





A Scientific Network for Earthquake, Landslide & Flood Hazard Prevention



SciNetNatHazPrev — STAKEHOLDERS MEETING
NOVEMBER 12-13, 2015, ISTANBUL, TURKEY

VENUE: MAÇKA SOCIAL CENTER, ISTANBUL TECHNICAL UNIVERSITY FOUNDATION

SEISMIC HAZARD ASSESSMENT METHODOLOGIES for TURKEY

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The main objectives of this project is

- to setup common terminology, methodologies and strategies for Earthquake, Landslide and Flood Hazards (ELFH) prevention.
- > To built a WebGIS platform including digital data and information to the scientific community interested in Earthquake, Landslide and Flood Hazards (ELFH)
- > To Implement finally selected (developed or adapted) methodologies to assess hazards on a regional scale and on local scale in selected locations.
- > To provide training with open seminars and workshops

Regional Scale): Marmara Region (Time

Dependent and Time Independent

PSHA)

ISTANBUL

TEKİRDAĞ

Local Scale: (Time Independent -PSHA and DS

SAMSUN



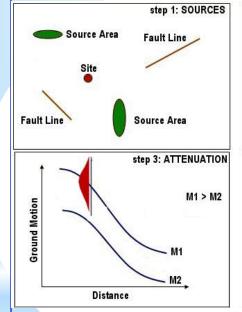


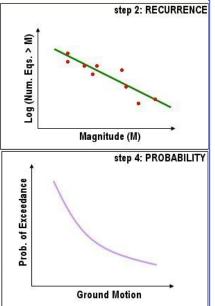




Seismic Hazard Analysis

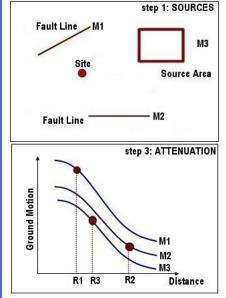
Probabilistic SHA - PSHA

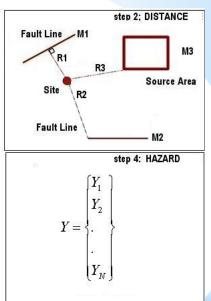




Step of the analysis (1) Definiton of the seismic sources (2) earthquake recurrence characteristics for each source, (3) GMPEs with magnitude and distance, and (4) ground motions for specified probability of exceedance levels (calculated by summing probabilities ovel all the sources, magnitude and distances)

Deterministic SHA - DSHA





Step of the analysis (1) Definition of the seismic sources (2) selection of a source to site distance parameter for each source zone, (3) Selection of the controlling earthquake (GMPEs with magnitude and distance), and (4) Definition of the hazard at site in terms of the ground motions produced at the site by the controlling earthquake.





Dextral faults



Seismic Hazard Assessment: For the Source Model:

MARMARA REGION

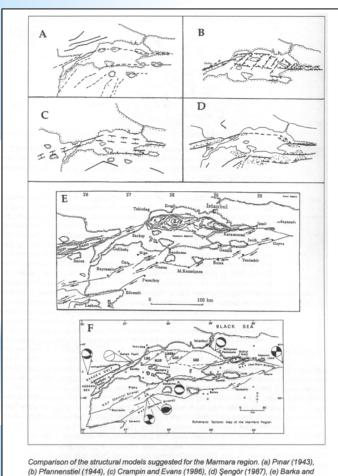
Istanbul

Tectonic Settings

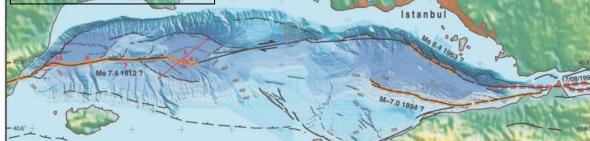
The most prominent models are the "pull apart" model (A) proposed by Armijo et al. (2005) and the "single fault" model (B) proposed by Le Pichon et al. (2003).

Le Pichon et al. (2003)

Armijo et al. (2005)



Kadınsky-Cade (1988), f) Wong et al. (1995), Ergün and Özel (1995).



