' = 0, \phi' = 35^\circ$ )
C	Argillaceous Rocks (shales, clayey soil, existing landslides, poorly compacted fills, $c' = 0, \phi' = 20^\circ$ )

## How to...2/4

Common borders. Common solutions.

1. Reclassify “**slope**” into the slope categories shown in **Table 8**
2. Create a NEW raster with all six categories (as the slope\_hazus shown)
3. Create for **EACH** category, a **SEPARATE file** to be used as **MASK** (slope\_0-10 etc)
4. The classes made will cover the entire area as shown on the map

Slope Angle, degrees					
0-10	10-15	15-20	20-30	30-40	>40



# How to...3/4

Common borders. Common solutions.

Table 8

Geologic Group		Slope Angle, degrees					
		0-10	10-15	15-20	20-30	30-40	>40
(a) DRY (groundwater below level of sliding)							
A	Strongly Cemented Rocks (crystalline rocks and well-cemented sandstone, $c' = 300$ psf, $\phi' = 35^\circ$ )	None	None	I	II	IV	VI
B	Weakly Cemented Rocks and Soils (sandy soils and poorly cemented sandstone, $c' = 0$ , $\phi' = 35^\circ$ )	None	III	IV	V	VI	VII
C	Argillaceous Rocks (shales, clayey soil, existing landslides, poorly compacted fills, $c' = 0$ , $\phi' = 20^\circ$ )	V	VI	VII	IX	IX	IX
(b) WET (groundwater level at ground surface)							
A	Strongly Cemented Rocks (crystalline rocks and well-cemented sandstone, $c' = 300$ psf, $\phi' = 35^\circ$ )	None	III	VI	VII	VIII	VIII
B	Weakly Cemented Rocks and Soils (sandy soils and poorly cemented sandstone, $c' = 0$ , $\phi' = 35^\circ$ )	V	VIII	IX	IX	IX	X
C	Argillaceous Rocks (shales, clayey soil, existing landslides, poorly compacted fills, $c' = 0$ , $\phi' = 20^\circ$ )	VII	IX	X	X	X	X

1. Calculate the respective **susceptibility category for each Geologic Group Class** and then **for each moisture condition** (DRY or WET)

2. i.e. For calculating the Geologic Group "A" susceptibility under **WET conditions**, the formula used was:

$"C\_hazus\_A\_category@1" * (0 * "slope\_0-10@1" + 3 * "slope\_10-15@1" + 6 * "slope\_15-20@1" + 7 * "slope\_20-30@1" + 8 * "slope\_30-40@1" + 8 * "slope\_GreaterThan40@1")$  \* See the layer names in the next image

Where:

- "C\_Hazus\_A\_category" is the mask to erase values outside this specific category area (is "1" where valid and "0" outside the specific category area)
- Slope\_\*@1 are the "slope" classes and
- the multiplication factors correspond to the susceptibility values shown in the table



# How to...4/4

Common borders. Common solutions.

## Susceptibility under different moisture conditions

Geologic Group		Slope Angle, degrees					
		0-10	10-15	15-20	20-30	30-40	>40
(a) DRY (groundwater below level of sliding)							
A	Strongly Cemented Rocks (crystalline rocks and well-cemented sandstone, $c' = 300$ psf, $\phi' = 35^\circ$ )	None	None	I	II	IV	VI

**Raster calculator**

**Raster bands**

- WI values@1
- Z\_10m@1
- Z\_1m@1
- slope\_30-40@1
- slope\_GreaterThan\_40@1

**Result layer**

Output layer: AIA/A\_DRY\_susceptibility

Output format: GeoTIFF

Current layer extent

X min: 615986.55061 XMax: 627073.71572

Y min: 4552183.40088 Y max: 4570650.49570

Columns: 409 Rows: 682

Output CRS: Project CRS (EPSG:2100 - GGRS8')

☒ Add result to project

**Operators**

+, \*, sqrt, cos, sin, tan, log10, (, -, /, ^, acos, asin, atan, ln, ), <, >, =, !=, <=, >=, AND, OR

**Raster calculator expression**

```
"GeolGroup_class_A@1" * ( "slope_0-10@1" * 0 + "slope_10-15@1" * 0 + "slope_15-20@1" * 1 + "slope_20-30@1" * 2 + "slope_30-40@1" * 4 + "slope_GreaterThan_40@1" * 6 )
```

Expression valid

OK Cancel



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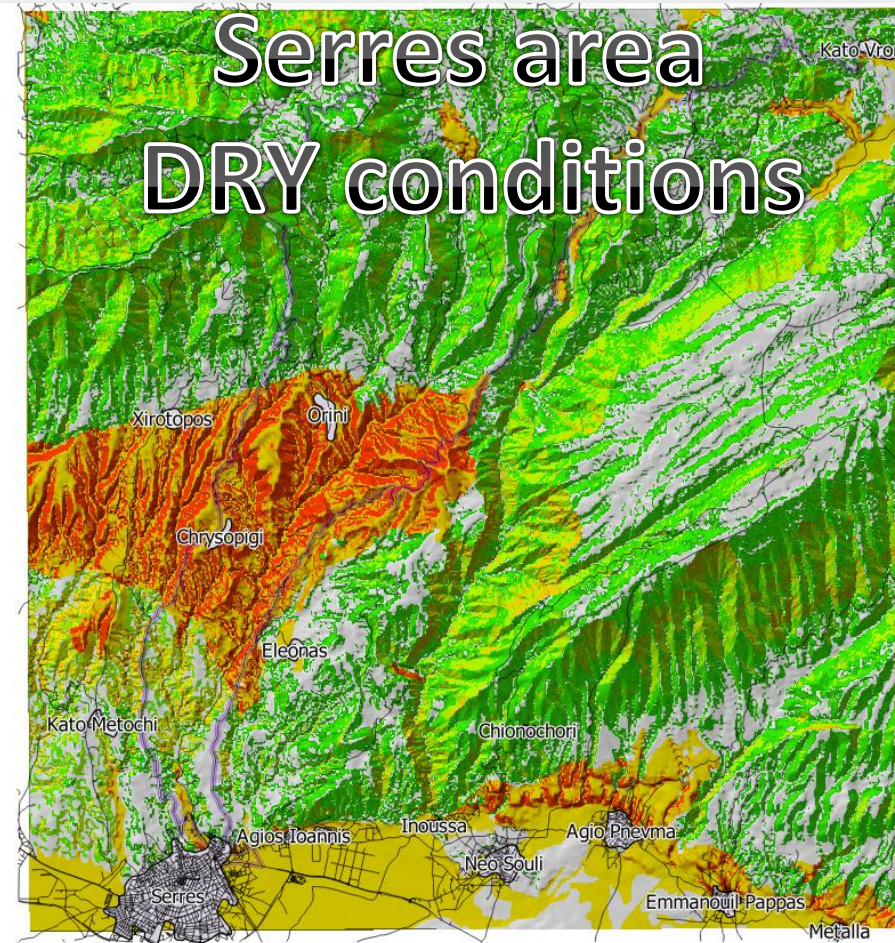
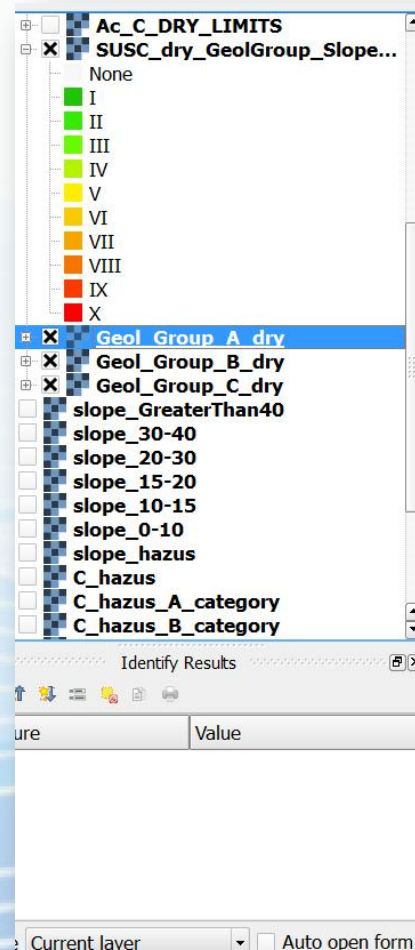


Common borders. Common solutions.

# Landslide Susceptibility under static conditions

## Susceptibility under different moisture conditions

is calculated by adding the individual Susceptibilities Per Geologic Group





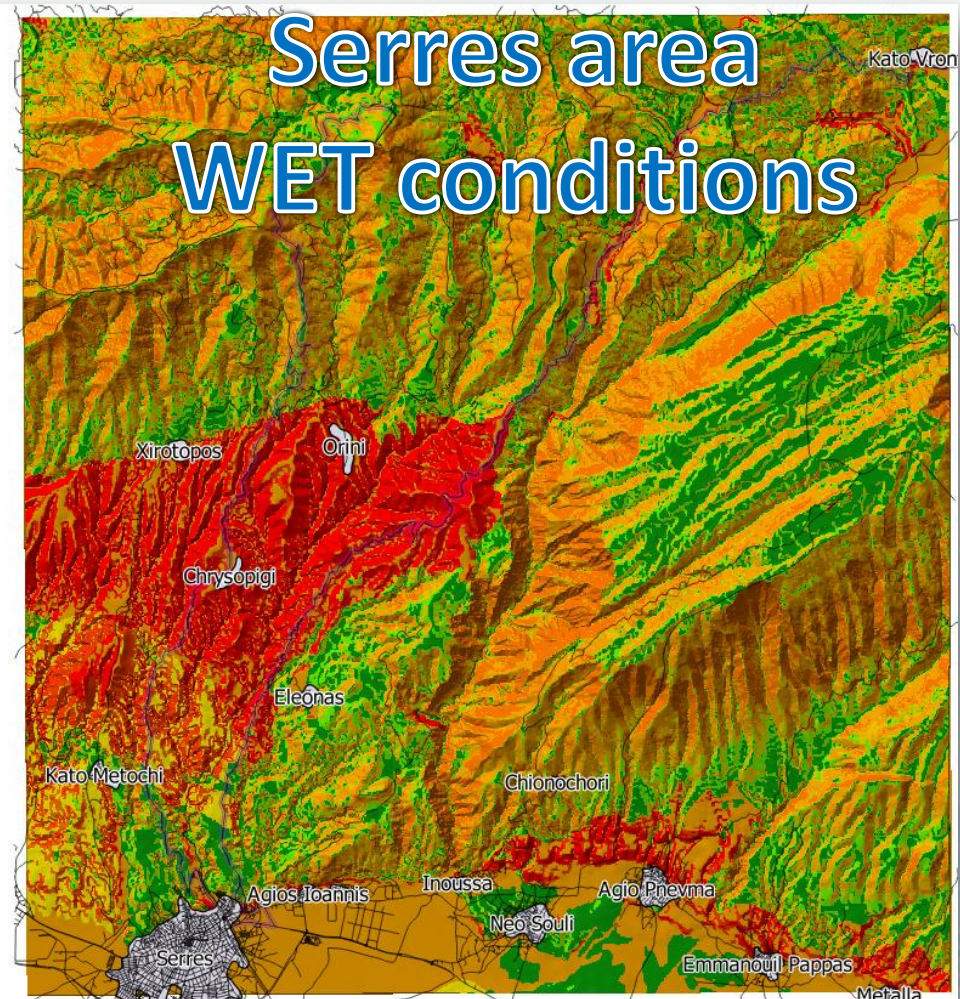
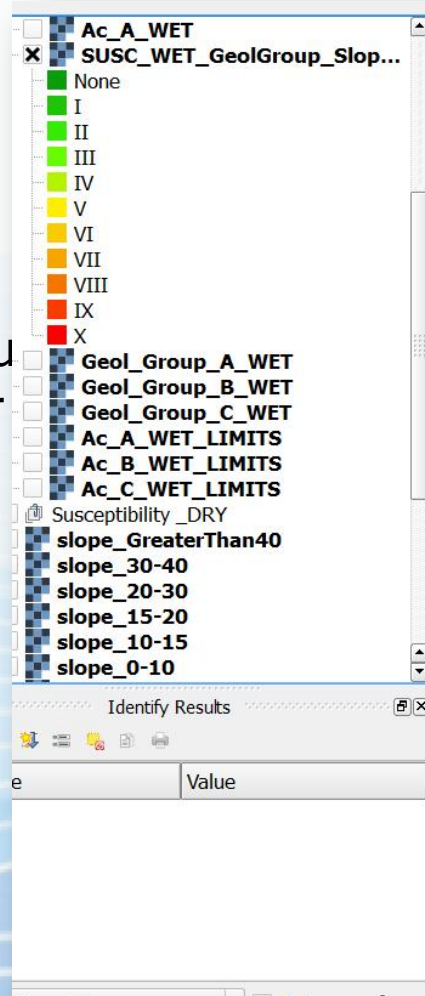
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## Susceptibility under different moisture conditions

is calculated by  
adding the individu  
Susceptibilities Per  
Geologic Group





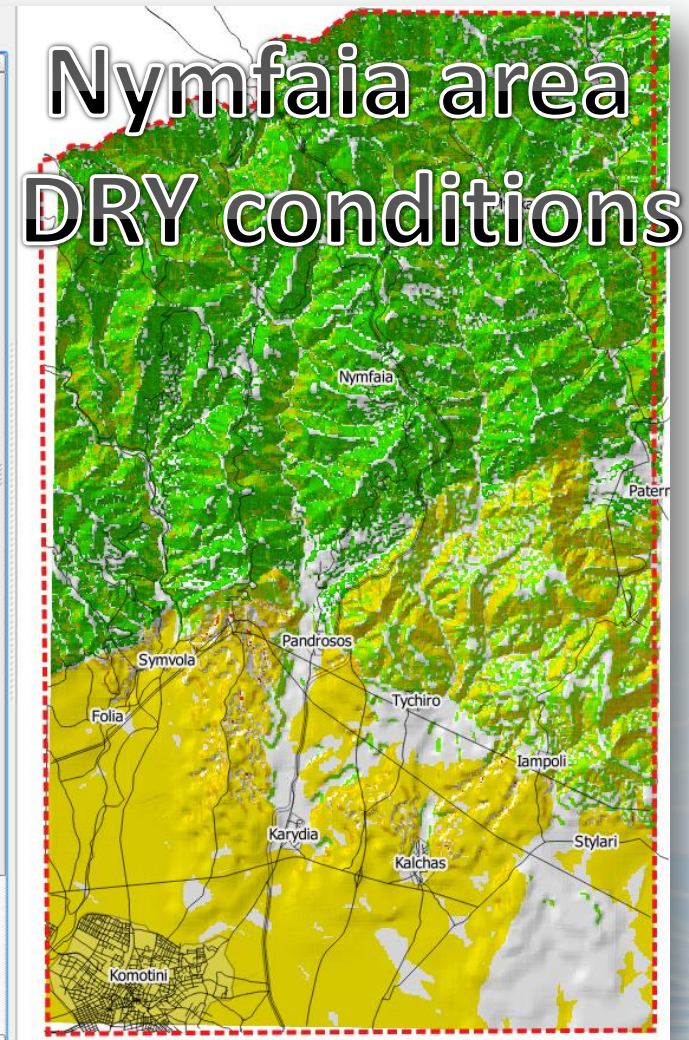
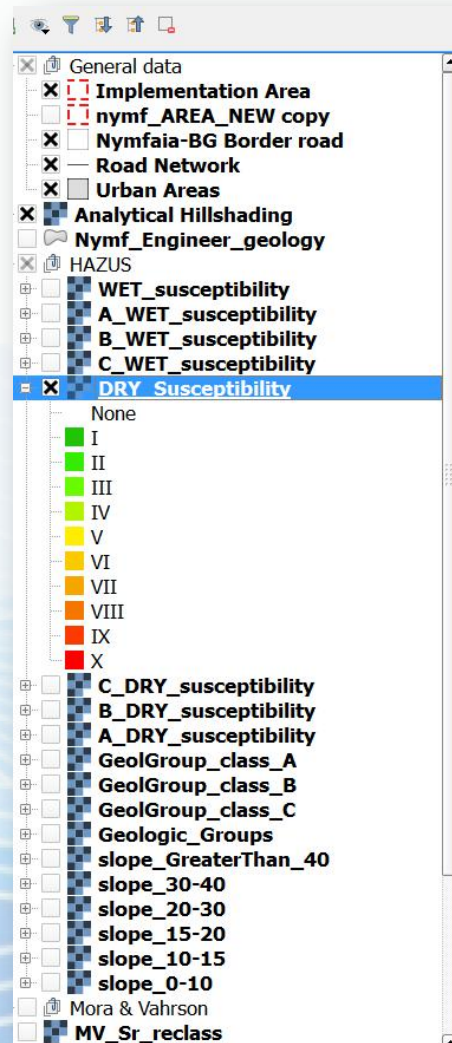
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Common borders. Common solutions.

## Susceptibility under different moisture conditions

is calculated by adding the  
individual Susceptibilities Per  
Geologic Group





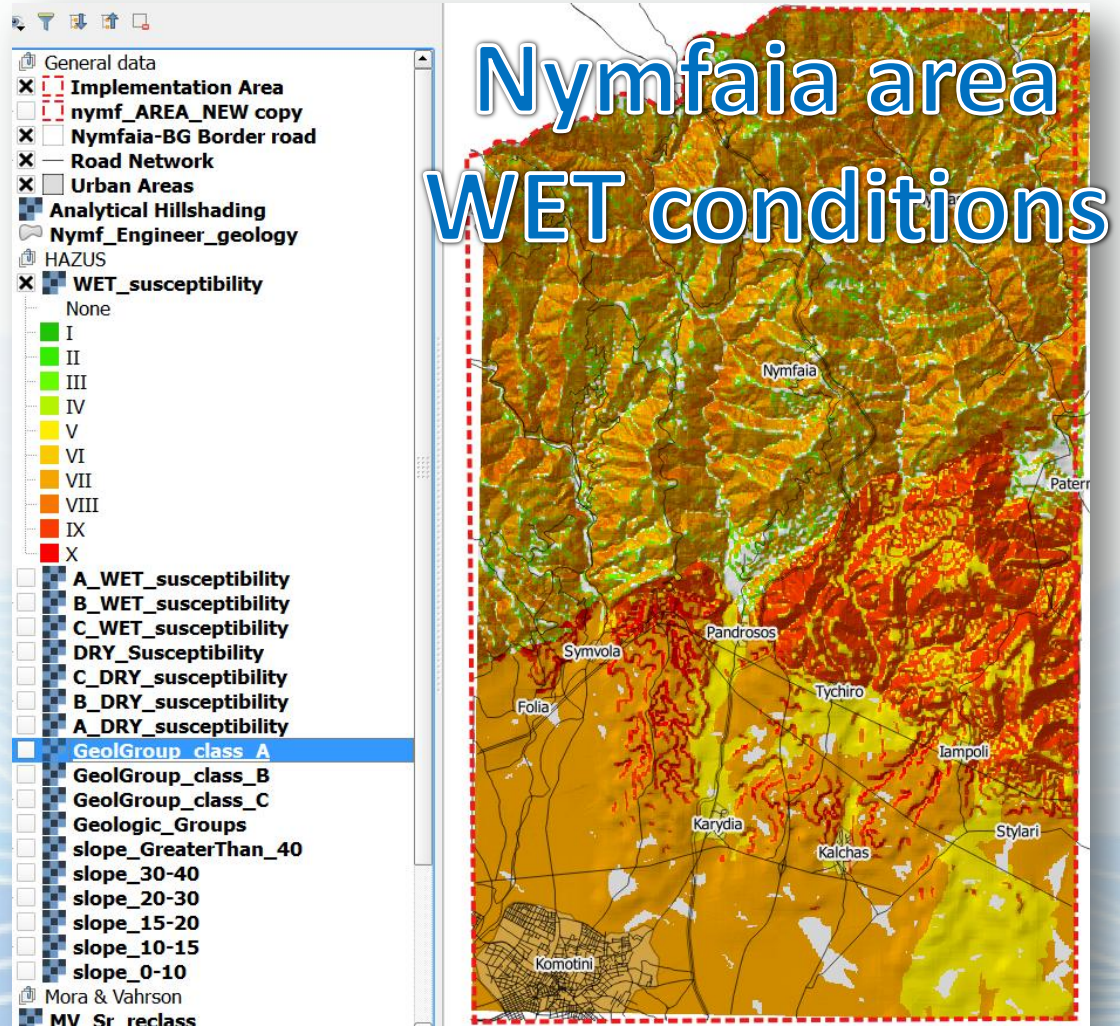
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Common borders. Common solutions.

## Susceptibility under different moisture conditions

is calculated by adding the  
individual Susceptibilities Per  
Geologic Group



Common borders. Common solutions.

## 2. Landslide Susceptibility under seismic conditions

**Limit Equilibrium Method principle:** an earthquake is considered as a horizontal force (seismic coefficient \* weight of the potentially sliding mass of a slope)

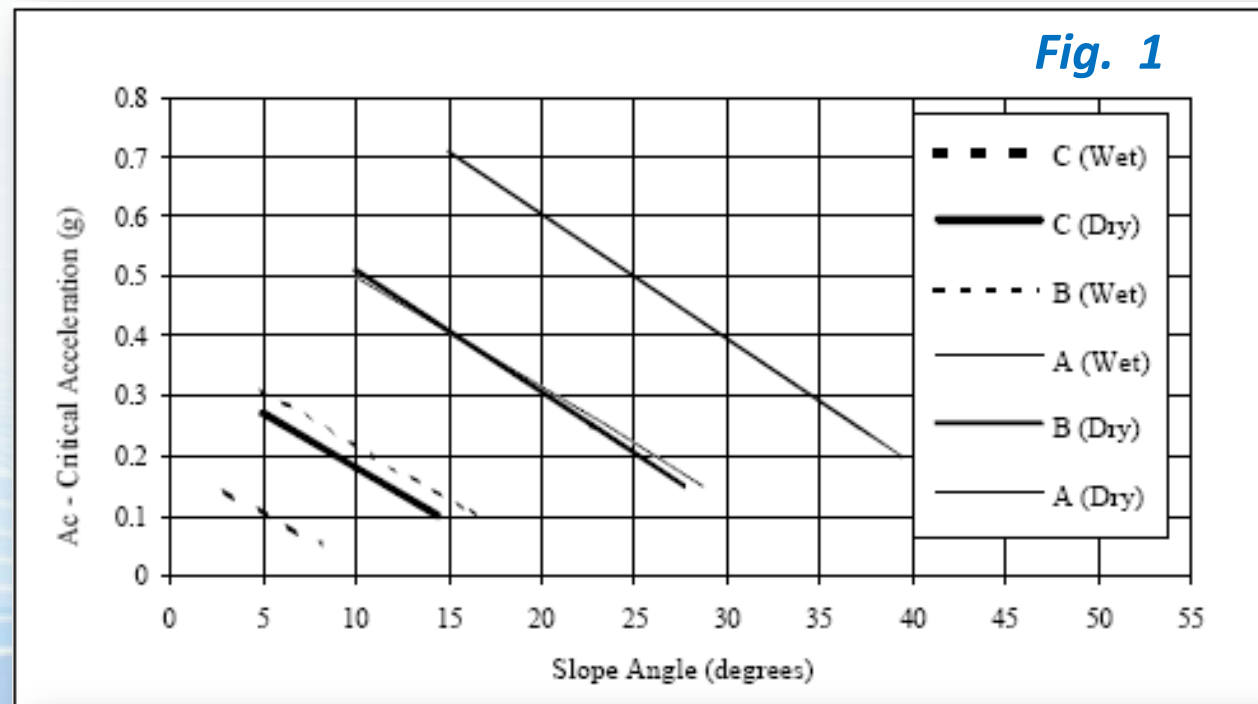
**Critical Acceleration ( $A_c$ )** is defined as the horizontal acceleration that produces a  $F_s = 1.0$

Common borders. Common solutions.

## Calculating the Critical Acceleration $A_c$

**Critical Acceleration ( $A_c$ )** is a complex function of **slope, geology, steepness, groundwater table, type of landsliding & history of previous slope performance.**

There are certain limits (bounds) for these relations (as shown in the graph)

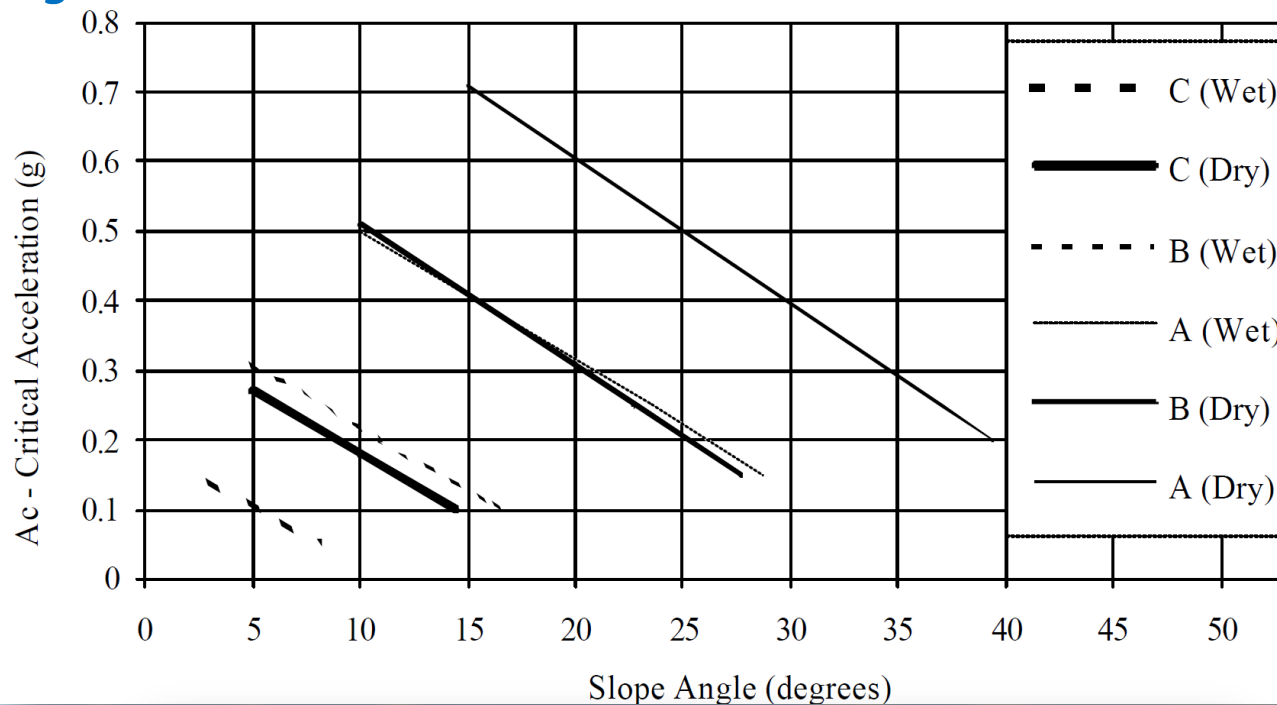


**Critical Acceleration as a Function of Geologic Group and Slope Angle (Wilson and Keefer, 1985).**

Common borders. Common solutions.

## Slope limits for a valid $A_c$

**Fig. 1**



**Critical Acceleration as a Function of Geologic Group and Slope Angle  
(Wilson and Keefer, 1985).**

	Slope Limits	
Geology	LOWER	HIGHER
<b>A_dry</b>	15	39
<b>B_dry</b>	10	27.80
<b>C_dry</b>	5	14.5
<b>A_wet</b>	10	28.75
<b>B_wet</b>	5	17
<b>C_wet</b>	3	8

**Table 9.** Upper and lower bounds of  $A_c$  calculated values

Common borders. Common solutions.

# Limits of slope angles and Critical Accelerations

**Table 10**

Group	Slope Angle, degrees		Critical Acceleration (g)	
	Dry Conditions	Wet Conditions	Dry Conditions	Wet Conditions
A	15	10	0.20	0.15
B	10	5	0.15	0.10
C	5	3	0.10	0.05

**Table 11** Critical Accelerations ( $a_c$ ) for Susceptibility Categories

Susceptibility Category	None	I	II	III	IV	V	VI	VII	VIII	IX	X
Critical Accelerations (g)	None	0.60	0.50	0.40	0.35	0.30	0.25	0.20	0.15	0.10	0.05

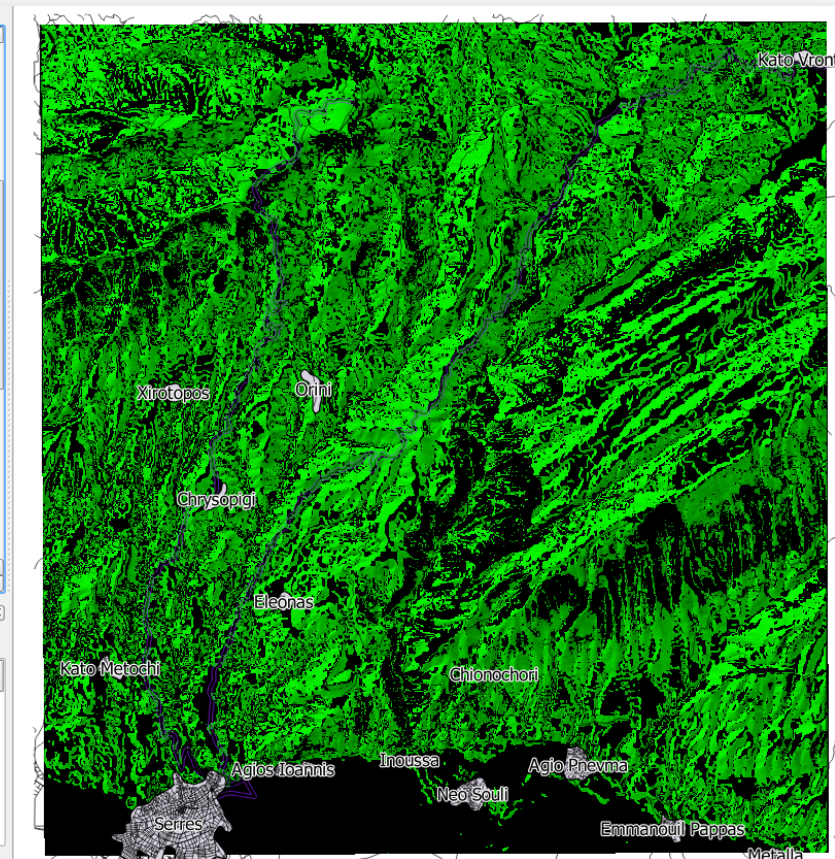
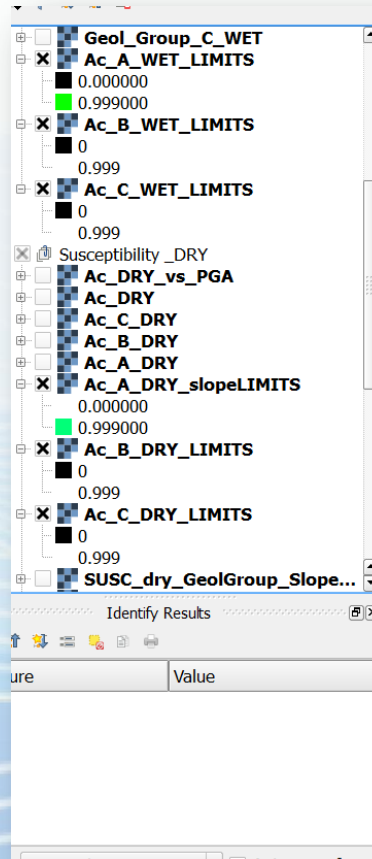
Common borders. Common solutions.

## Definition of Slope lower bounds for calculating a valid value of $Ac$ (how to...)

To calculate the  $Ac$  calculation **slope based limits** (Table 2: 10-28 degrees) for the **Geologic Group “A” - WET conditions**, in QGIS Raster Calculator insert:

"slope\_CLIP@1" >= 10 AND  
"slope\_CLIP@1" <= 28

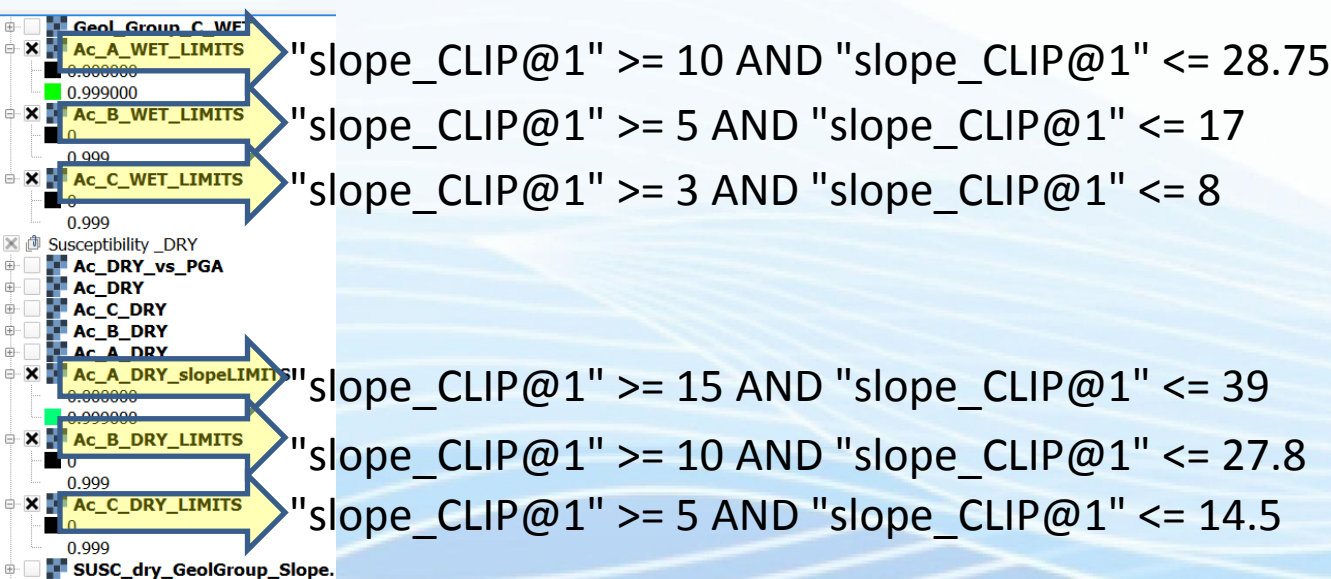
Where: “slope\_CLIP” is the slope map of the area in degrees



Common borders. Common solutions.

## Definition of Slope lower bounds for calculating a valid value of Ac (equations)

ie. To calculate the Ac calculation slope based limits (Table 2) for each **Geologic Group** and **WET conditions**, in QGIS Raster Calculator insert:



The screenshot shows the QGIS Raster Calculator interface with several expressions entered for different layers. The expressions are as follows:

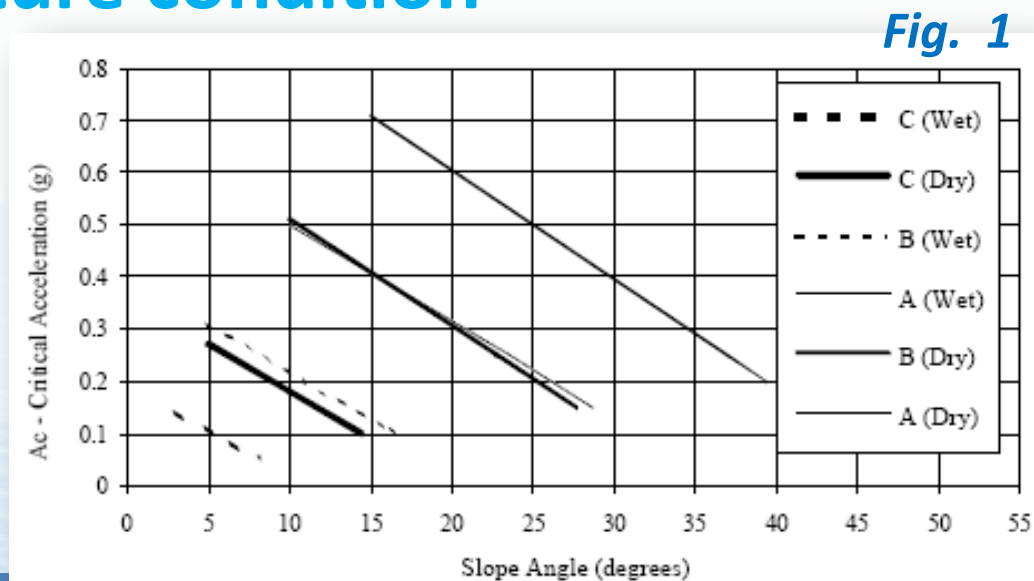
- Geol\_Group\_C\_WET**: "slope\_CLIP@1" >= 10 AND "slope\_CLIP@1" <= 28.75
- Ac\_A\_WET\_LIMITS**: "slope\_CLIP@1" >= 5 AND "slope\_CLIP@1" <= 17
- Ac\_B\_WET\_LIMITS**: "slope\_CLIP@1" >= 3 AND "slope\_CLIP@1" <= 8
- Ac\_C\_WET\_LIMITS**: "slope\_CLIP@1" >= 15 AND "slope\_CLIP@1" <= 39
- Ac\_A\_DRY\_LIMITS**: "slope\_CLIP@1" >= 10 AND "slope\_CLIP@1" <= 27.8
- Ac\_B\_DRY\_LIMITS**: "slope\_CLIP@1" >= 5 AND "slope\_CLIP@1" <= 14.5
- Ac\_C\_DRY\_LIMITS**: "slope\_CLIP@1" >= 5 AND "slope\_CLIP@1" <= 14.5
- SUSC\_dry\_GeolGroup\_Slope.**: (Expression not fully visible)

	Slope Limits	
GeolGr	LOWER	HIGHER
A_wet	10	28.75
B_wet	5	17
C_wet	3	8
A_dry	15	39
B_dry	10	27.80
C_dry	5	14.5

Common borders. Common solutions.

## Calculate the $A_c$ for EACH geologic Group and moisture condition

To that end, we need the **equations for calculating  $A_c$**  as a function of “Slope Angle”, as shown in Wilson & Keefer diagramm



	A dry	A wet	Bdry	Bwet	Cdry	Cwet
Slope	-0.02094	-0.0186	-0.20469	-0.01794	-0.01815	-0.01676
Interception	1.025017	0.68664	7.169656	0.397308	0.362313	0.187761
R	-0.99999	-0.9999	-0.99998	-0.99974	-0.99997	-0.99903

Common borders. Common solutions.

## Ac calculation for EACH geologic Group and moisture condition

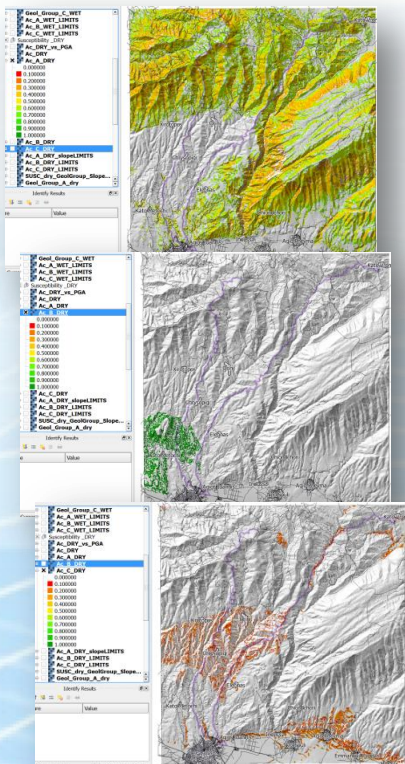
Equations in RasterCalc : "Slope Based Upper and Lower Bounds" \* "Geologic Group Category" \* [equation for calculating Ac as a function of SLOPE]

"Ac\_A\_DRY\_slopeLIMITS@1" \* "C\_hazus\_A\_category@1" \* ( 1.025017 - 0.02094 \* "slope\_CLIP@1" )

"Ac\_B\_DRY\_LIMITS@1" \* "C\_hazus\_B\_category@1" \* ( 7.169656 - 0.20469 \* "slope\_CLIP@1" )

"Ac\_C\_DRY\_LIMITS@1" \* "C\_hazus\_C\_category@1" \* ( 0.362313 - 0.01815 \* "slope\_CLIP@1" )

***Respective equations are used for calculating the Ac limits for WET conditions***



Common borders. Common solutions.

## PGA values

**PGA** values are calculated according to the seismic hazard assessment for the examined region (i.e. for 475 years or 1000years or 2000years) with the use of:

- **either** the relevant **Ground Motion Prediction Equations (GMPE)** suitable for the examined region and soil type
- **or** the relevant GMPEs suitable for the examined region and for rock conditions, which we will be multiplied with an amplification factor ( $PGA_i = PGA_R * F_{Ai}$ )

**Local GMPEs (Skarlatoudis et al., 2003) for the case of Greece**

**Example**

$$\log PGA = 1.07 + 0.45M - 1.35 \times \ln(R + 6) + 0.09F + 0.06S \pm 0.286$$

$$\log PGA = 0.86 + 0.45M - 1.27 \times \ln(R^2 + h^2)^{\frac{1}{2}} + 0.10F + 0.06S \pm 0.286$$

Common borders. Common solutions.

## Calculating PGA values

$$PGA_i = PGA * F_{Ai}$$

$PGA_i$  is peak ground acceleration for site class i (in units of g)

$PGA$  is peak ground acceleration for site class B (in units of g)

$F_{Ai}$  is the short period amplification factor for site class i, as specified for spectral acceleration  $S_{AS}(g)$

Site Class B Spectral Acceleration	Site Class				
	A	B	C	D	E
Short-Period, $S_{AS}$ (g)	Short-Period Amplification Factor, $F_A$				
$\leq 0.25$	0.8	1.0	1.2	1.6	2.5
0.50	0.8	1.0	1.2	1.4	1.7
0.75	0.8	1.0	1.1	1.2	1.2
1.0	0.8	1.0	1.0	1.1	0.9
$\geq 1.25$	0.8	1.0	1.0	1.0	0.8*

Soil amplification factors (Hazus 99-SR2 Technical Manual, Chapter 4-PESH)

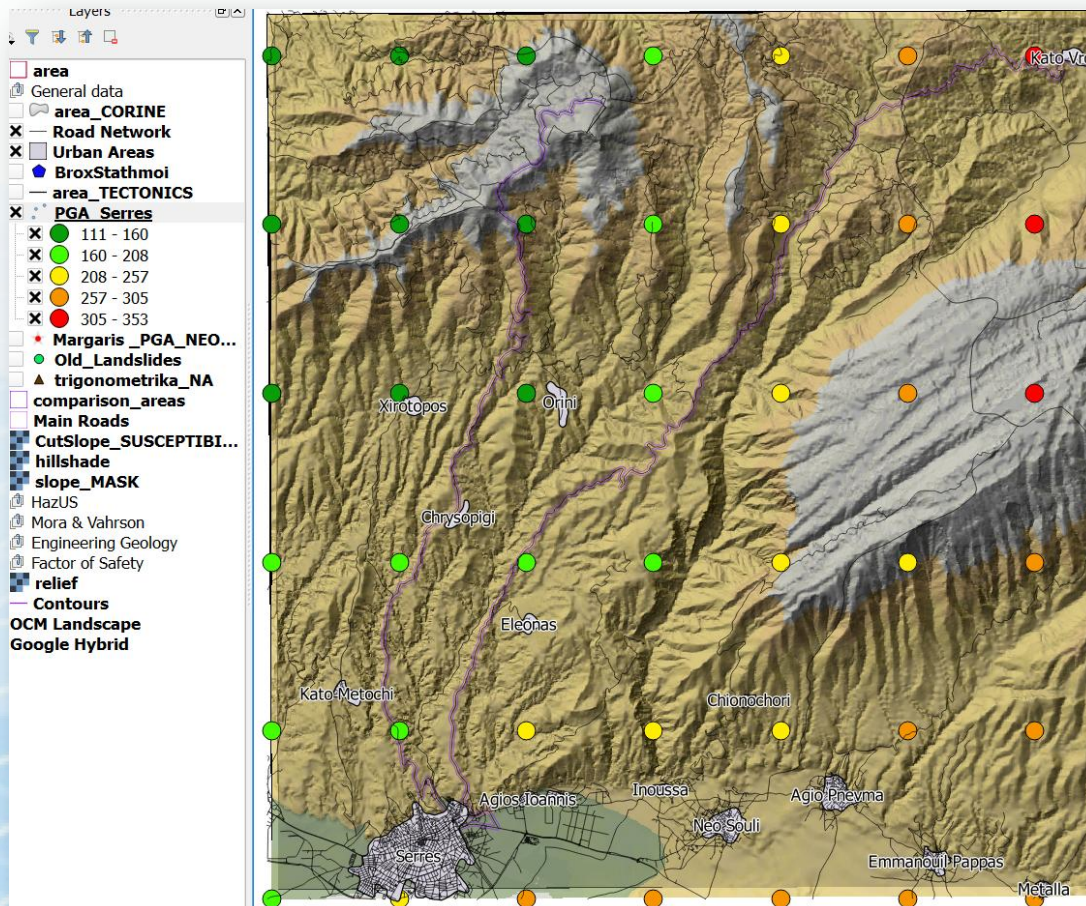


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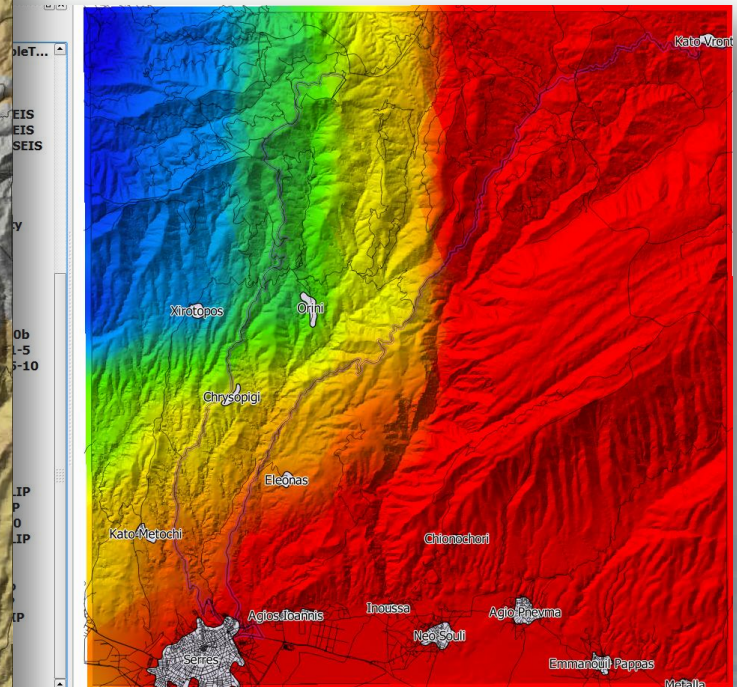


Common borders. Common solutions.