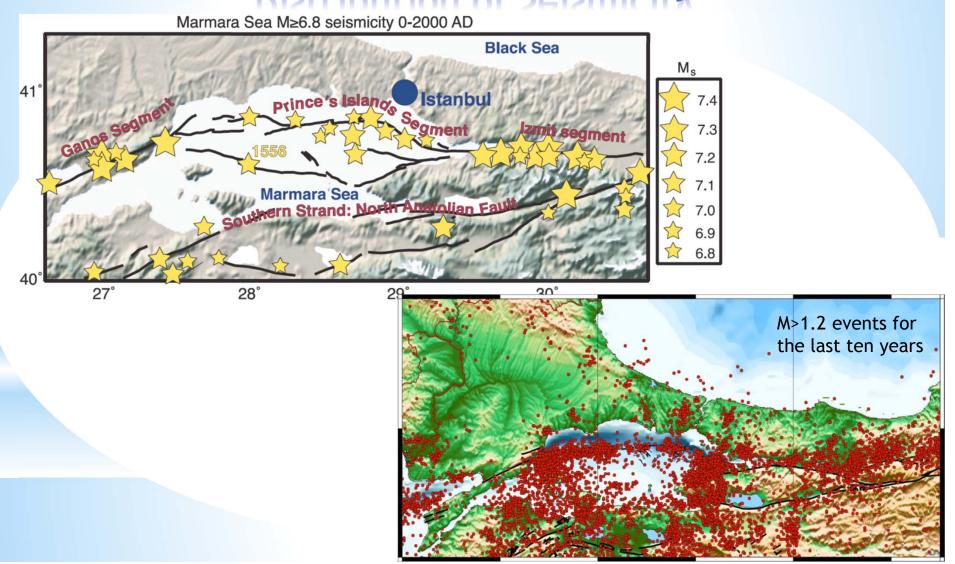






Seismic Hazard Assessment: For the Source Model:

Distribution of Seismicity MARMARA REGION



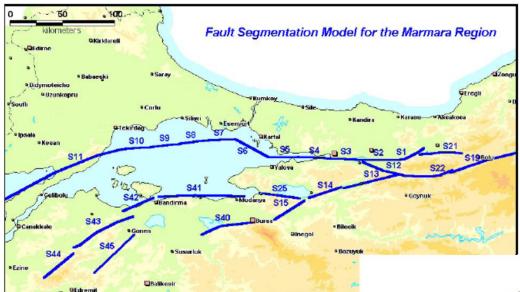






Seismic Hazard Assessment: Two Source Model for Marmara Region:

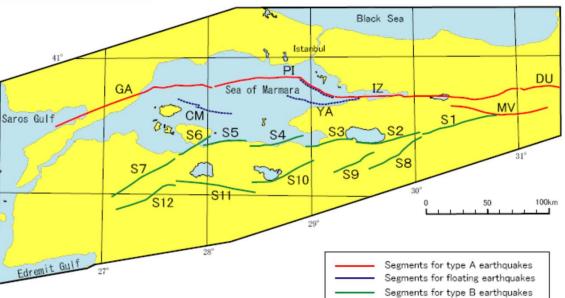
MARMARA REGION



Bogazici University

and Istanbul Metropolitan Municipality

FAULT SEGMENTATION MODELS



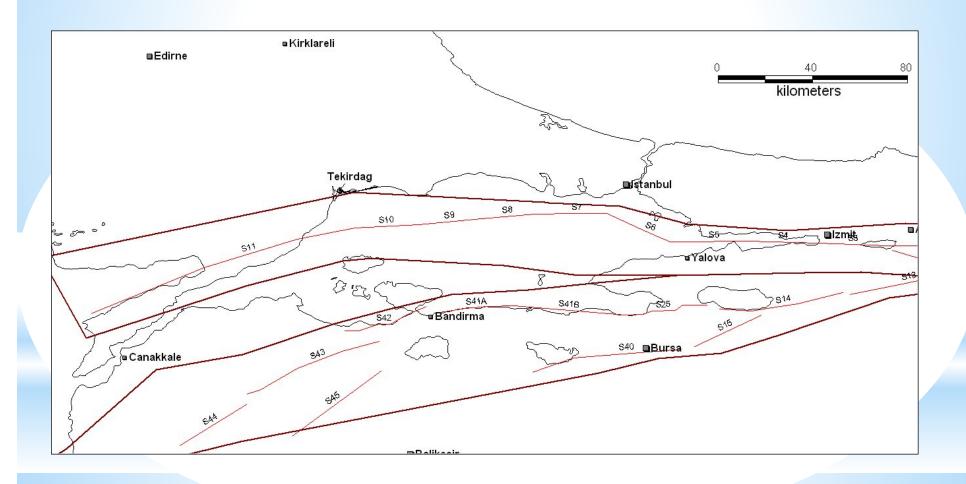






Seismic Hazard Assessment: Two Source Model for Marmara Region:

MARMARA REGION





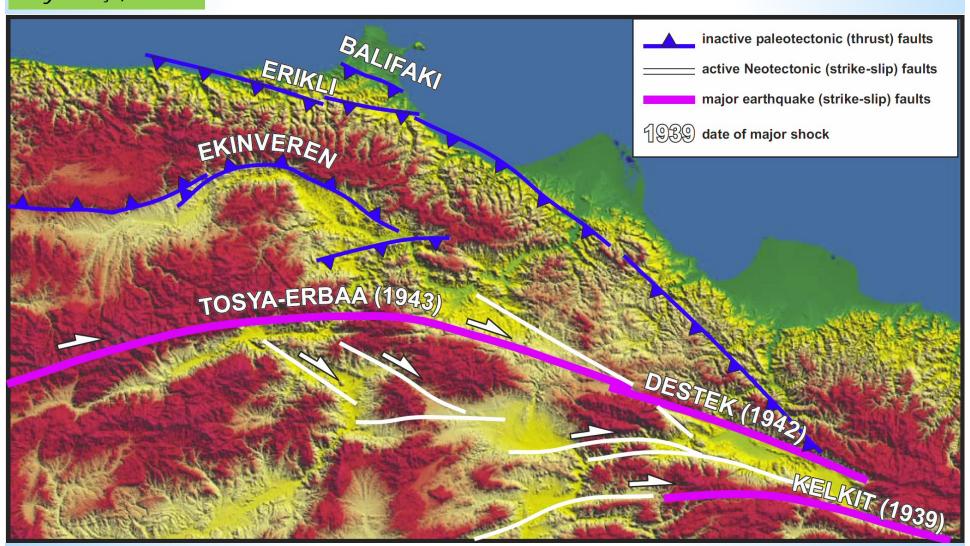




Tectonic Settings

SAMSUN REGION

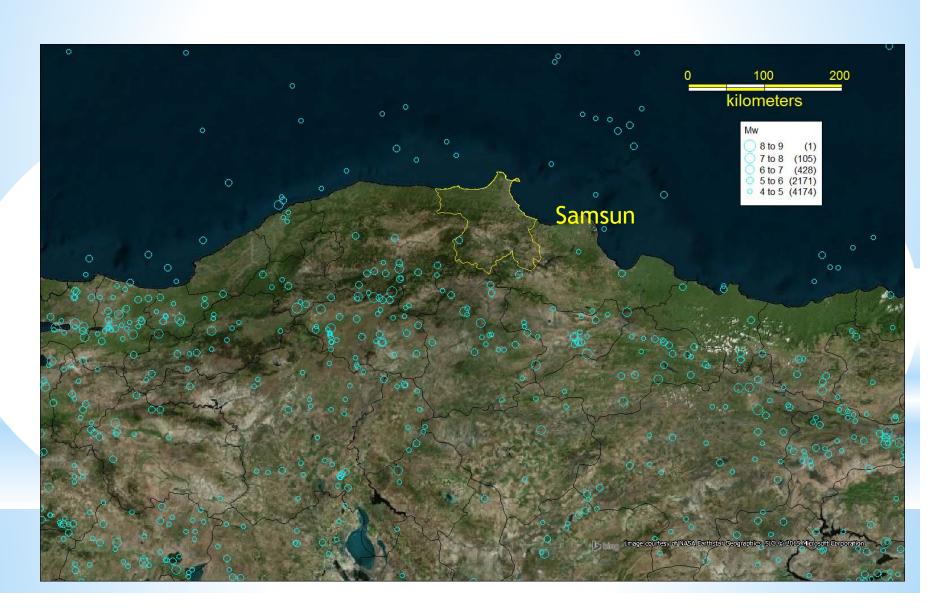
Kaymakçı, 2009











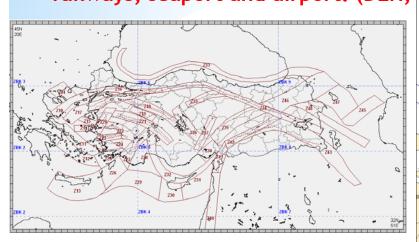


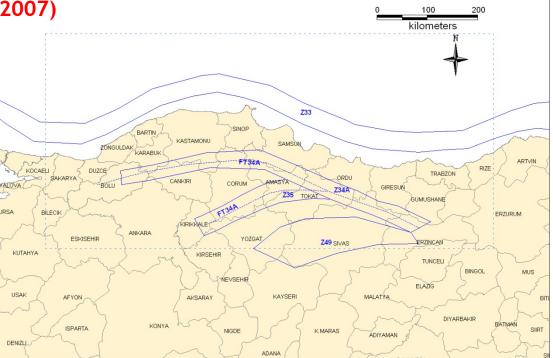




Seismic Hazard Assessment: For the Source Model:

The seismic source zonation model of Turkey developed within the context of a project conducted for the Ministry of Transportation Turkey, aiming the preparation of an earthquake resistant design code for the construction of railways, seaport and airport. (DLH, 2007)





- The earthquakes with magnitude > 6.5 are assumed to take place on the linear zones (Purple line), whereas the smaller magnitude events associated with the same fault are allowed to take place in the surrounding larger areal zone(Green Line).
- In addition to linear and areal source zones, background seismicity zones are defined to model the floating earthquakes that are located outside these distinctly defined source zones and to delineate zones where no significant earthquake has taken place.

* ESTIMATION OF THE SOURCE SEISMICITY PARAMETERS AND PROBABILISTIC MODEL

The earthquake recurrence model for the fault segments

Poisson Model

- ✓ characteristic earthquake recurrence is assumed,
- ✓ probability of occurrence of the characteristic event does not change in time
- ✓ The annual rate is calculated as:

R=1/ mean recurrence interval

Time Dependent (Renewal model)

- ✓ the probability of occurrence of the characteristic event increase s as a function of the time elapsed since the last characteristic event,
- ✓ A lognormal distribution with a coefficient of variation of 0.5 is assumed to represent the earthquake probability density distribution.
- ✓ The annual rate is calculated as:

Reff=-In(1-Pcond) / T



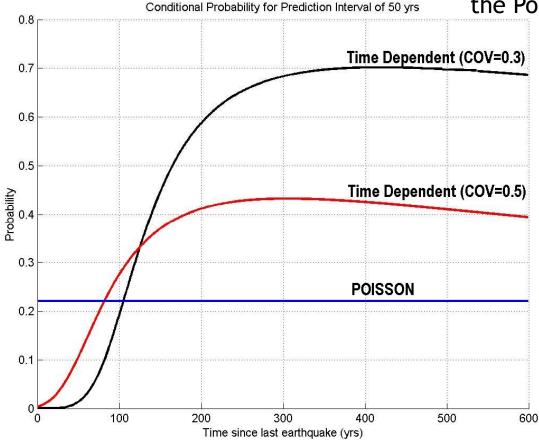




Calculation of the probability For 200 yrs return Period and exposure periods of 50 yrs

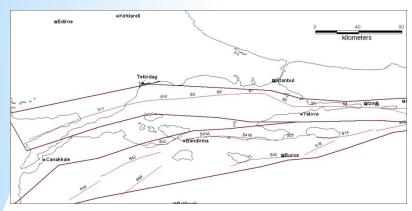
P=1-exp(-(1/yinelenme süresü)*T)						
Yinelenme süresi = 200						
T=50 yıl						
P=1-exp((-1/200)*50))						
P=0.22						

The figure shows that the probability remains constant for the Poisson model and that as the covariance becomes larger, the conditional probability approaches the Poisson probability



* ESTIMATION OF THE SOURCE SEISMICITY PARAMETERS AND PROBABILISTIC MODEL for (
Time-dependent method - the Marmara region)