# PGA values for Serres pilot implementation area



## PGA values





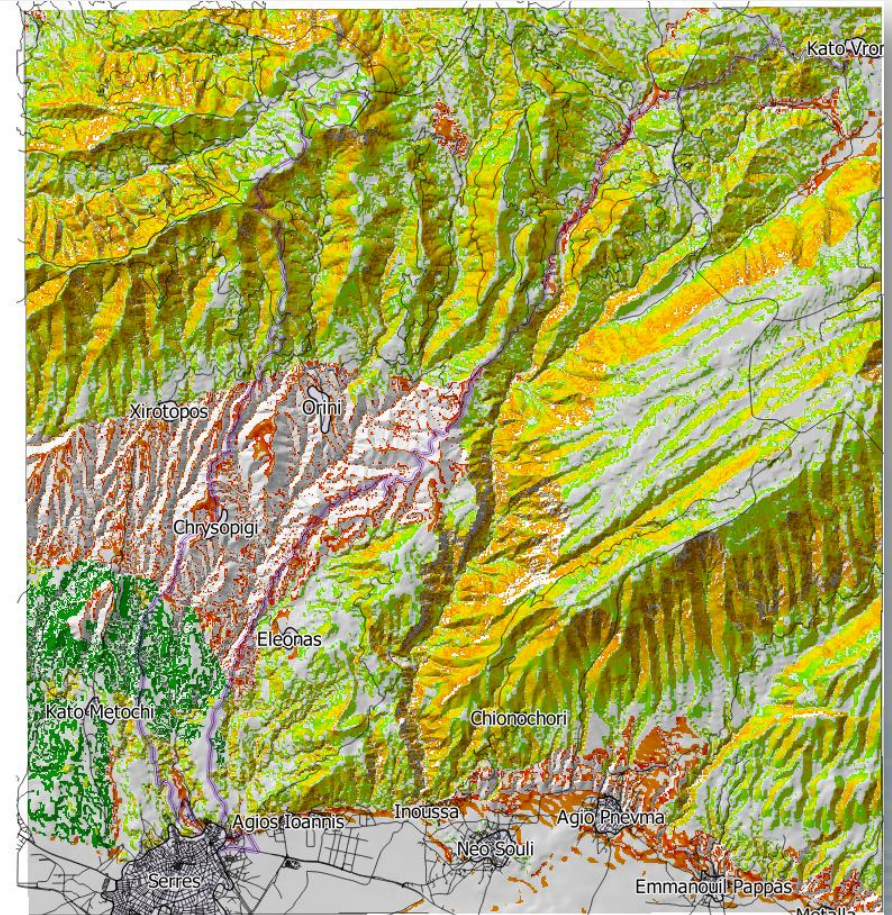
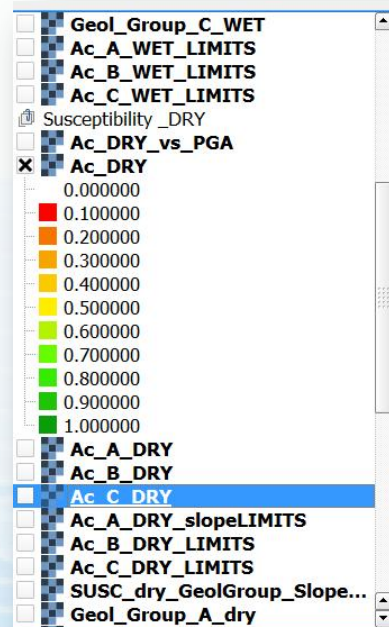
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Common borders. Common solutions.

## Ac calculation for EACH geologic Group and moisture condition

ADD the  $Ac\_A\_DRY$  +  
 $Ac\_B\_DRY$  +  $Ac\_C\_DRY$  to  
get the  **$Ac\_DRY$**  of the  
**entire area**



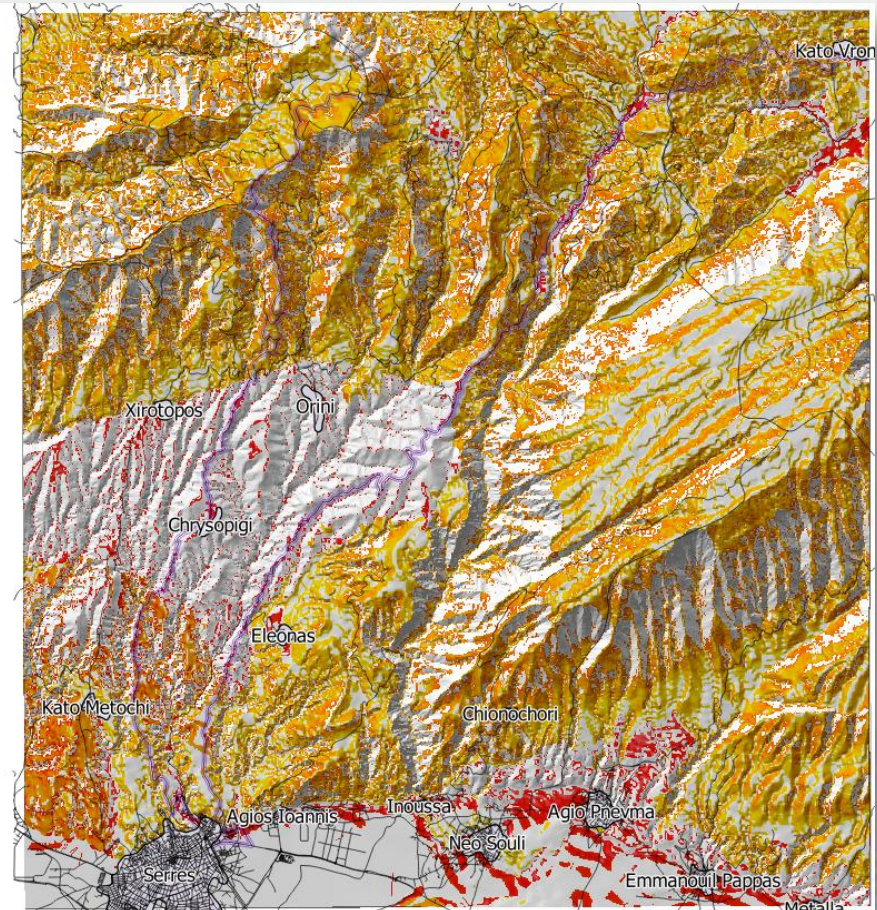
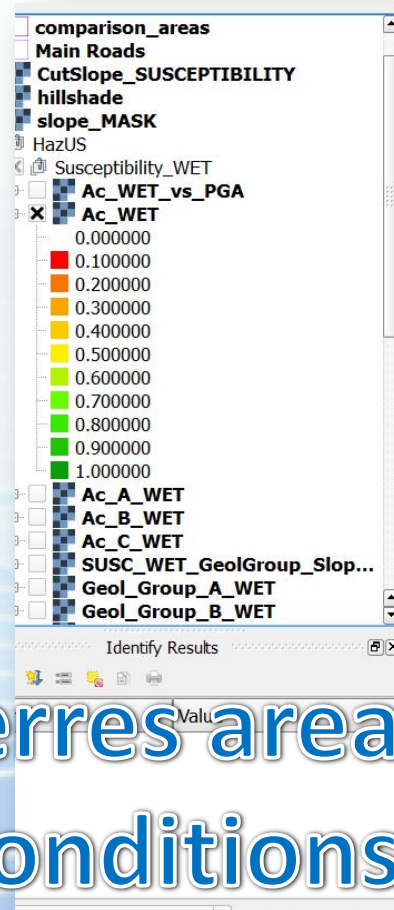
Serres area  
**DRY conditions**

Common borders. Common solutions.

## Ac calculation for EACH geologic Group and moisture condition

The same procedure with the respective files to calculate the Ac\_WET for the entire area

*Note: High Ac values are missing because of the slope based bounds applied*



Serres area  
WET conditions

Common borders. Common solutions.

## “Shallow” landslide Susceptibility under seismic conditions

**Critical Acceleration ( $A_c$ )** is defined as the horizontal acceleration that produces a  $F_s = 1.0$

### Criterion:

Index  $A_c/PGA$  and a  
“subjective” categorization

- ☐ Very high:  $< 0.3$
- ☐ High:  $0.3 - 0.6$
- ☐ Moderate:  $0.6 - 0.8$
- ☐ Low:  $0.8 - 1.0$
- ☐ Very Low:  $1.0 - 3.0$
- ☐ None:  $> 3.0$

“Shallow” landslide susceptibility to earthquake-induced displacements, as specified by the index  $A_c/PGA$



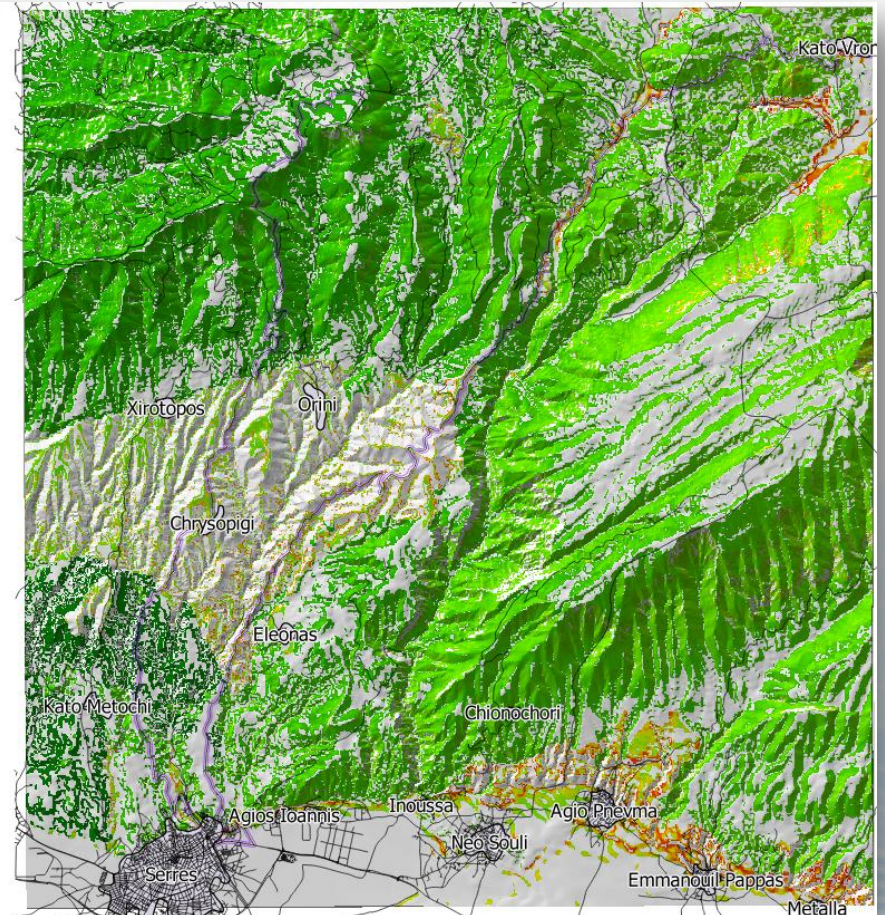
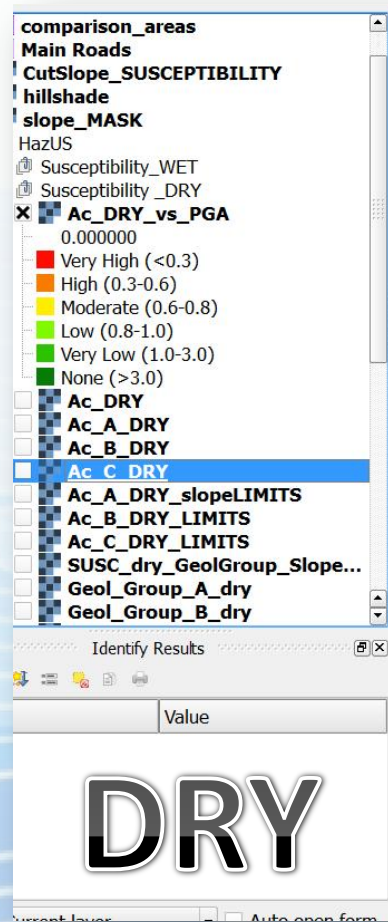
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Common borders. Common solutions.

## “Shallow” landslide susceptibility under seismic conditions

# Ac/PGA





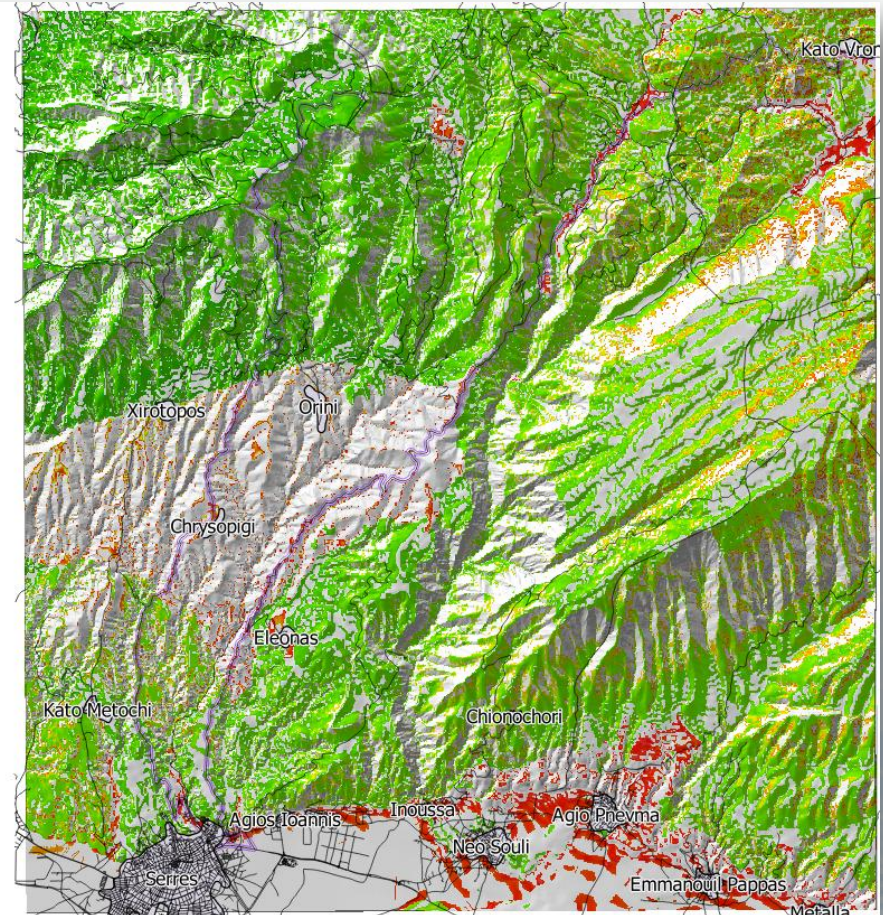
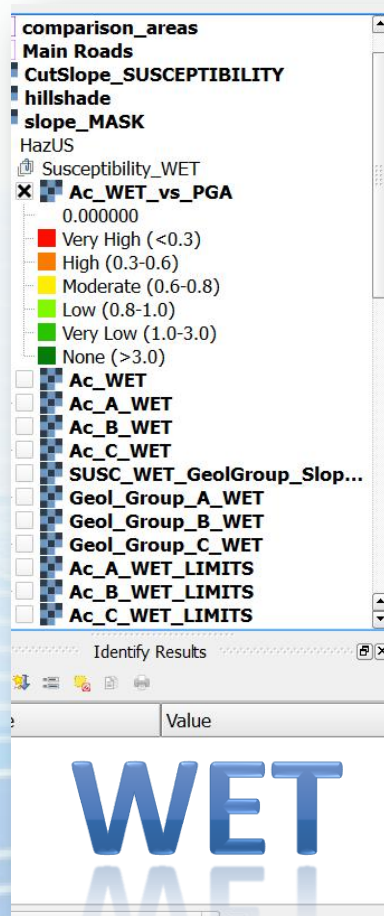
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Common borders. Common solutions.

## “Shallow” landslide susceptibility under seismic conditions

# Ac/PGA

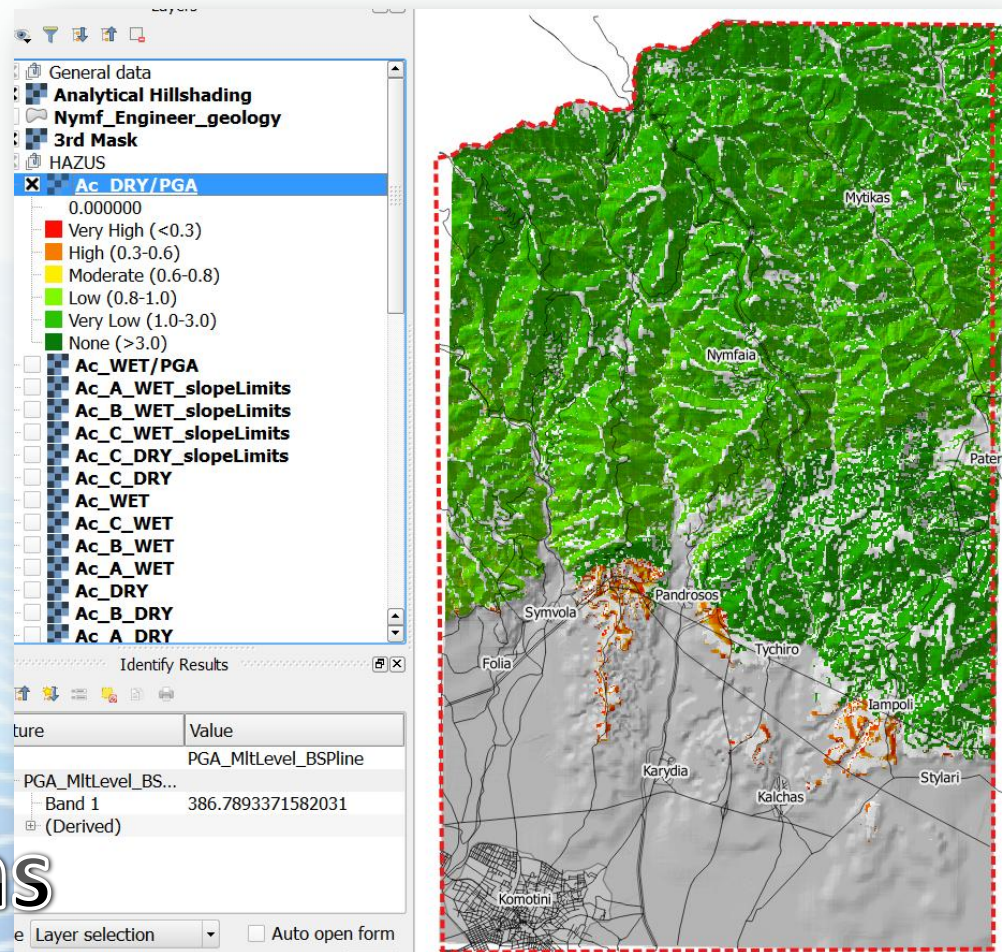


Common borders. Common solutions.

# “Shallow” landslide susceptibility under seismic conditions

## Ac/PGA

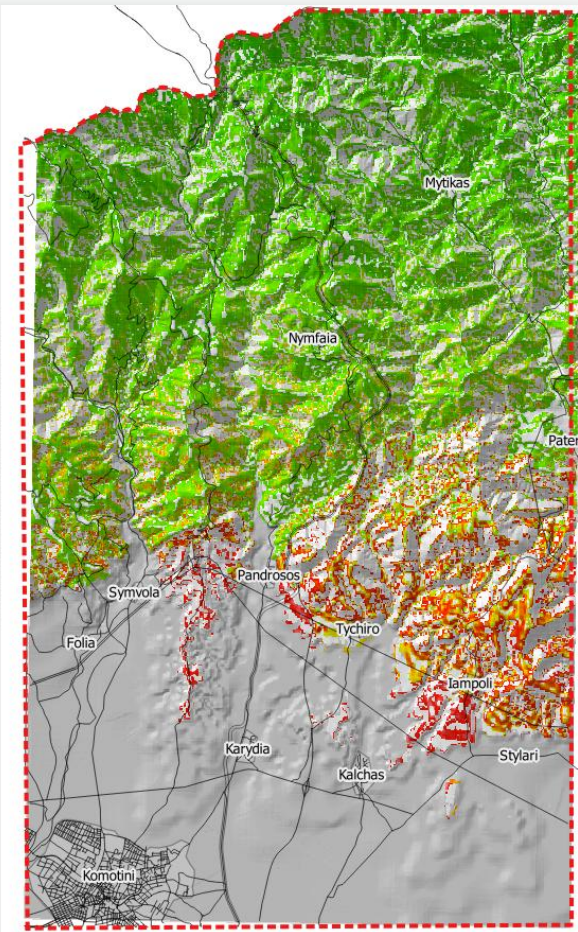
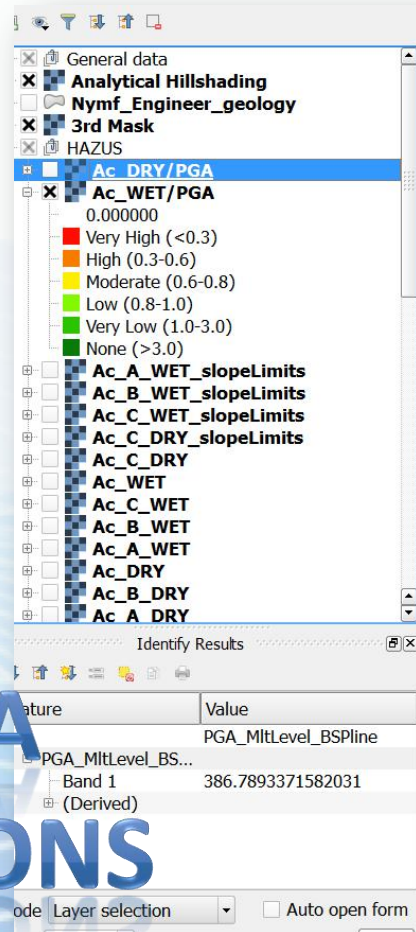
## Nymfaia area DRY conditions



Common borders. Common solutions.

# “Shallow” landslide susceptibility under seismic conditions

Ac/PGA



NYMFAIA AREA  
WET CONDITIONS

Common borders. Common solutions.

### 3. Landslide Hazard under seismic conditions

- Based on FEMA method.
- Hazard is assessed over the calculation of Permanent Ground Displacements
- The methodology is applicable to Hazard assessment of “shallow” landslides

#### Data Requirements

- Data produced during the previous implementation stages

Common borders. Common solutions.

## Permanent Ground Displacements (PGD) assessment

- The FEMA method is based on the assessment of **PGD (Permanent Ground Displacements)** for landslides;
- it is valid for “shallow” landslides, i.e with a depth of the failure surface not exceeding 7 to 10m max from the surface.

Requirements:

**$A_c$ :** critical acceleration (g); has already been analyzed and calculated in previous stages

Common borders. Common solutions.

## Permanent Ground Displacements (PGD) assessment

- The FEMA method is based on the assessment of **PGD (Permanent Ground Displacements)** for landslides (Goodman and Seed, 1966)

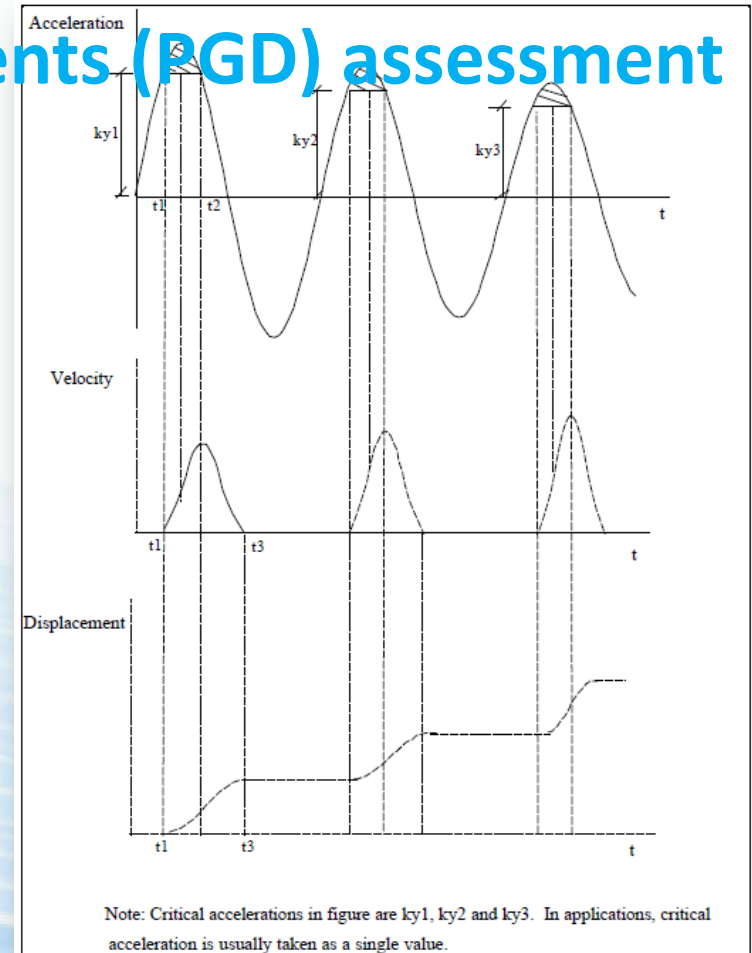


Figure 4.11 Integration of Accelerograms to Determine Downslope Displacements (Goodman and Seed, 1966).

Common borders. Common solutions.

## Permanent Ground Displacements (PGD) assessment

$$E[PGD] = E[d/A_{is}] * A_{is} * n$$

$A_{is}$ : induced acceleration (g) –  $A_{is} = PGA$

$A_{is} = PGA$  : for shallow landslides

$A_{is} = 2/3 * PGA$ : for massive, deep and large landslides

$n$ : number of cycles (function of earthquake magnitude  $M_w$ )

$E[d/A_{is}]$ : expected displacement factor for each cycle

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## n: Number of Cycles (moment Magnitude)

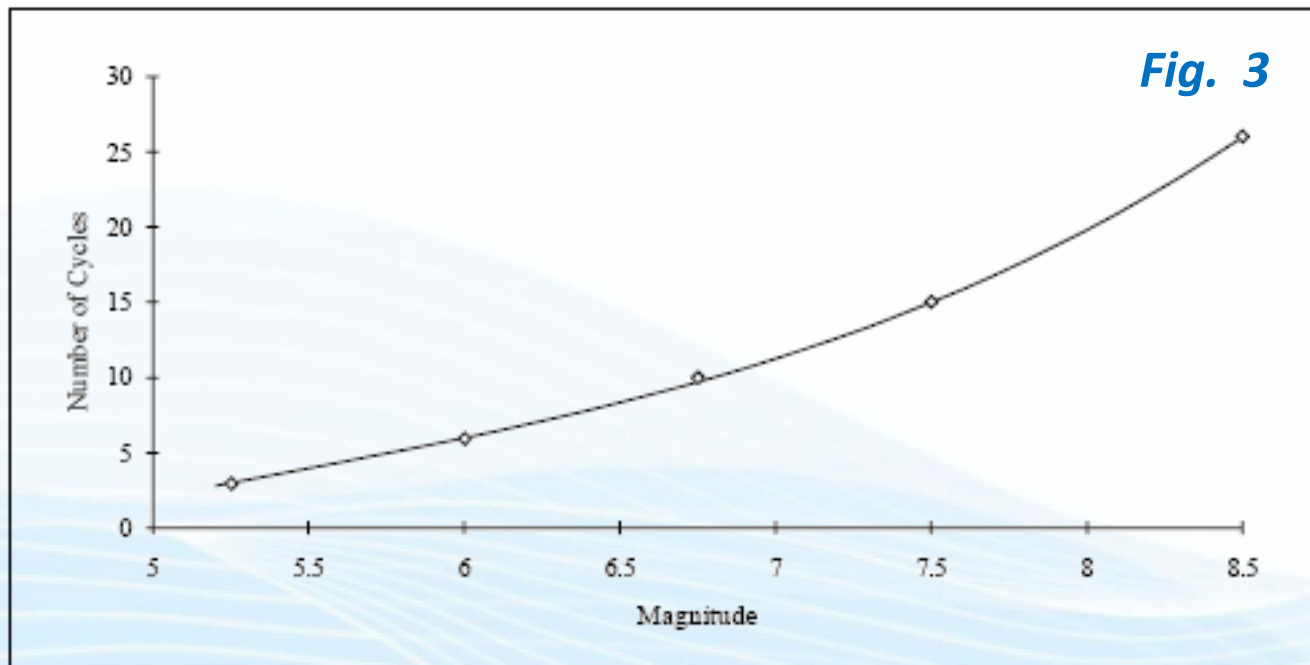


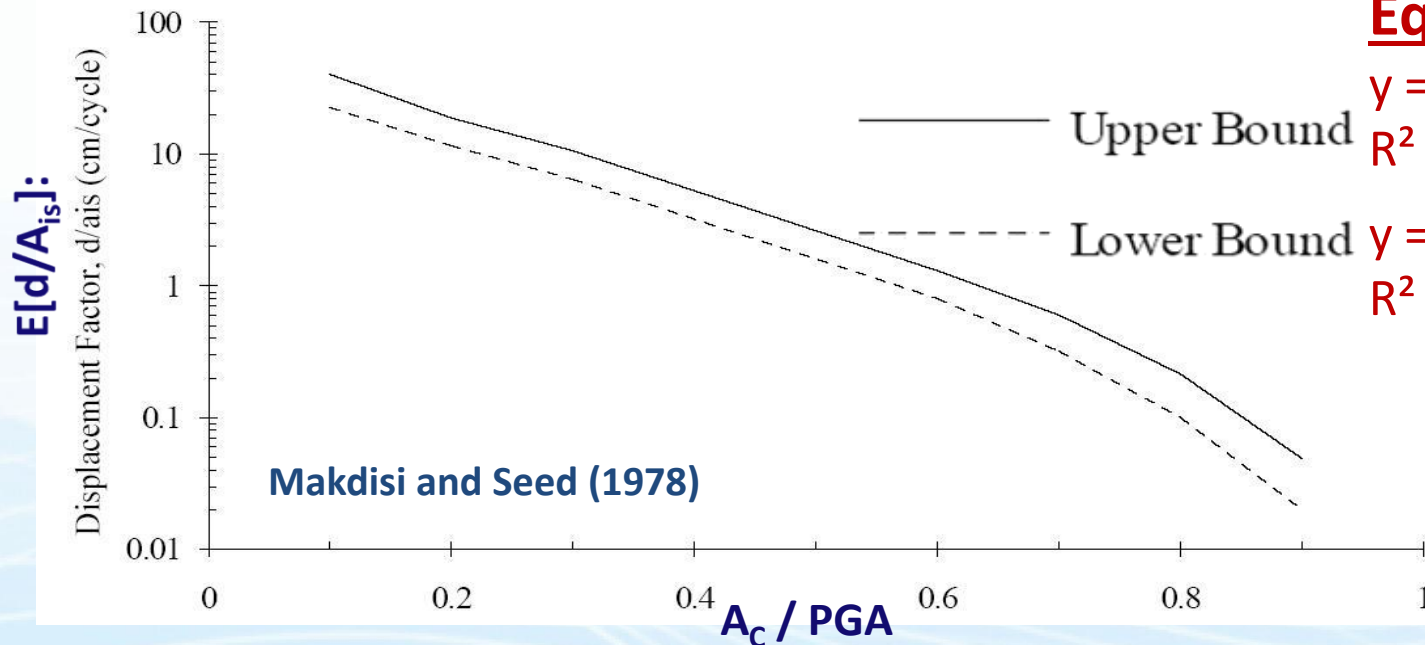
Figure 4.15 Relationship between Earthquake Moment Magnitude and Number of Cycles.

$$n = 0.3419M_w^3 - 5.5214M_w^2 + 33.6154M_w - 70.7692$$

(Seed and Idriss, 1982)

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## Permanent Ground Displacements (PGD) assessment



### Equations

$$y = 103.68e^{-7.784x}$$

$$R^2 = 0.9865$$

$$y = 69.806e^{-7.953x}$$

$$R^2 = 0.9818$$

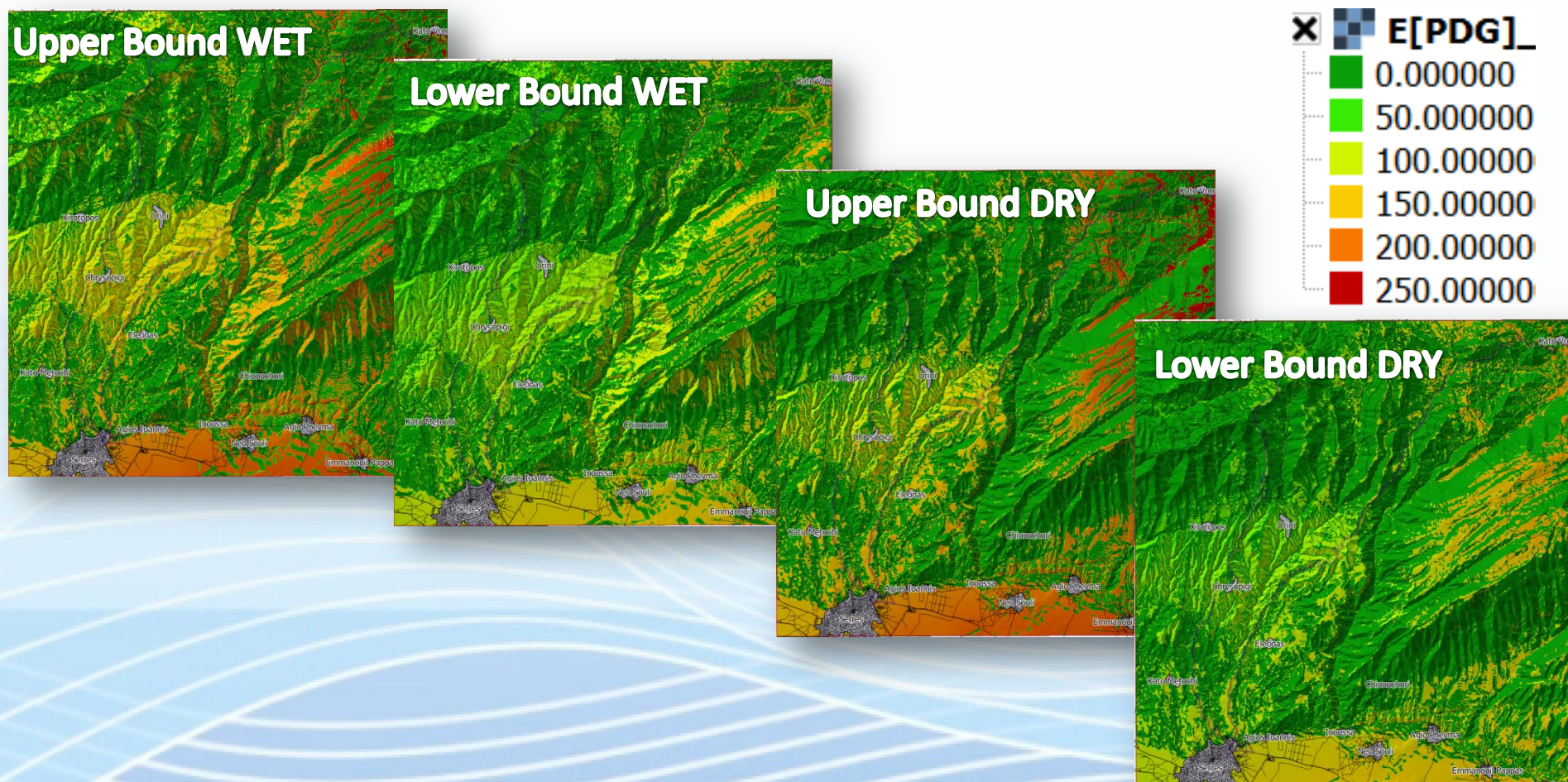
**Fig.2.** Relationship between Displacement Factor and ratio Critical Acceleration ( $A_c$ ) to Induced Acceleration (PGA)

Calculation of the expected displacement factor in cm/cycle. Two (2) equations are given for the lower and upper bound for the earthquake induced permanent displacements



# Common borders. Common solutions.

## Permanent Ground Displacements (PGD) assessment



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## B. FEMA methodology (Hazard US)

Areas of pilot implementation

**END of the 2<sup>nd</sup> cycle**

A. Serres

B. Komotini-Nymfaia

Scale of Regional Implementation

1:50.000 (input data & analysis)

**Thank you!**



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## C. Landslide Hazard Assessment - FS

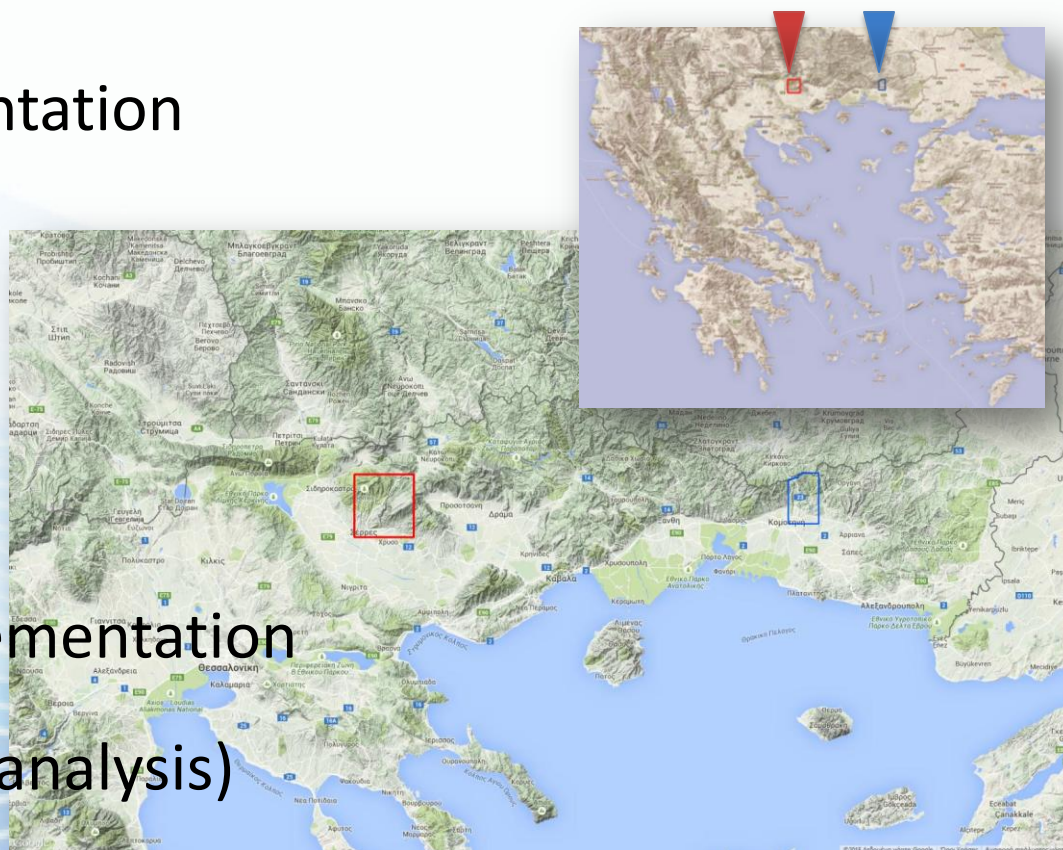
Areas of pilot implementation

**A.** Serres

**B.** Komotini-Nymfaia

Scale of Regional Implementation

1:50.000 (input data & analysis)



Common borders. Common solutions.

# Landslide Hazard Assessment - FS

- Physically based landslide hazard assessment methods are based on *modeling of slope failure processes*
- Applicable over large areas if geological & geomorphological conditions are fairly homogeneous and landslide types relatively simple
- Applicable to areas with incomplete or even non - existing landslide inventories
- Most of them apply the infinite slope model, therefore they are applicable in the case of shallow landslides
- Also, a deterministic model for plane or circular landslides can be applied
- They account for different triggering parameters: rainfall and transient groundwater response or to the effects of earthquake excitation

Common borders. Common solutions.

# Landslide Hazard Assessment - FS

- Physically based landslide hazard assessment methods are based on *modeling of slope failure processes*
- the factor of safety  $F_s$  computation method (**triggering factors: rainfall & earthquake**)

Common borders. Common solutions.

# Landslide Hazard– Static conditions / Precipitation

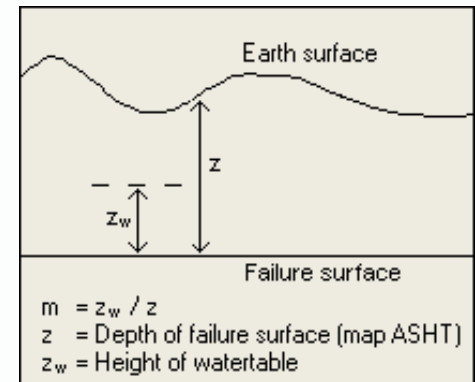
## Infinite Slope Model (Factor of Safety)

$$F_S = \frac{c' + (\gamma_{app} - m * \gamma_w) * z * \cos^2 \beta * \tan \phi'}{\gamma_{app} * z * \sin \beta * \cos \beta}$$

$$\gamma_{app} = \gamma * (1 - m) + \gamma_{sat} * m$$

If totally dry slope, then  $\gamma_{app} = \gamma$  (m=0%)

If totally saturated slope, then  $\gamma_{app} = \gamma_{sat}$  (m=100%)



$\phi'$ : **effective angle of friction** of geomaterial ( $^{\circ}$ )

$c'$ : **effective cohesion** of geomaterial (kPa),

$\gamma$ : **specific weight** (kN/m<sup>3</sup>),

$\beta$ : **slope angle** (Deg),

$\gamma_w$ : **specific weight** of the water (kN/m<sup>3</sup>),

$z$ : **normal thickness** of the failure slab (m)

$m$ : **percentage** of the water **saturated** failure slab (%)

Common borders. Common solutions.

## C. LHA Factor of Safety -Data requirements

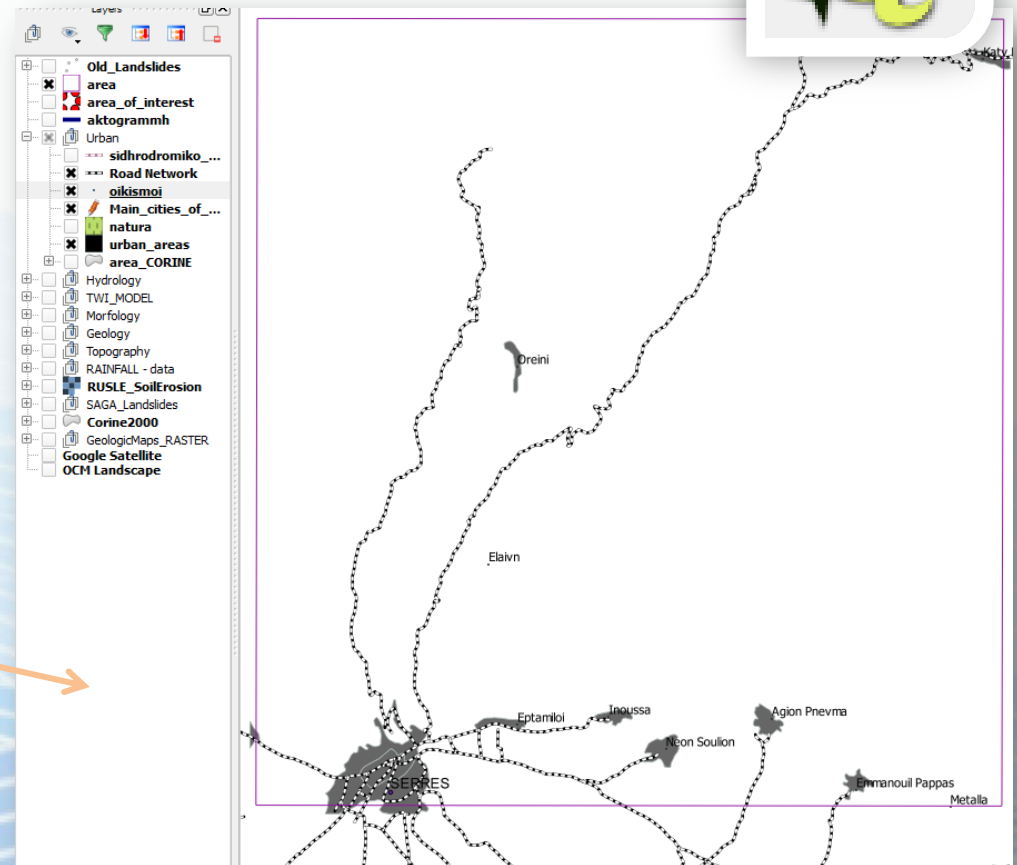
- Scale of Implementation 1:50.000
- Topographic data (topographic Maps, elevation data, lattice points etc). In case topographic data at a 1:50.000 scale are not available, ASTER DEMs can be used at the expense of accuracy.
- Geologic Maps
- Engineering geologic/geotechnical parameters (Cohesion, Friction angle, unit weight)
- Ground Motion data (PGA values)
- Mean Monthly Rainfall (mm) and MAX daily precipitations

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## Basic Info – Starting a Project in



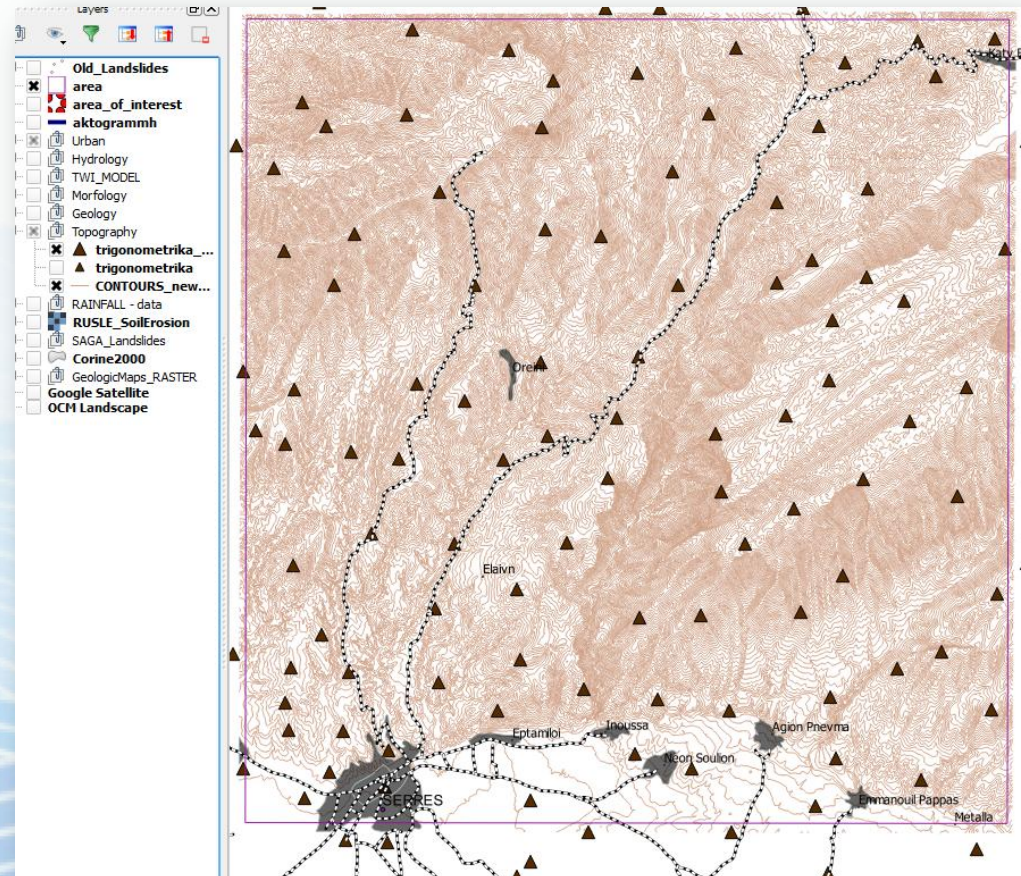
- **Set REFERENCE SYSTEM**
- **Input General data**
  - Road network
  - Railroad network
  - Urban areas ....etc
- **Define the AREA**



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## Topographic Data

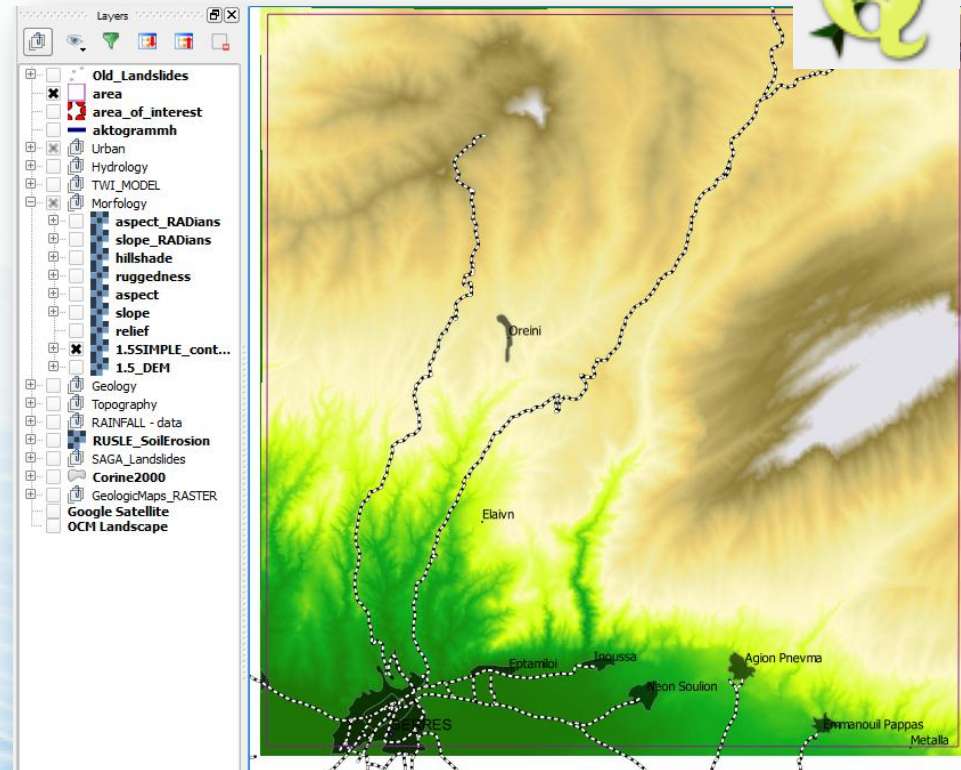
- Input topographic data
  - Contour Lines
  - Elevation points
- **Please Note!** We will be working on a 1:50.000 (Regional) scale



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## Digital Elevation Model

- Create a Digital Elevation Model (DEM)
  - You can use your preferred method
  - ....BUT....
  - Pay attention to the **PIXEL SIZE**. Once defined it can not be changed and all outputs will be based on that. For a 1:50.000 scale map, contours per 20m, a pixel size of 15m is fine!
- In case the DEM covers a larger area, CROP it using the “AREA” polygon.

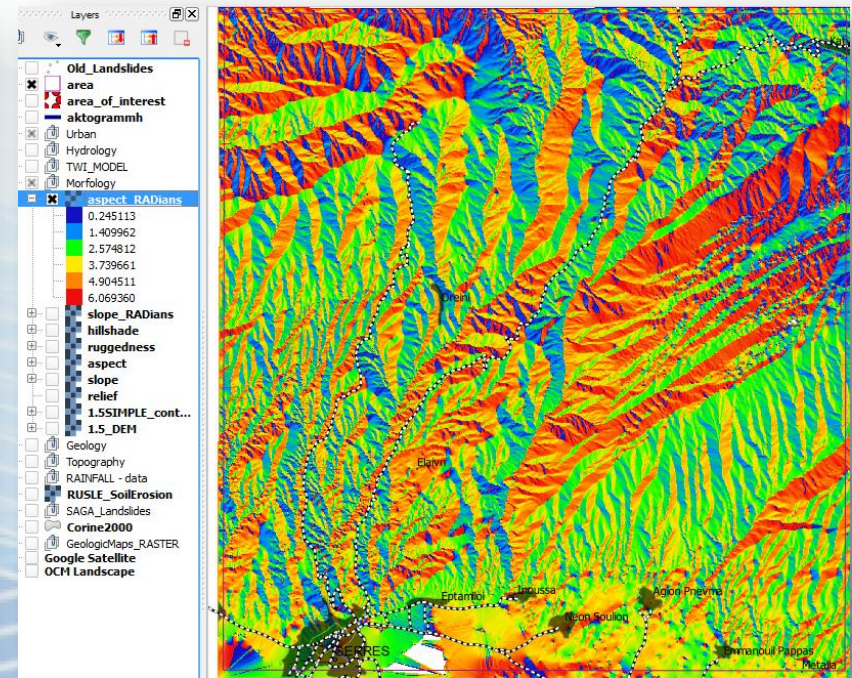
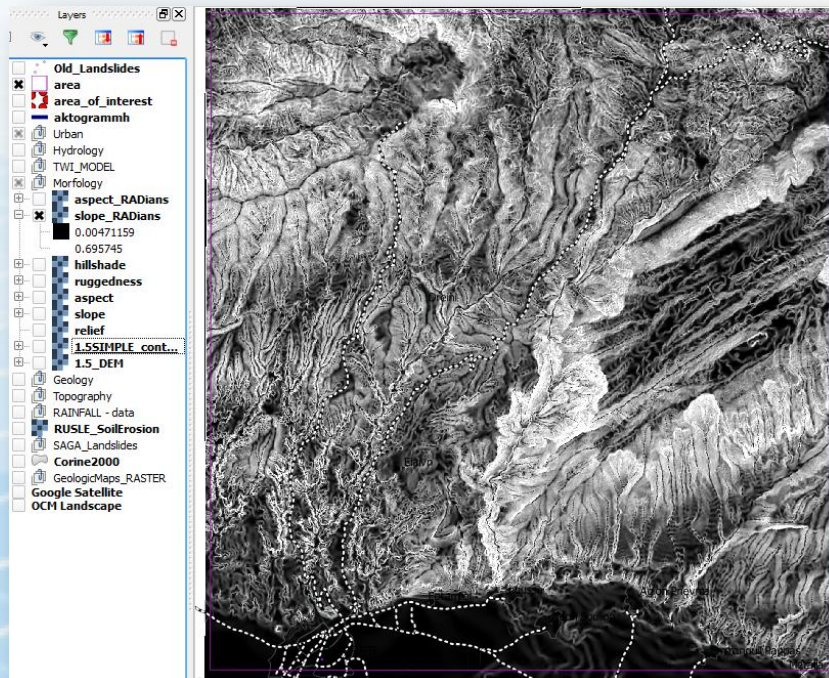


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# Slope and Aspect maps



- Create SLOPE and ASPECT maps
  - **Please Note!** QGIS uses/calculates angles in RADIANS. Conversions in DEGREES may be needed in the process



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## Calculating effective Cohesion ( $c'$ ) and friction angle ( $\phi'$ )

- IF the geological formation is a **ROCKMASS**, then **Hoek and Brown failure criterion** is used in order to establish two pairs of ( $\phi'$  &  $c'$ ) for low and high normal stress (small slope and high slope).
- **GSI (Geological Strength Index) and Uniaxial Compressive Strength** must be estimated according to rockmass lithology and the condition of the rockmass.

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## Geotechnical parameters ( $c'$ , $\phi'$ , $\gamma$ )

- **IF the geological formation is a SOIL**, then according to the geological description (see geological maps) values of  $\phi'$ ,  $c'$  and  $\gamma$  can be attributed according to international bibliography and your experience.

No matter if **SOIL** or **ROCKMASS** is encountered, geotechnical parameters should be estimated or calculated in a conservative way.



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# Analysis of Rock Strength using RocLab

## Analysis of Rock Strength using RocLab

H=5m

### Hoek-Brown Classification

intact uniaxial comp. strength ( $\sigma_{ci}$ ) = 25 MPa  
GSI = 32  $m_i$  = 8 Disturbance factor ( $D$ ) = 1  
intact modulus ( $E_i$ ) = 16875 MPa  
modulus ratio (MR) = 675

### Hoek-Brown Criterion

$m_b = 0.062$   $s = 1.2e-5$   $a = 0.520$

### Mohr-Coulomb Fit

cohesion = 0.027 MPa friction angle = 34.17 deg

### Rock Mass Parameters

tensile strength = -0.005 MPa  
uniaxial compressive strength = 0.069 MPa  
global strength = 0.723 MPa  
deformation modulus = 503.42 MPa

$c' = 27\text{kPa}$

$\phi' = 22^\circ$

## Analysis of Rock Strength using RocLab

H=50m

### Hoek-Brown Classification

intact uniaxial comp. strength ( $\sigma_{ci}$ ) = 25 MPa  
GSI = 32  $m_i$  = 8 Disturbance factor ( $D$ ) = 1  
intact modulus ( $E_i$ ) = 16875 MPa  
modulus ratio (MR) = 675

### Hoek-Brown Criterion

$m_b = 0.062$   $s = 1.2e-5$   $a = 0.520$

### Mohr-Coulomb Fit

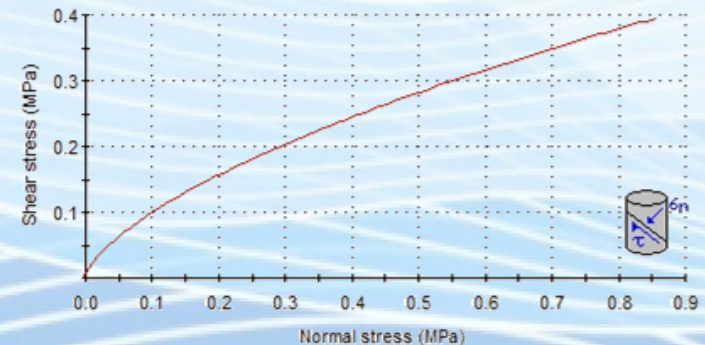
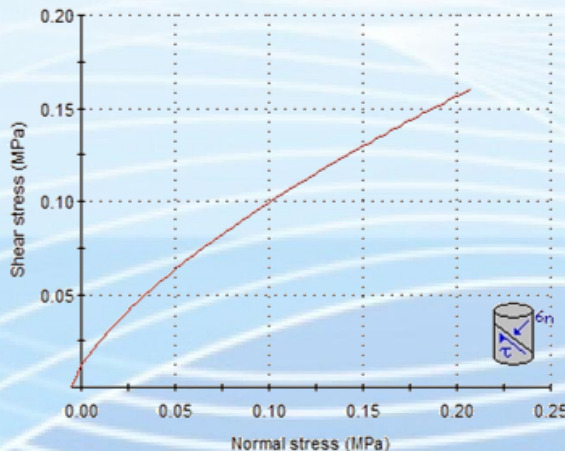
cohesion = 0.072 MPa friction angle = 21.91 deg

### Rock Mass Parameters

tensile strength = -0.005 MPa  
uniaxial compressive strength = 0.069 MPa  
global strength = 0.723 MPa  
deformation modulus = 503.42 MPa

<http://www.rocscience.com>

<http://roclab.software.informer.com/1.0/>



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## Calculating effective Cohesion ( $c'$ ) and friction angle ( $\phi'$ )

- Calculate i) Cohesion ( $c'$ ); ii) angle of Internal Friction ( $\phi$ ); iii) Unit Weight and iv) Hydraulic Conductivity for each of the geologic formations of the area

	gn,ab			gn,ab,sch			gn,mr			gn-sch			gn-γ			gn-μv			gn1		
Hoek Brown Classification	H=5m	H=50m		H=5m	H=50m		H=5m	H=50m		H=5m	H=50m		H=5m	H=50m		H=5m	H=50m		H=5m	H=50m	
sigci (Mpa)	100	100		100	100		100	100		100	100		120	120		175	175		100	100	
GSI	30	30		31	31		30	30		29	29		31	31		31	31		33	33	
mi	23	23		23	23		12	12		10	10		26	26		26	26		25	25	
D	1	1		1	1		1	1		1	1		1	1		1	1		1	1	
Ei	40000	40000		30000	30000		85000	85000		30000	30000		48000	48000		70000	70000		30000	30000	
MR	400	400		300	300		850	850		300	300		400	400		400	400		300	300	
Hoek Brown Criterion																					
mb	0.15497	0.15497		0.16645	0.16645		0.08086	0.08086		0.06273	0.06273		0.18816	0.18816		0.18816	0.18816		0.20870	0.20870	
s	8.57E-06	8.57E-06		1.01E-05	1.01E-05		8.57E-06	8.57E-06		7.26E-06	7.26E-06		1.01E-05	1.01E-05		1.01E-05	1.01E-05		1.41E-05	1.41E-05	
a	0.52234	0.52234		0.52089	0.52089		0.52234	0.52234		0.52390	0.52390		0.52089	0.52089		0.52089	0.52089		0.51826	0.51826	
Failure Envelope Range																					
Application	Slopes	Slopes		Slopes	Slopes		Slopes	Slopes		Slopes	Slopes		Slopes	Slopes		Slopes	Slopes		Slopes	Slopes	
sig3max (Mpa)	0.12892	1.04787		0.12946	1.05227		0.12066	0.98074		0.12344	1.00331		0.13236	1.07584		0.13693	1.11300		0.13103	1.06504	
Unit Weight (MN/m3)	0.026	0.026		0.026	0.026		0.025	0.025		0.026	0.026		0.026	0.026		0.026	0.026		0.026	0.026	
Slope Height (m)	5	50		5	50		5	50		5	50		5	50		5	50		5	50	
Mohr-Coulomb Fit																					
c (Mpa)	0.0587	0.2299		0.0616	0.2391		0.0530	0.1798		0.0500	0.1653		0.0685	0.2671		0.0827	0.3084		0.0688	0.2651	
phi (degrees)	51.6	35.1		52.3	35.9		46.3	29.9		43.6	27.4		54.4	38.3		56.7	41.1		54.3	38.0	
Rock Mass Parameters																					
sigt (Mpa)	-0.0055	-0.0055		-0.0061	-0.0061		-0.0106	-0.0106		-0.0116	-0.0116		-0.0065	-0.0065		-0.0094	-0.0094		-0.0068	-0.0068	
sigc (Mpa)	0.2256	0.2256		0.2503	0.2503		0.2256	0.2256		0.2031	0.2031		0.3004	0.3004		0.4380	0.4380		0.3067	0.3067	
sigcm (Mpa)	4.5577	4.5577		4.7751	4.7751		3.2471	3.2471		2.8123	2.8123		6.1073	6.1073		8.9065	8.9065		5.4597	5.4597	
Erm (Mpa)	1128.98	1128.98		869.793	869.793		2399.08	2399.08		825.615	825.615		1391.67	1391.67		2029.52	2029.52		922.432	922.432	
Results																					
	H(m)	φ	c (kPa)	H(m)	φ	c (kPa)	H(m)	φ	c (kPa)	H(m)	φ	c (kPa)	H(m)	φ	c (kPa)	H(m)	φ	c (kPa)	H(m)	φ	c (kPa)
	5	51.61	58.71	5	52.30	61.65	5	46.31	52.98	5	43.63	50.02	5	54.43	68.54	5	56.70	82.66	5	54.27	68.77
	50	35.14	229.90	50	35.88	239.11	50	29.90	179.85	50	27.39	165.30	50	38.29	267.10	50	41.10	308.41	50	38.04	265.11
Final Values		φ	c (kPa)		φ	c (kPa)		φ	c (kPa)		φ	c (kPa)		φ	c (kPa)		φ	c (kPa)		φ	c (kPa)
		35	59		36	62		30	53		27	50		38	69		41	83		38	69

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## Geotechnical Parameters Spatial Distribution

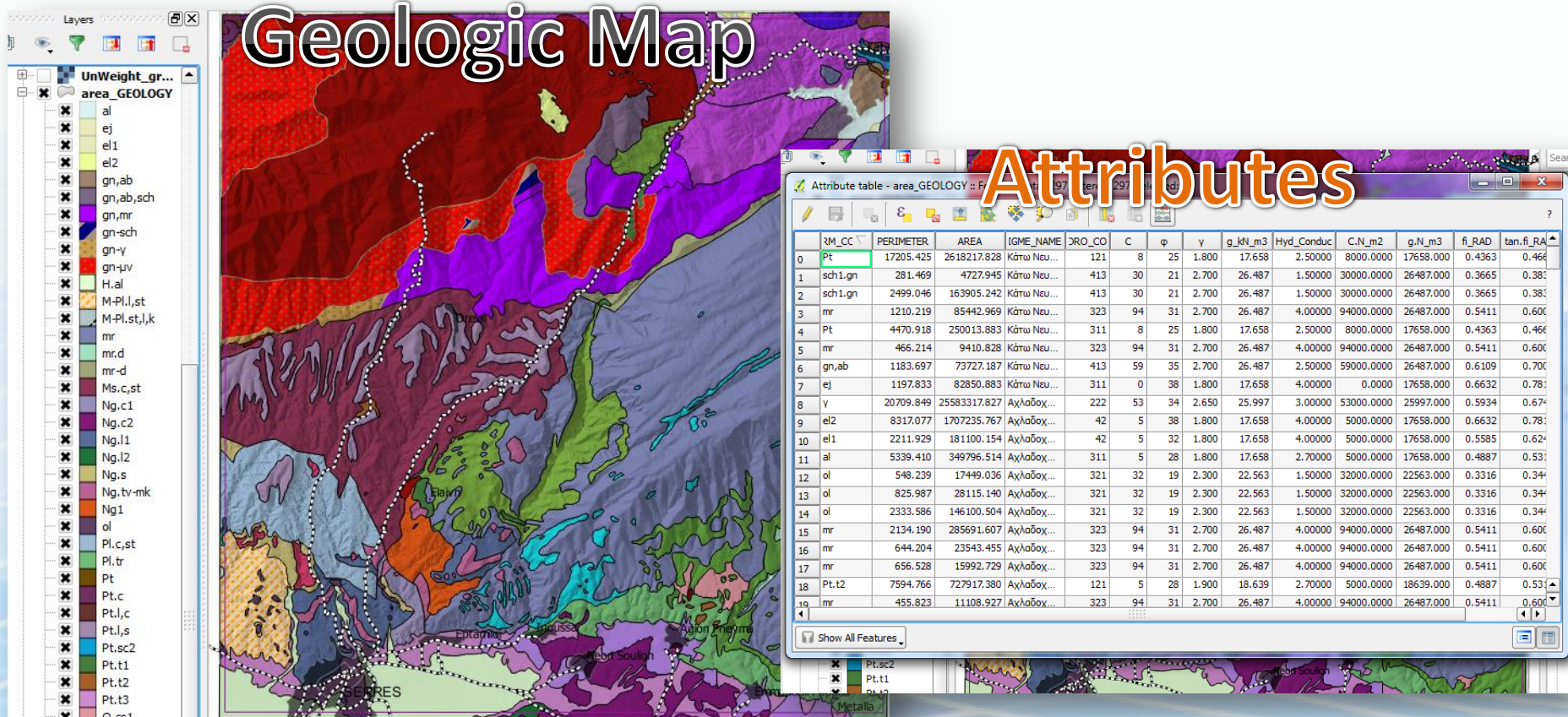
- Digitize the **Geologic Map**
- **Assign additional attributes** to geologic formation polygons
  - C: effective Cohesion
  - $F_i$  ( $\phi$ ): effective Internal Friction angle
  - Hc: hydraulic conductivity
  - ...etc....
- **Please! Pay attention to** the respective to each parameter,  
**UNITS**

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# Geotechnical Parameters Spatial Distribution

## Geologic Map

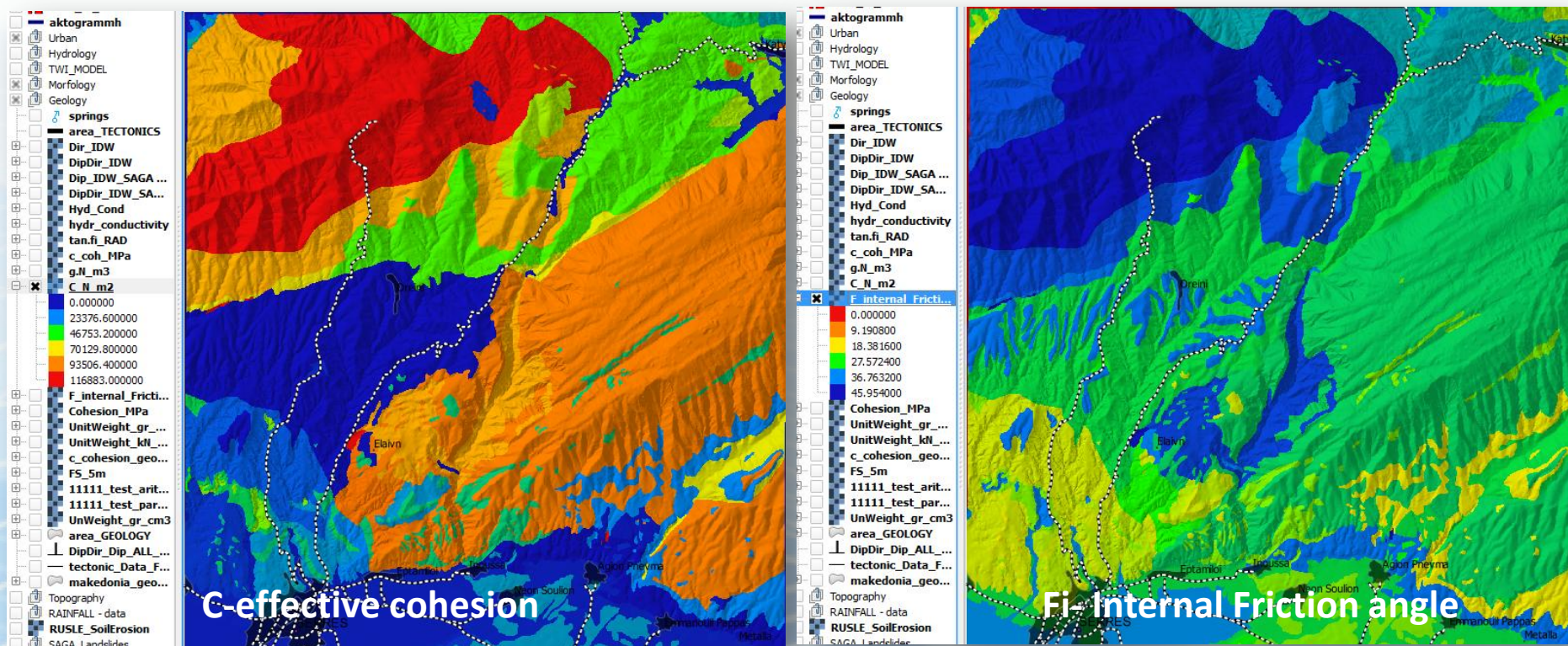
## Attributes



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## Calculating effective Cohesion ( $c'$ ) and friction angle ( $\phi'$ )

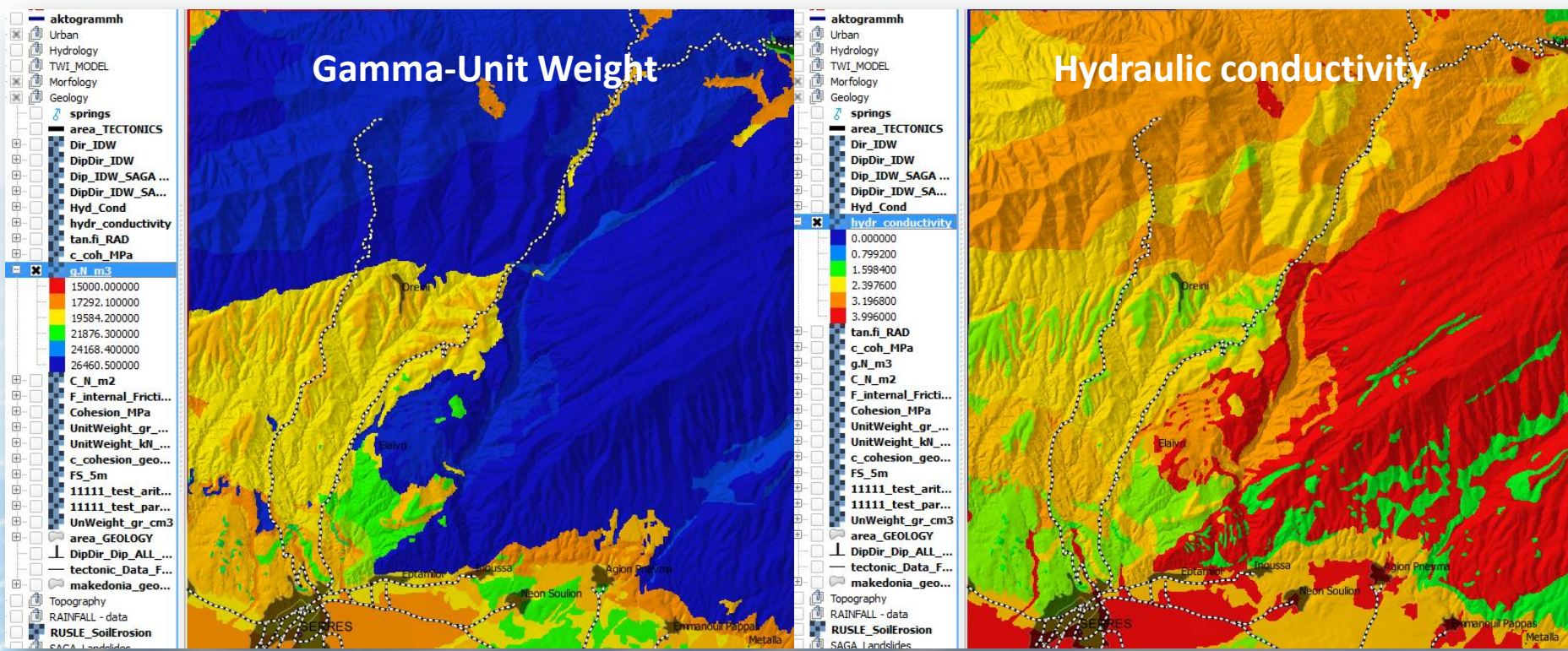
- Preparing the parameters for the calculation of Factor of Safety (convert vector to Raster);  $c'$  – effective cohesion and  $\phi'$  – Internal Friction angle



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## Unit Weight & Hydraulic Conductivity Spatial Distribution

- Preparing the parameters for the calculation of Factor of Safety: Unit Weight and Hydraulic Conductivity (needed to calculate Saturation in SAGA GIS)



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# Thickness and saturation of sliding slab

The Most difficult parameters to estimate for the infinite slope model !

**z: normal thickness of the failure slab (m)**

**m: percentage of saturation of the failure slab (%)**

- **Normal thickness of failure slab (z)** is to be determined as a function of slope angle ( $\beta$ ), in order to calculate the factor of safety
- **Percentage of saturation (m %)** needs to be correlated with rainfall (mm) and a mean return period for the rainfall event (if such data exist for the examined region)

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# Thickness and saturation of sliding slab

- **The Normal thickness of failure slab ( $z$ )** can be defined parametrically (i.e. 1m, 5m, 10m) and taken into account as such or physically based models can be used to link it to soil (and regolith) development natural parameters related to weathering, erosion and deposition (morphometric: slope, curvature, position on slope, etc; hydrologic, geologic etc)

**Indicative Relative Research:** Dietrich and Reiss, 1995; Catani et.al, 2010; Shafique et.al, 2011.

## Potentially useful info:

- [Pan-European Soil Databases for Landslide Mapping \(JRC\)](#)
- [ESDAC Data Inventory](#)
- [EU Soils](#)

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# Saturation percentage of sliding slab

- **Percentage of saturation (m %)** needs to be correlated with rainfall (mm) and a mean return period for the rainfall event (if such data exist for the examined region)
- Create the Saturation Percentage (SP) using the WETNESS module in SAGA GIS
- Please note! The **SP** is **calculated** for a **respective sliding mass thickness**
- References and help are given within SAGA GIS (shown below).

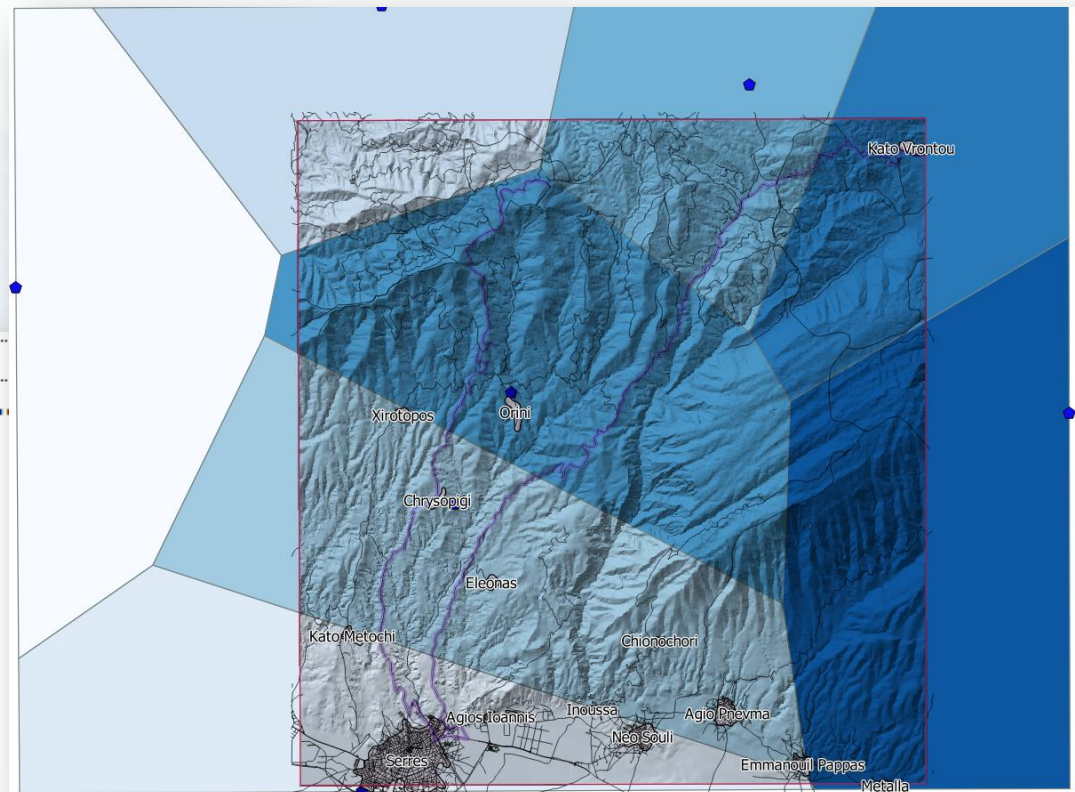
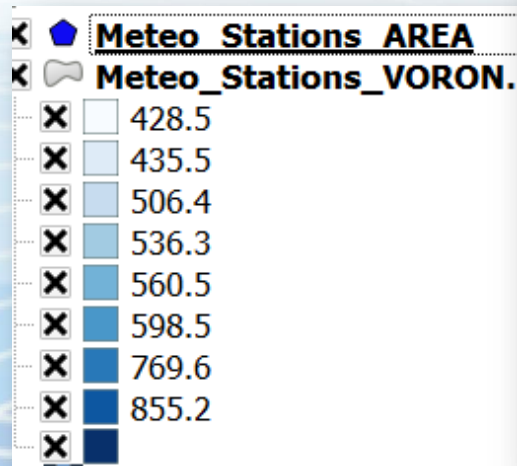
## References:

- Beven, K.J., Kirkby, M.J. (1979) A physically-based variable contributing area model of basin hydrology. Hydrology Science Bulletin, 24, 43-69..
- Montgomery D. R., Dietrich, W. E. (1994) A physically based model for the topographic control on shallow landsliding. Water Resources Research, 30, 1153-1171.

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# Mean annual Rainfall (mm)

- Location of the Meteorological stations around the pilot implementation area





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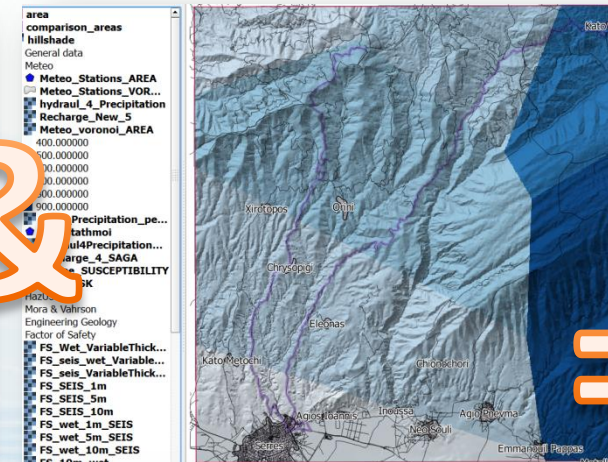
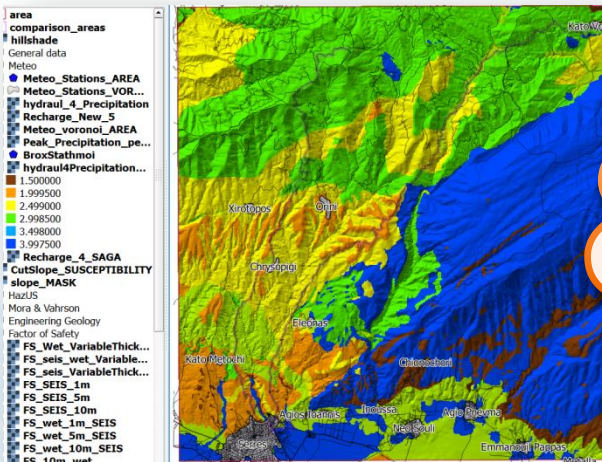


Common borders. Common solutions.

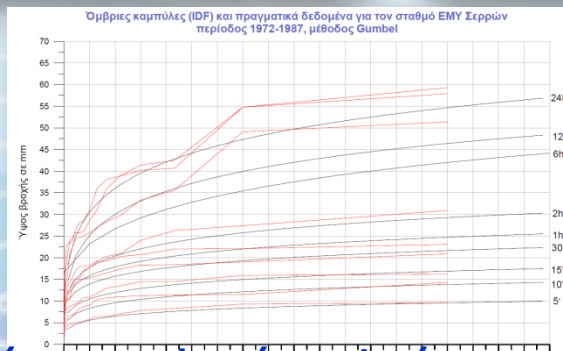
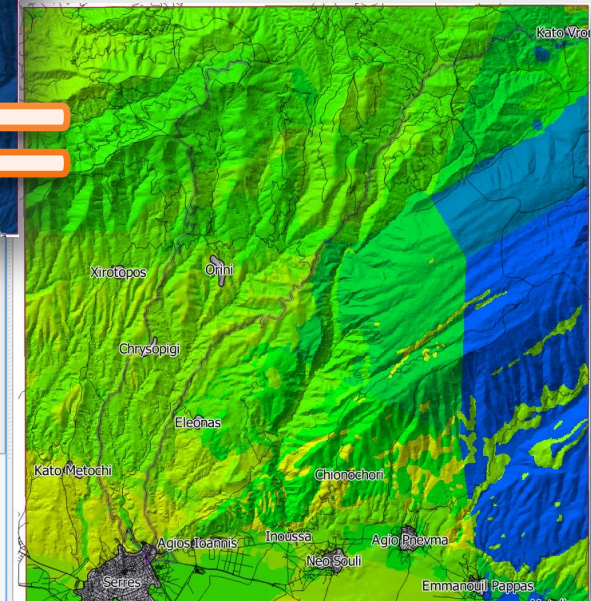
# SAGA “Recharge” (m/hour)

• Effective INFILTRATION

• PEAK Rainfall (m/hour)



• Recharge (m/hour)



• <http://users.auth.gr/vmarios/courses/IDF.pdf>



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# Saturation percentage of sliding slab

The screenshot displays the SAGA GIS interface with the WETNESS tool settings window open. The tool is used for calculating a topographic wetness index (TWI) to estimate the degree of saturation of unconsolidated, permeable materials above impermeable bedrock. The settings window shows various input parameters and options for the calculation.

**WETNESS Tool Settings:**

- Name:** WETNESS
- ID:** 3
- Author:** A. Günther (c) 2012
- Specification:** grid
- Menu:** Terrain Analysis > Slope Stability

**Description:**

This module calculates a topographic wetness index (TWI) following Montgomery & Dietrich (1994) that can be used to estimate the degree of saturation of unconsolidated, permeable materials above (more or less) impermeable bedrock. In contrast to the common TOPMODEL (Beven & Kirkby, 1979) - based TWI, this index differs in such that it considers hydraulic conductivity to be constant in a soil mantle overlying relatively impermeable bedrock. Also, it uses the sine of the slope rather than its tangents, which is more correct and significantly matters for steeper slopes that give rise to landslides. For computation, a slope (in radians) and a catchment area (in m<sup>2</sup>) grid are required. Additionally, information on groundwater recharge (m/hr), material hydraulic conductivity (m/hr), and depth to potential shear plane (m) are required that can be specified either globally or through grids. The module produces a continuous wetness index (-) where cells with WI values > 1 (overland flow) set to 1, and optionally creates a classified WI grid rendering three saturation classes:

- 0: Low moisture (WI smaller 0.1)
- 1: Partially wet (0.1 smaller WI smaller 1)
- 2: Saturation zone (WI larger 1)

**References:**

- Beven, K.J., Kirkby, M.J. (1979) A physically-based variable contributing area model of basin hydrology. *Hydrology Science Bulletin*, 24, 43-69.
- Montgomery, D.R., Dietrich, W.E. (1994) A physically based model for the topographic control on shallow landsliding. *Water Resources Research*, 30, 1153-1171.

**Input Parameters:**

Name	Grid	DEM	Description	Constraints
DEM	Grid	DEM	A DEM	
Min hydraulic conductivity grid (m/hr) (*)	Grid (optional input)	Cmin	A grid representing minimum material hydraulic conductivity (in m/hr)	
Max hydraulic conductivity grid (m/hr) (*)	Grid (optional input)	Cmax	A grid representing maximum material hydraulic conductivity (in m/hr)	

**Options:**

- Min global material conductivity (m/hr): 2.7000000000000002
- Max global material conductivity (m/hr): 2.7000000000000002
- Min global groundwater recharge (m/hr): 0.001
- Max global groundwater recharge (m/hr): 0.001
- Min global material depth (m): 5
- Max global material depth (m): 10
- Parameter sampling runs: 1
- Catchment Area Calculation: Multiple Flow Direction
- Preprocessing: ☐

**Output Maps:**

- 24. WI values: A map showing the continuous wetness index (WI) values, ranging from 0 to 48000.
- 25. WI classes: A map showing the classified wetness index (WI) into three saturation classes (0, 1, 2).

**SAGA GIS Logo:**

**SAGA**  
www.saga-gis.org  
System for Automated Geoscientific Analyses

- Percentage of saturation (m %) needs to be correlated with rainfall (mm) and a mean return period for the rainfall event (if such data exist for the examined region)



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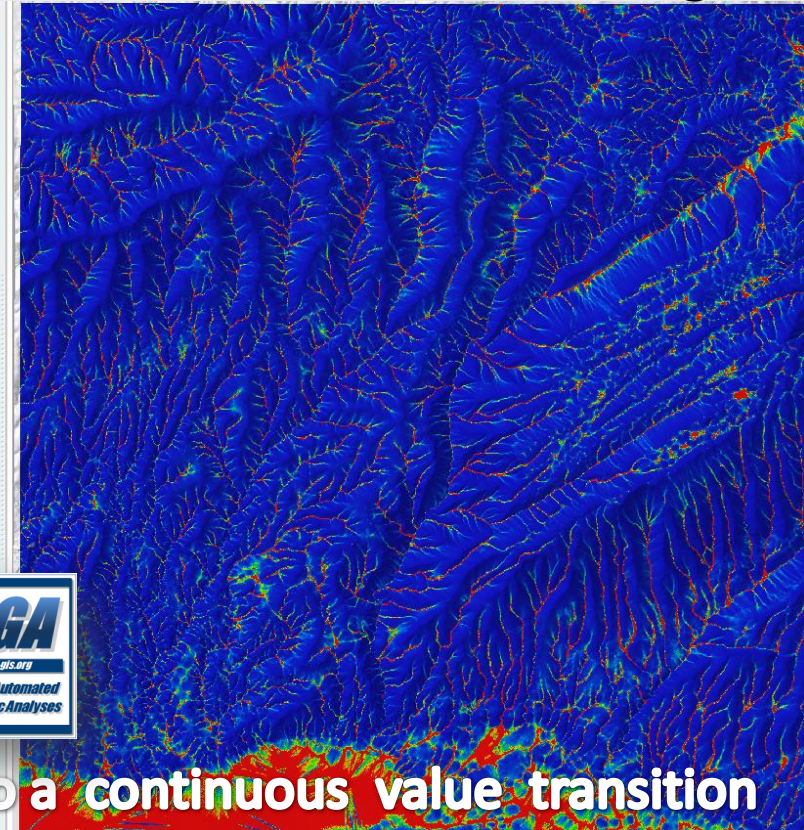
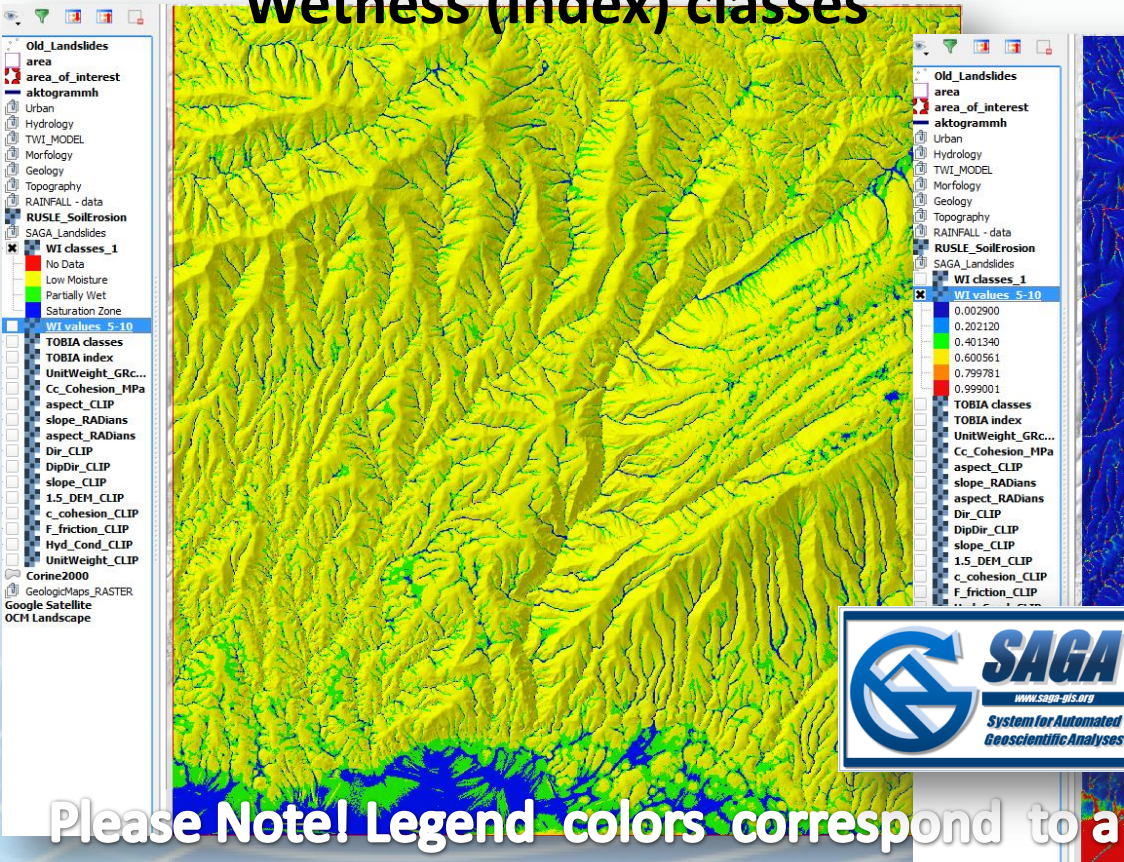


Common borders. Common solutions.

# Saturation percentage of sliding slab

Wetness (Index) classes

Saturation Percentage



Please Note! Legend colors correspond to a continuous value transition

Common borders. Common solutions.

# Landslide Hazard – Seismic/Wet conditions

## Infinite Slope Model (Factor of Safety for a Wet slope)

$$F = \frac{c' + (z \gamma \cos^2 \beta - z \rho a \cos \beta \sin \beta - \gamma_w z_w \cos^2 \beta) \tan \phi'}{z \gamma \sin \beta \cos \beta + z \rho a \cos^2 \beta}$$

$\phi'$ : effective angle of friction of geomaterial ( $^\circ$ )

$c'$ : effective cohesion of geomaterial (kPa),

$\beta$ : slope angle (Deg),

$\rho$ : bulk density ( $\text{Kg/m}^3$ )

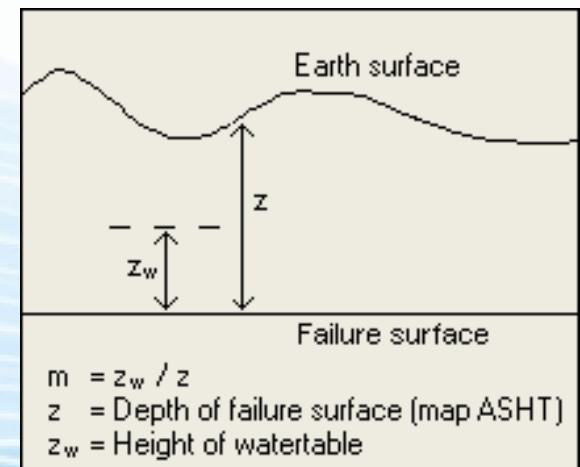
$\gamma$ : specific weight ( $\text{kN/m}^3$ ),

$\gamma_w$ : specific weight of the water ( $\text{kN/m}^3$ ),

$a$ : earthquake acceleration ( $\text{m/sec}^2$ )

**$z$ : normal thickness of the failure slab (m)**

**$m = z_w / z$  % of the water saturated failure slab**



Common borders. Common solutions.

# Landslide Hazard – Seismic/Wet conditions

Landslide Hazard is assessed for the following conditions

- **DRY:** Thickness of failure slab 1, 5 and 10m (three cases)
- **WET:** Thickness of failure slab 1, 5 and 10m (three cases)

## Seismic conditions

- **DRY:** Thickness of failure slab 1, 5 and 10m (three cases)
- **WET:** Thickness of failure slab 1, 5 and 10m (three cases)

Common borders. Common solutions.

# Calculate Factor of Safety– wet–5m thick sliding mass\*

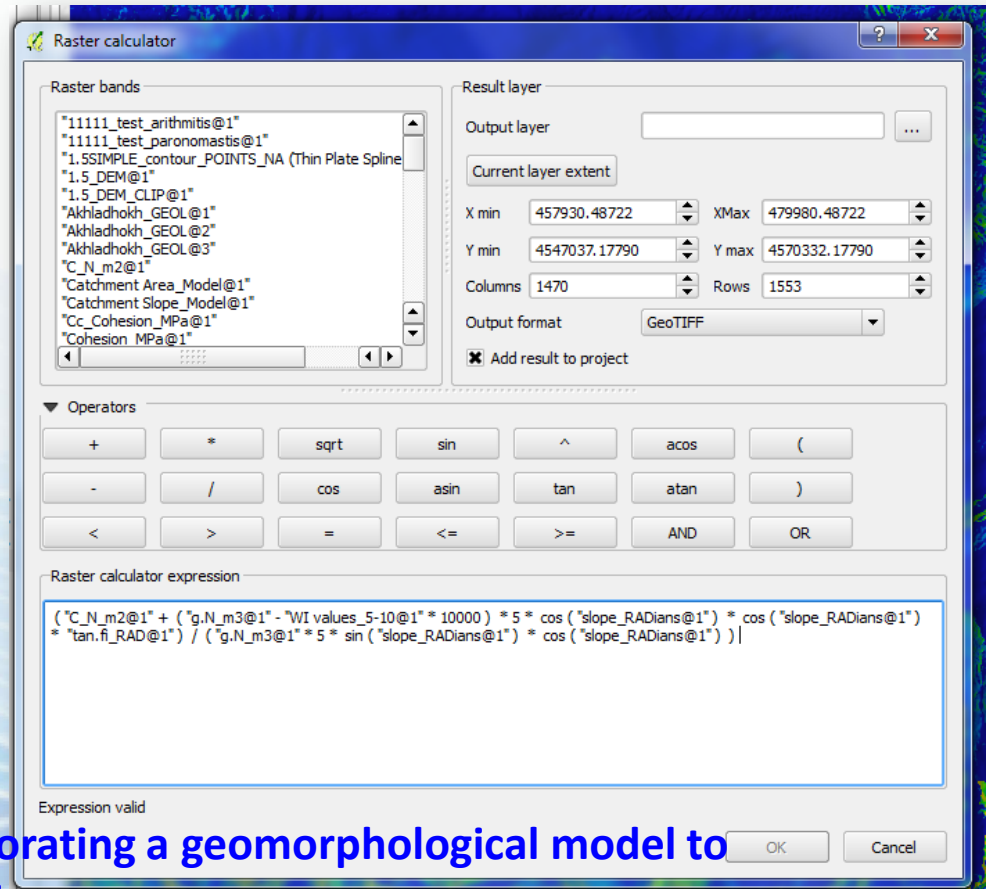
$$F = \frac{c' + (\gamma - m\gamma_w) z \cos^2\beta \tan\phi'}{\gamma z \sin\beta \cos\beta}$$

in which:

- $c'$  = effective cohesion (Pa= N/m<sup>2</sup>).
- $\gamma$  = unit weight of soil (N/m<sup>3</sup>).
- $m$  =  $z_w/z$  (dimensionless).
- $\gamma_w$  = unit weight of water (N/m<sup>3</sup>).
- $z$  = depth of failure surface below the surface (m).
- $z_w$  = height of watertable above failure surface (m).
- $\beta$  = slope surface inclination (°).
- $\phi'$  = effective angle of shearing resistance (°).

...using the information layers  
created previously and the RASTER  
CALCULATOR module in QGIS

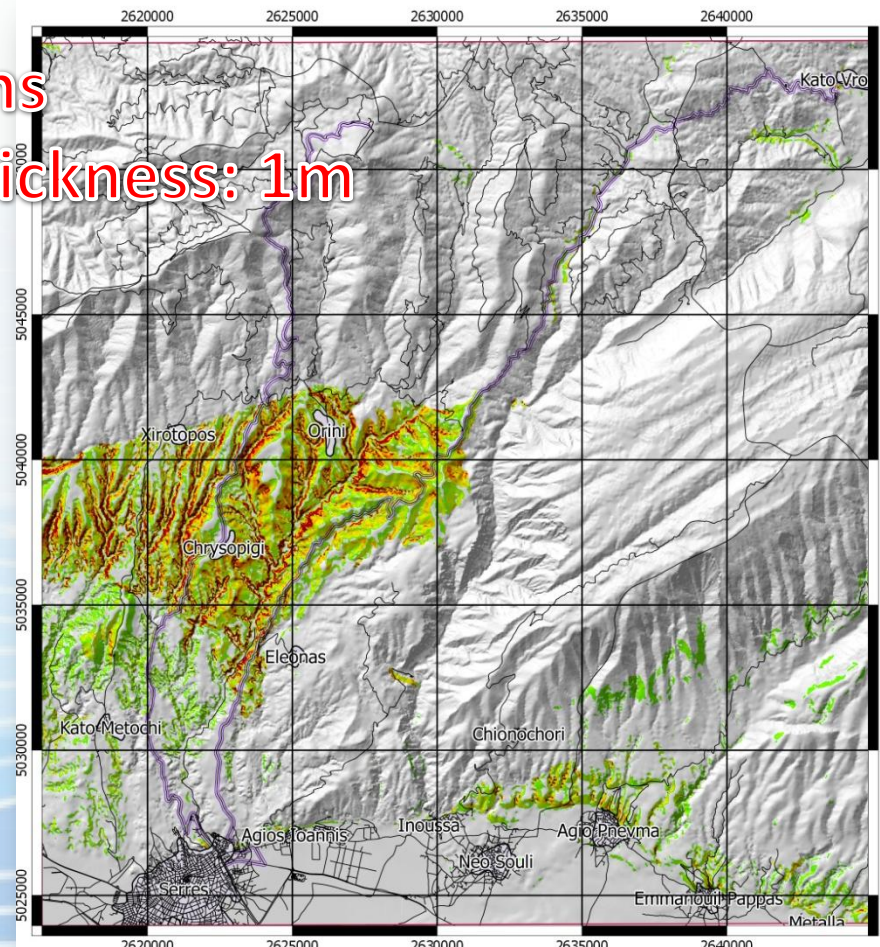
\* We are currently working into incorporating a geomorphological model to calculate the soil thickness in the entire area



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# Factor of Safety – Serres Pilot Implementation Area

**WET conditions**  
**Sliding slab thickness: 1m**



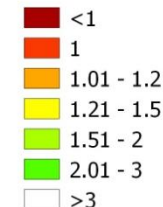
**SciNetNatHaz Project**  
**Black Sea Basin JOP**  
**200713**

**Infinite Slope Model**  
**Factor of Safety map**

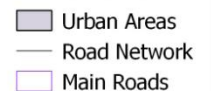
Triggering factor: Precipitation (200 yrs)  
Sliding mass thickness: 1m  
Moisture conditions: Wet

## Legend

Factor of Safety



General data



1 0 1 2 3 4 5 km



Scale 1 : 125000

Coordinate Reference System: HGRS  
(Hellenic Coordinate Reference System '87)



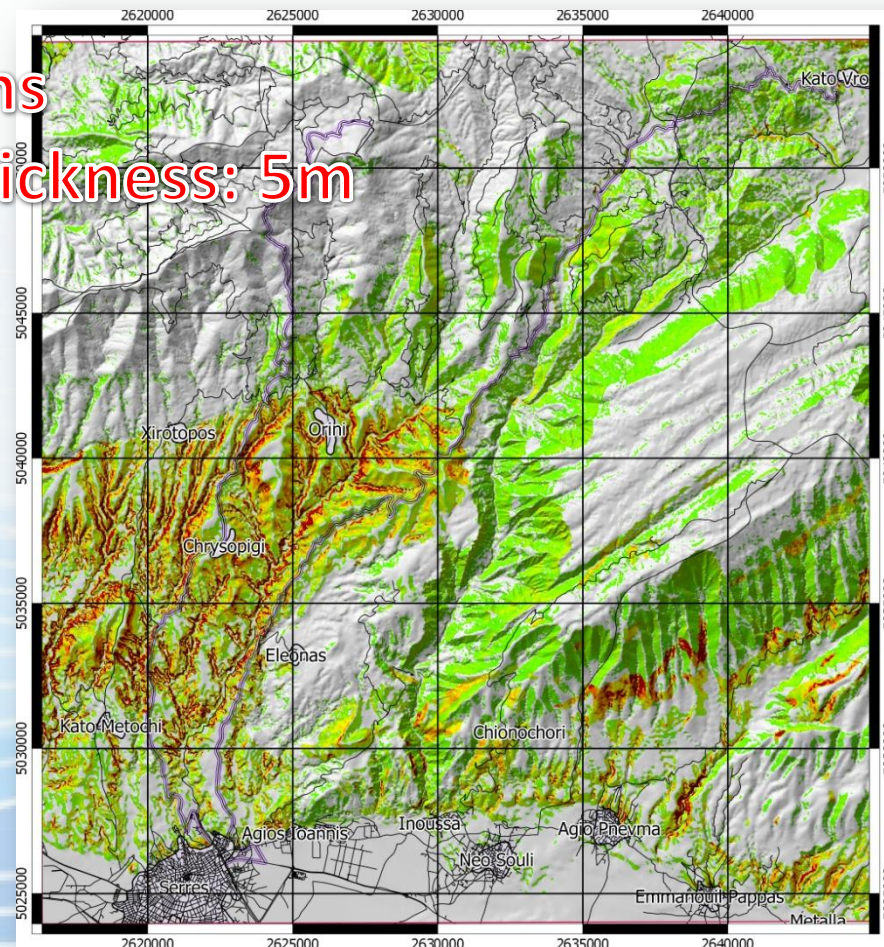
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## Factor of Safety – Serres Pilot Implementation Area

**WET conditions**  
**Sliding slab thickness: 5m**



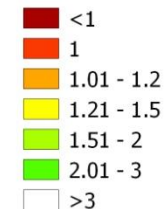
**SciNetNatHaz Project**  
**Black Sea Basin JOP**  
**200713**

### Infinite Slope Model Factor of Safety map

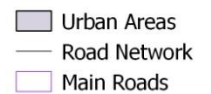
Triggering factor: Precipitation (200 yrs)  
Sliding mass thickness: 5m  
Moisture conditions: Wet

#### Legend

##### Factor of Safety



##### General data



1 0 1 2 3 4 5 km



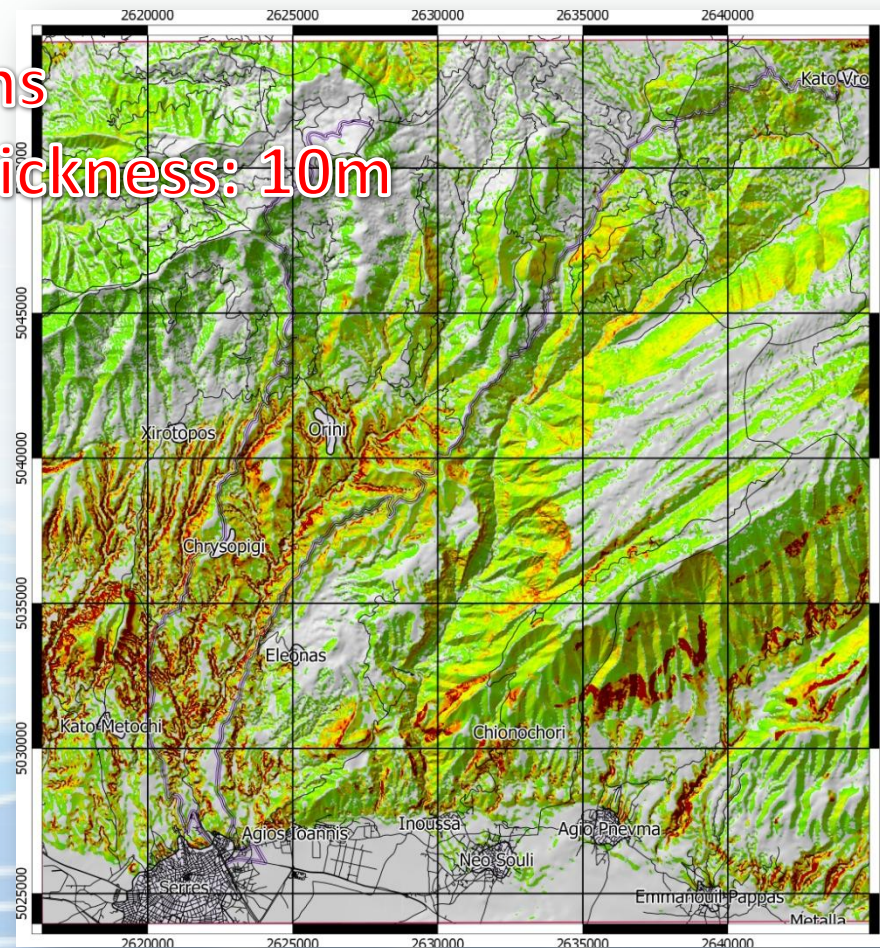
Scale 1 : 125000

Coordinate Reference System: HGRS  
(Hellenic Coordinate Reference System '87)

Common borders. Common solutions.

# Factor of Safety – Serres Pilot Implementation Area

**WET conditions**  
**Sliding slab thickness: 10m**



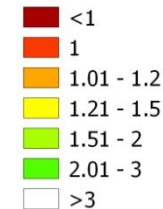
**SciNetNatHaz Project**  
**Black Sea Basin JOP**  
**200713**

## Infinite Slope Model Factor of Safety map

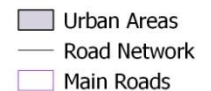
Triggering factor: Precipitation (200 yrs)  
Sliding mass thickness: 10m  
Moisture conditions: Wet

### Legend

#### Factor of Safety



#### General data



1 0 1 2 3 4 5 km



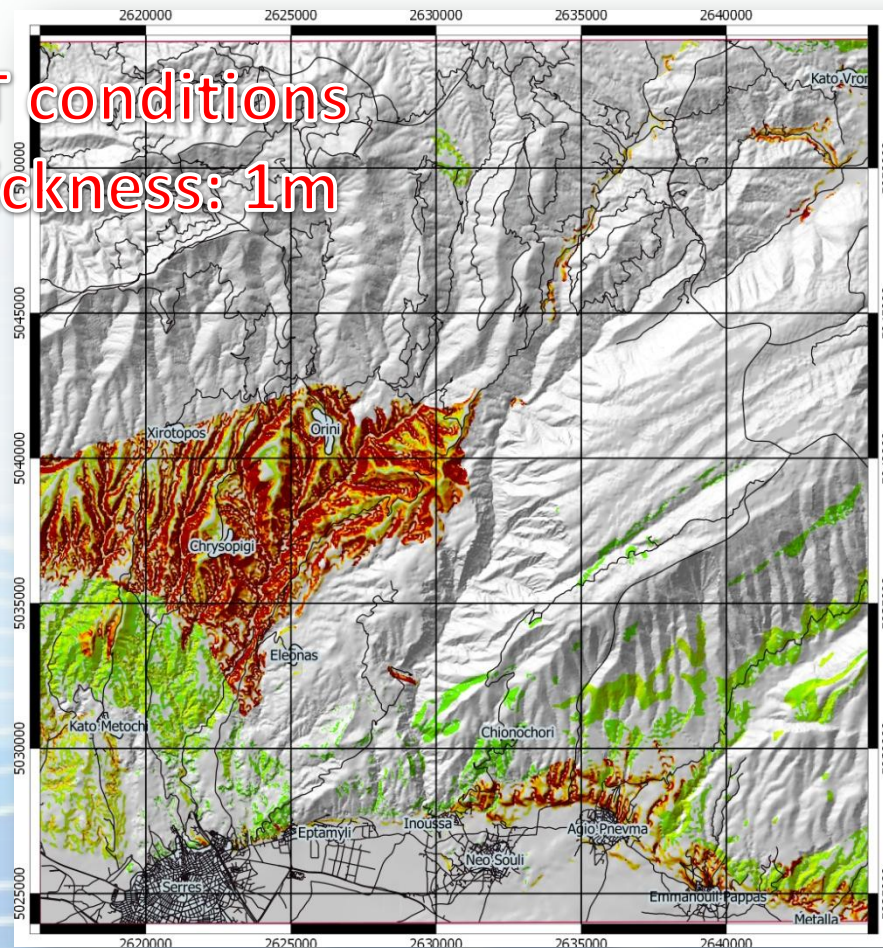
Scale 1 : 125000

Coordinate Reference System: HGRS  
(Hellenic Coordinate Reference System '87)

Common borders. Common solutions.

## Factor of Safety – Serres Pilot Implementation Area

Seismic & WET conditions  
Sliding slab thickness: 1m



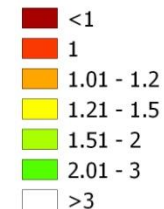
**SciNetNatHaz Project  
Black Sea Basin JOP  
2007-13**

**Infinite Slope Model  
Factor of Safety map**

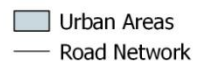
Triggering factors: Earthquake (475 yrs)  
Precipitation (200 yrs)  
Sliding mass thickness: 1m  
Moisture conditions: Wet

### Legend

Factor of Safety



General data



1 0 1 2 3 4 5 km



Scale 1 : 125000

Coordinate Reference System: HGRS  
(Hellenic Geodetic Reference System '87)

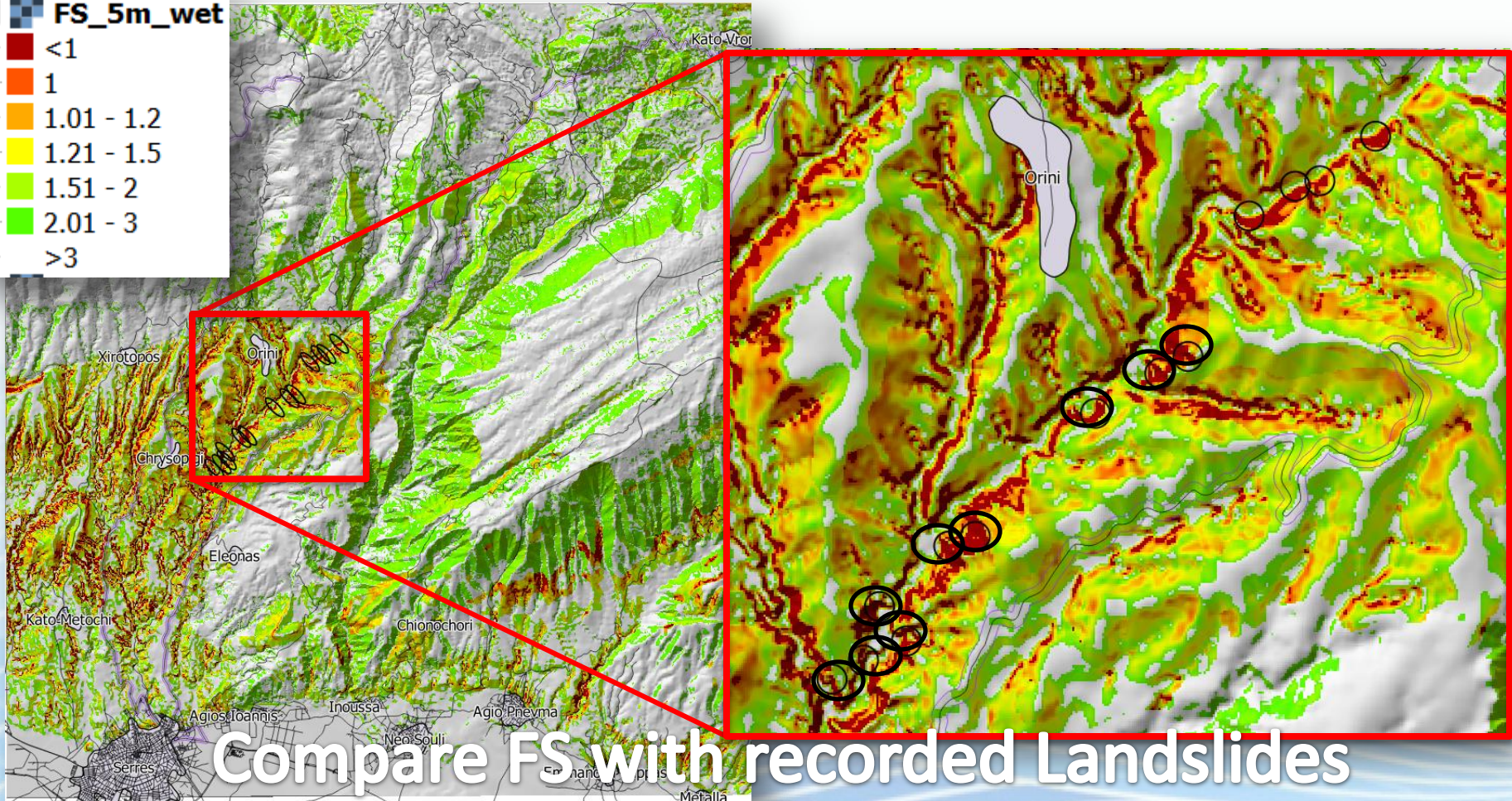
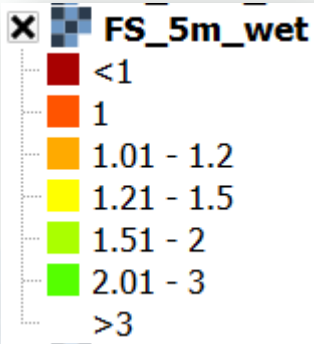


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## EVALUATION of Outputs – wet; $z=5m$



Compare FS with recorded Landslides

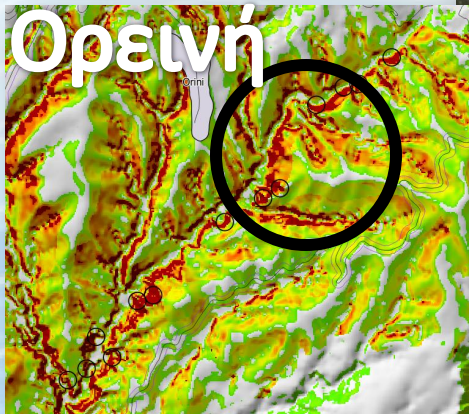


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## EVALUATION of Outputs – Recorded Landslides



Common borders. Common solutions.

## General Conclusions (1/3)

### Landslide **Susceptibility** Assessment, Regional Scale 1:250,000 to 1:25,000 (*static & seismic conditions*)

- FEMA method (**for static conditions**: geologic maps + topography maps + hydraulic conditions) needs improvements (introduction of structure of soils/rocks: dip & dip direction of bedding, schistosity, interface of weathered zone and rockmass or soil over rockmass)
- FEMA method (**for seismic conditions**: geologic maps + topography maps + hydraulic conditions) + Critical Acceleration Index [ $A_c$ /PGA] seems to work fine with local GMPEs and “shallow” landslides

Common borders. Common solutions.

## General Conclusions (2/3)

### Landslide **Hazard** Assessment, Regional Scale 1:250,000 to 1:25,000 (static & seismic conditions)

- **Factor of Safety** method (for **static & seismic conditions**: geologic maps + topography maps + hydraulic conditions (% of sliding slab saturation) + geotechnical parameters ( $\phi'$ ,  $c'$ ) + sliding slab normal thickness). For seismic conditions bulk density ( $\rho$ ) + earthquake acceleration ( $a$ ) are needed. The methodology **works fine** for “shallow” landslides **BUT** needs some improvement regarding the assessment of sliding slab thickness.
- FEMA method (for **seismic conditions**: geologic maps + topography maps + hydraulic conditions) + Critical Acceleration Index [ $A_c/PGA$ ] resulting in the assessment of Permanent Ground Displacements, seems to work fine with local GMPEs and for “shallow type” landslides.

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# Landslide Hazard Assessment

## on Regional Scales:

## Thank You All

## Pilot Implementation in Greece

## for your Attention!

Acknowledgments:

The SciNet NatHaz Project is partially funded by the EU and Hellenic National funds within the context of the

Black Sea Basin Joint Operational Programme 2007-2013

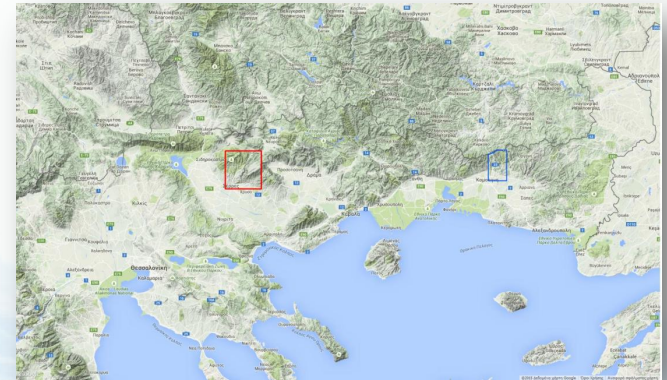
K. Papatheodorou, TEI of Kentriki Makedonia, Hellas  
Nikolaos Klimis, Democritus University of Thrace

Common borders. Common solutions.

## Landslide Susceptibility -Some additional Info

Landslide susceptibility is closely related to low shear strength surfaces as :

- Bedding
- Schistosity
- Joints



Recording of the later (joints), requires field work thus...local scale implementation (costs in time and money)

Information regarding the other two parameters, can be digitized from geologic maps (minimal cost)

Common borders. Common solutions.

# Landslide Susceptibility Mapping

- Create TOBIA index and Classes..
- ..Using the respective SAGA GIS module and..
- ...Slope, Aspect, Dip and DipDirection maps

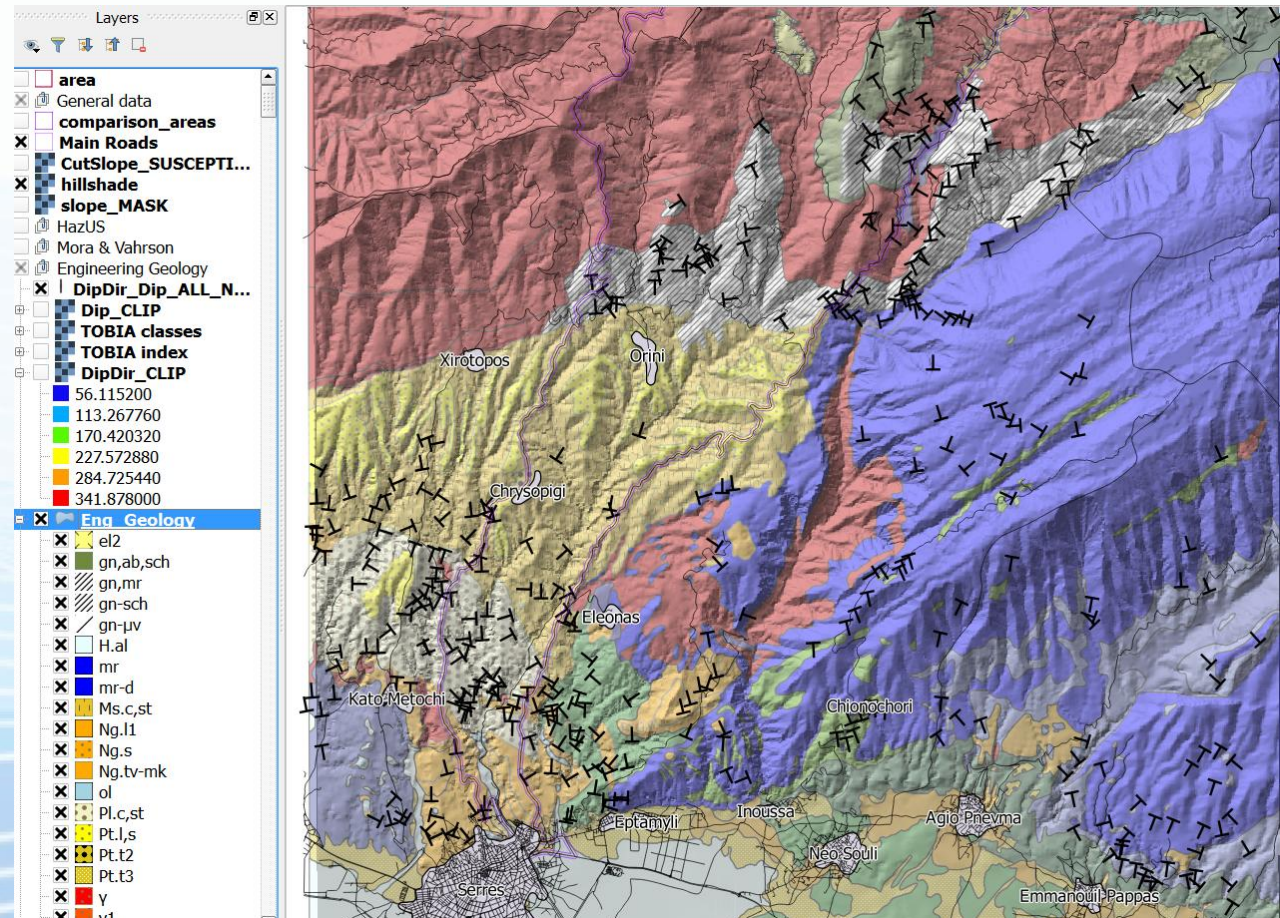


Meentemeyer R. K., Moody A. (2000). Automated mapping of conformity between topographic and geological surfaces. Computers & Geosciences, 26, 815 - 829.

Common borders. Common solutions.

# Landslide Susceptibility Mapping

- Digitize  
**Bedding and  
Schistosity**  
orientation  
(Dip & Dip  
Direction) from  
geologic maps





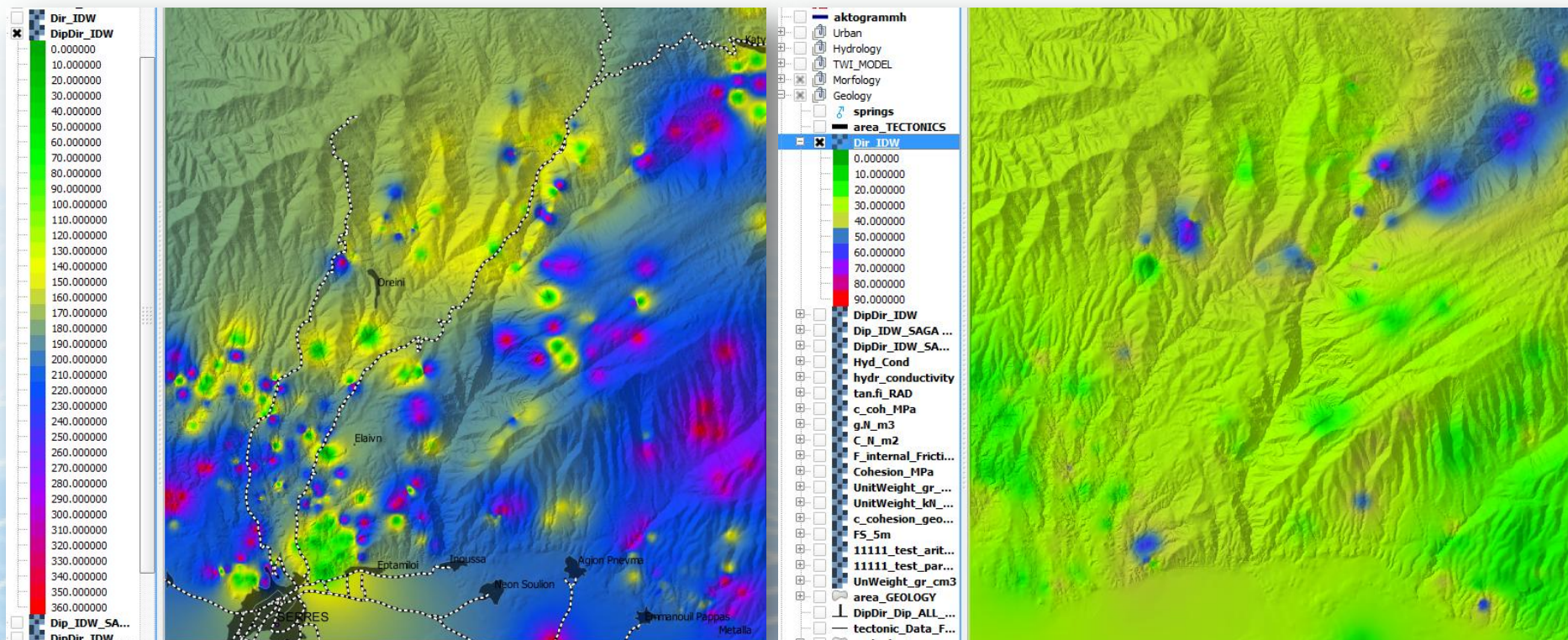
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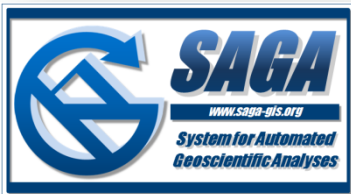
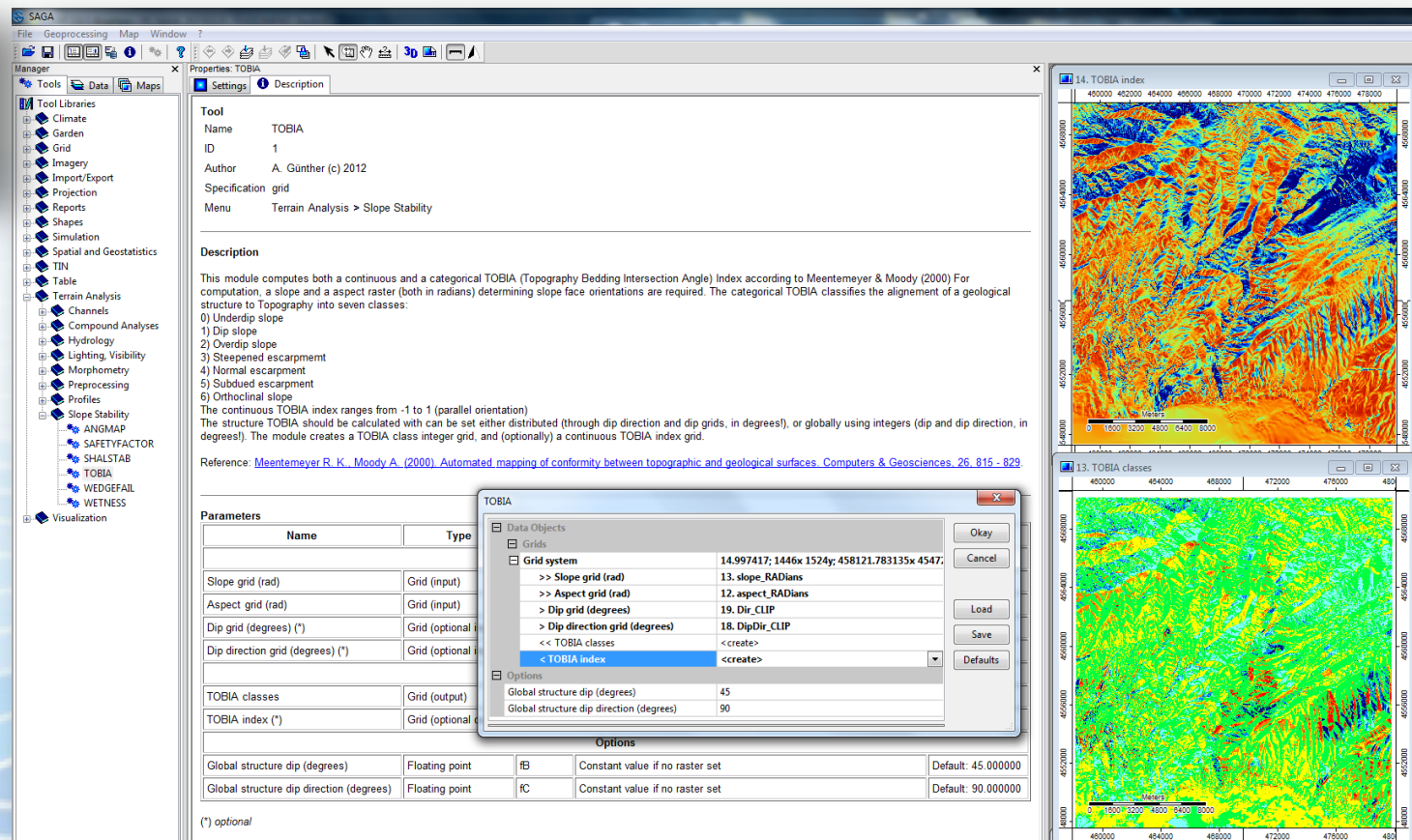
# Landslide Susceptibility Mapping

- Create spatial distribution maps of each parameter using the IDW method (does not exceed minimum-maximum value limits)



Common borders. Common solutions.

# Use SAGA “TOBIA” module to ....

The screenshot displays the SAGA GIS software interface. On the left is the 'Tool Libraries' panel with a tree view showing various processing tools. The main window is titled 'Properties: TOBIA' and contains a 'Description' tab. Below this is a 'Parameters' table with input and output fields. A 'TOBIA' dialog box is open in the foreground, showing a list of data objects and options for the calculation. On the right side of the interface, two maps are displayed: '14. TOBIA index' and '13. TOBIA classes'. Both maps show a topographic area with color-coded data representing the TOBIA index and classes respectively.

**TOBIA**

**Description**

This module computes both a continuous and a categorical TOBIA (Topography Bedding Intersection Angle) Index according to Meentemeyer & Moody (2000). For computation, a slope and an aspect raster (both in radians) determining slope face orientations are required. The categorical TOBIA classifies the alignment of a geological structure to Topography into seven classes:

- 1) Underdip slope
- 2) Dip slope
- 3) Overdip slope
- 4) Steepened escarpment
- 5) Normal escarpment
- 6) Subdued escarpment
- 7) Orthoclinal slope

The continuous TOBIA index ranges from -1 to 1 (parallel orientation). The structure TOBIA should be calculated with can be set either distributed (through dip direction and dip grids, in degrees!), or globally using integers (dip and dip direction, in degrees!). The module creates a TOBIA class integer grid, and (optionally) a continuous TOBIA index grid.

Reference: [Meentemeyer R. K., Moody A. \(2000\). Automated mapping of conformity between topographic and geological surfaces. Computers & Geosciences, 26, 815 - 829.](#)

**Parameters**

Name	Type
Slope grid (rad)	Grid (input)
Aspect grid (rad)	Grid (input)
Dip grid (degrees) (*)	Grid (optional)
Dip direction grid (degrees) (*)	Grid (optional)
TOBIA classes	Grid (output)
TOBIA index (*)	Grid (optional)

**TOBIA**

**Data Objects**

- Grids
  - >> Slope grid (rad) 13. slope\_RADians
  - >> Aspect grid (rad) 12. aspect\_RADians
  - > Dip grid (degrees) 19. Dir\_CLIP
  - > Dip direction grid (degrees) 18. DipDir\_CLIP
  - << TOBIA classes <create>
  - << TOBIA index <create>

**Options**

Global structure dip (degrees)	Global structure dip direction (degrees)
45	90

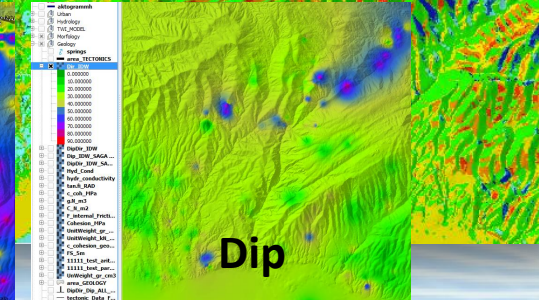
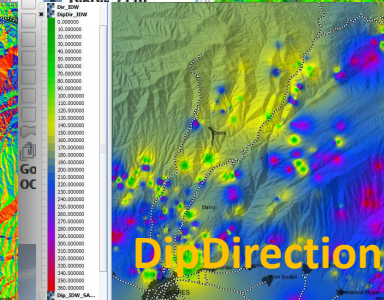
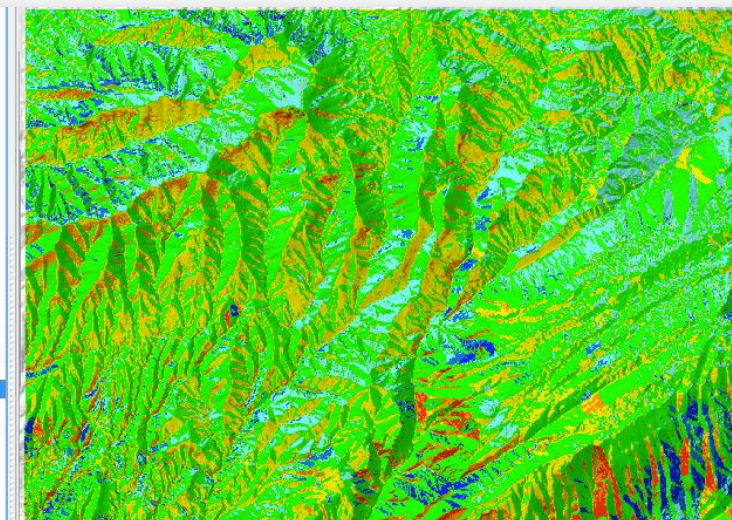
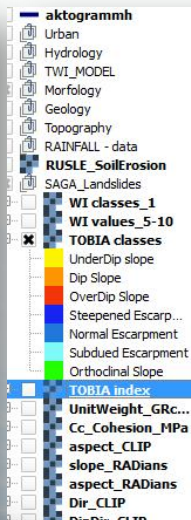
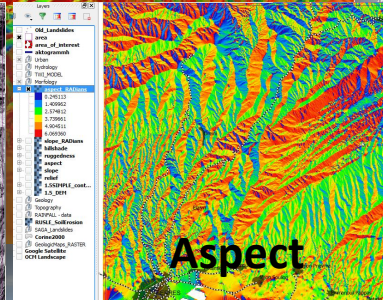
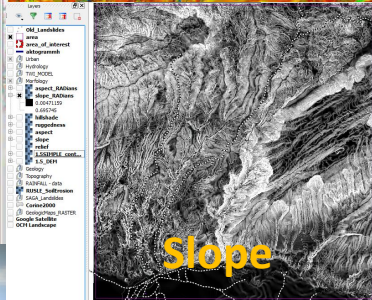
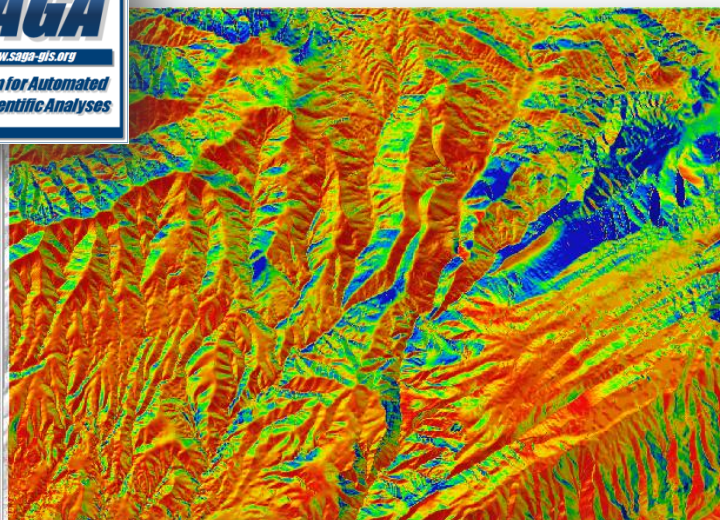
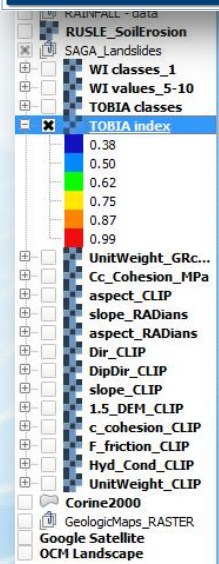
**Options**

Global structure dip (degrees)	Global structure dip direction (degrees)
Floating point	Floating point
Constant value if no raster set	Constant value if no raster set
Default: 45.000000	Default: 90.000000

(\*) optional

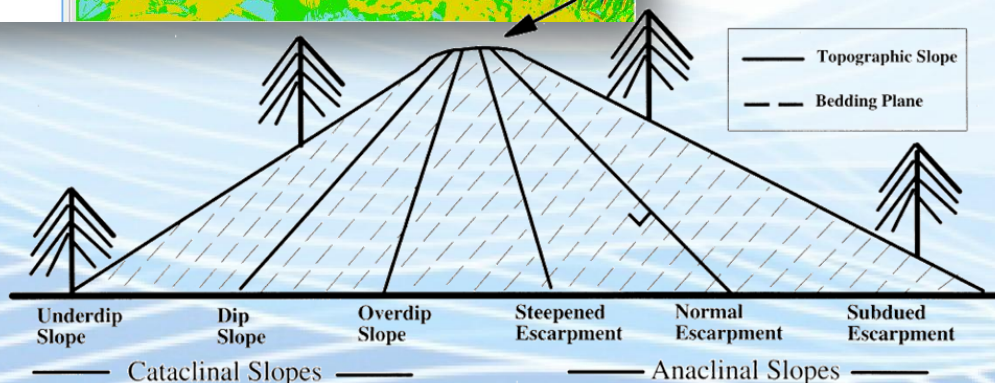
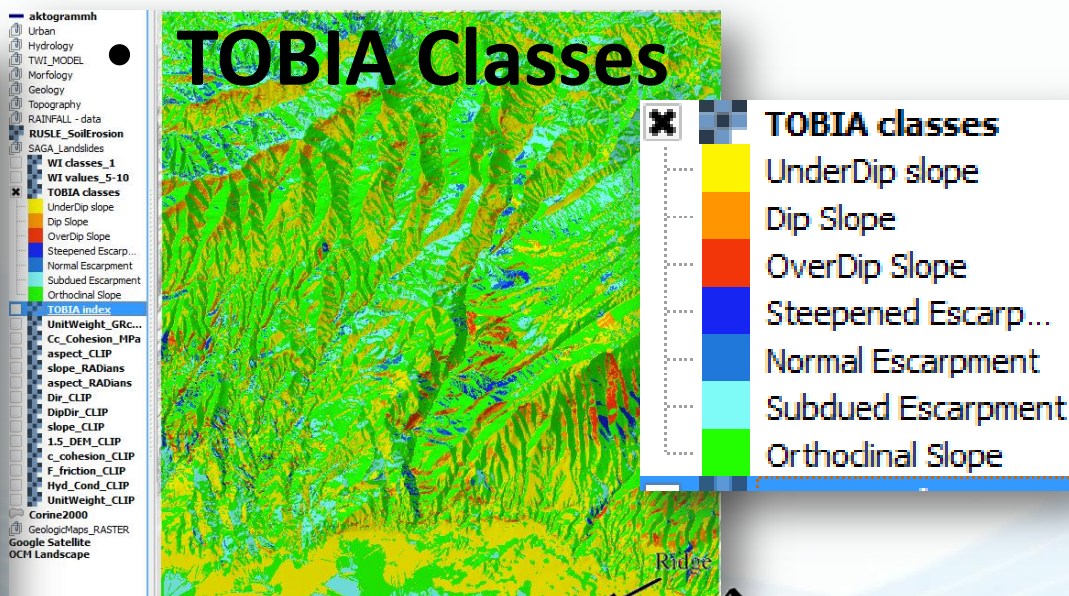
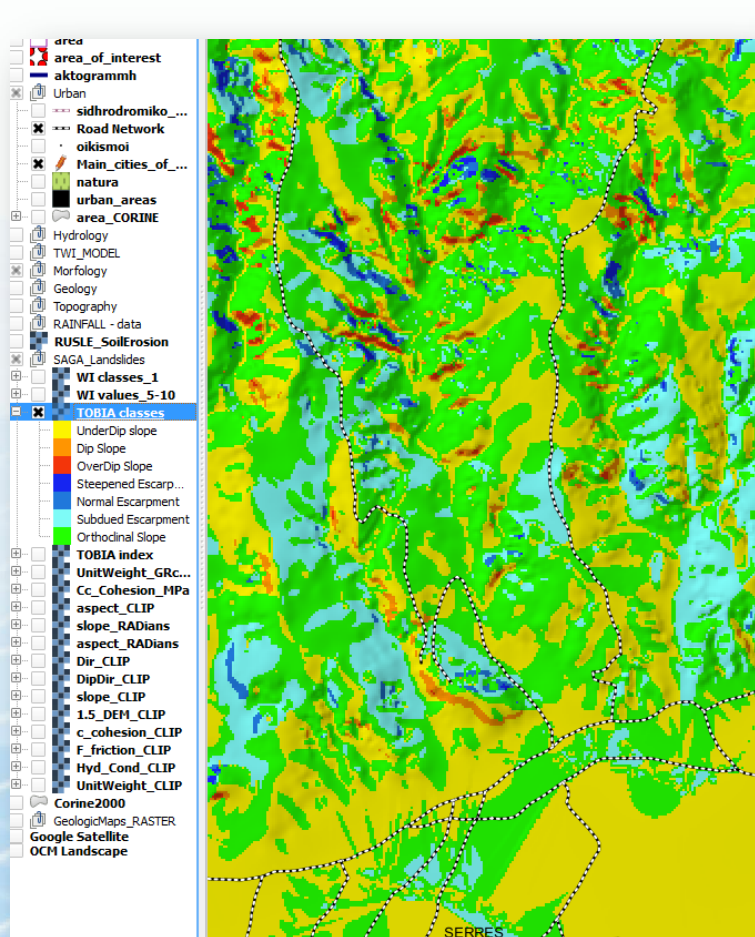
Common borders. Common solutions.

..compare Slope with Dip and Aspect with DipDirection..



Common borders. Common solutions.

..and create TOBIA Index classes..



Common borders. Common solutions.

# Landslide Hazard Assessment

## on Regional Scales:

## Thank You All

## Pilot Implementation in Greece

## for your Attention!

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*SciNetNatHaz project Open Seminars, September-October 2015*