MARMARA REGION



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12 1967 0.5 250 7.2 47 0.03810 0.00078 0.0040 13 - 0.5 600 7.2 1012 0.17200 0.00377 0.0017 14 - 0.5 600 7.2 1012 0.17200 0.00377 0.0017 15 - 0.5 1000 7.2 1012 0.09790 0.00206 0.0010 19 1944 0.5 250 7.5 70 0.08750 0.00183 0.0040 21 1999 0.5 250 7.2 15 0.00450 0.00099 0.0040 22 1957 0.5 250 7.2 57 0.05750 0.00118 0.0040 25 - 0.5 1000 7.2 1012 0.09790 0.00206 0.0010 40 1855 0.5 1000 7.2 159 0.00092 0.00002 0.0010 41 - 0.5 1	10	-	0.5	200	7.2	1012	0.33250	0.00808	0.0050
13 - 0.5 600 7.2 1012 0.17200 0.00377 0.0017 14 - 0.5 600 7.2 1012 0.17200 0.00377 0.0017 15 - 0.5 1000 7.2 1012 0.09790 0.00206 0.0010 19 1944 0.5 250 7.5 70 0.08750 0.00183 0.0040 21 1999 0.5 250 7.2 15 0.00450 0.00009 0.0040 22 1957 0.5 250 7.2 57 0.05750 0.00118 0.0040 25 - 0.5 1000 7.2 1012 0.09790 0.00206 0.0010 40 1855 0.5 1000 7.2 159 0.00092 0.00002 0.0010 41 - 0.5 1000 7.2 1012 0.09790 0.00206 0.0010 42 - 0.5 1	11	1912	0.5	150	7.5	102	0.44960	0.01194	0.0067
13 - 0.5 600 7.2 1012 0.17200 0.00377 0.0017 14 - 0.5 600 7.2 1012 0.17200 0.00377 0.0017 15 - 0.5 1000 7.2 1012 0.09790 0.00206 0.0010 19 1944 0.5 250 7.5 70 0.08750 0.00183 0.0040 21 1999 0.5 250 7.2 15 0.00450 0.00009 0.0040 22 1957 0.5 250 7.2 57 0.05750 0.00118 0.0040 25 - 0.5 1000 7.2 1012 0.09790 0.00206 0.0010 40 1855 0.5 1000 7.2 159 0.00092 0.00002 0.0010 41 - 0.5 1000 7.2 1012 0.09790 0.00206 0.0010 42 - 0.5 1	12	1967	0.5	250	7.2	47	0.03810	0.00078	0.0040
15 - 0.5 1000 7.2 1012 0.09790 0.00206 0.0010 19 1944 0.5 250 7.5 70 0.08750 0.00183 0.0040 21 1999 0.5 250 7.2 15 0.00450 0.00009 0.0040 22 1957 0.5 250 7.2 57 0.05750 0.00118 0.0040 25 - 0.5 1000 7.2 1012 0.09790 0.00206 0.0010 40 1855 0.5 1000 7.2 159 0.00092 0.00002 0.0010 41 - 0.5 1000 7.2 1012 0.09790 0.00206 0.0010 42 - 0.5 1000 7.2 1012 0.09790 0.00206 0.0010 43 1737 0.5 1000 7.2 277 0.01010 0.00206 0.0010 45 1953 0.5	13	-			7.2	1012			
15 - 0.5 1000 7.2 1012 0.09790 0.00206 0.0010 19 1944 0.5 250 7.5 70 0.08750 0.00183 0.0040 21 1999 0.5 250 7.2 15 0.00450 0.00009 0.0040 22 1957 0.5 250 7.2 57 0.05750 0.00118 0.0040 25 - 0.5 1000 7.2 1012 0.09790 0.00206 0.0010 40 1855 0.5 1000 7.2 159 0.00092 0.00002 0.0010 41 - 0.5 1000 7.2 1012 0.09790 0.00206 0.0010 42 - 0.5 1000 7.2 277 0.01010 0.00206 0.0010 44 - 0.5 1000 7.2 277 0.01010 0.00206 0.0010 45 1953 0.5 <t< td=""><td>14</td><td>-</td><td>0.5</td><td>600</td><td>7.2</td><td>1012</td><td>0.17200</td><td>0.00377</td><td>0.0017</td></t<>	14	-	0.5	600	7.2	1012	0.17200	0.00377	0.0017
19 1944 0.5 250 7.5 70 0.08750 0.00183 0.0040 21 1999 0.5 250 7.2 15 0.00450 0.00009 0.0040 22 1957 0.5 250 7.2 57 0.05750 0.00118 0.0040 25 - 0.5 1000 7.2 1012 0.09790 0.00206 0.0010 40 1855 0.5 1000 7.2 159 0.00092 0.00002 0.0010 41 - 0.5 1000 7.2 1012 0.09790 0.00206 0.0010 42 - 0.5 1000 7.2 1012 0.09790 0.00206 0.0010 43 1737 0.5 1000 7.2 277 0.01010 0.00206 0.0010 44 - 0.5 1000 7.2 1012 0.09790 0.00206 0.0010 45 1953 0.5	15	-	0.5	1000	7.2	1012		0.00206	0.0010
21 1999 0.5 250 7.2 15 0.00450 0.00009 0.0040 22 1957 0.5 250 7.2 57 0.05750 0.00118 0.0040 25 - 0.5 1000 7.2 1012 0.09790 0.00206 0.0010 40 1855 0.5 1000 7.2 159 0.00092 0.00002 0.0010 41 - 0.5 1000 7.2 1012 0.09790 0.00206 0.0010 42 - 0.5 1000 7.2 1012 0.09790 0.00206 0.0010 43 1737 0.5 1000 7.2 277 0.01010 0.00206 0.0010 44 - 0.5 1000 7.2 1012 0.09790 0.00206 0.0010 45 1953 0.5 1000 7.2 61 - - 0.0010 Mmax Beta	_	1944			7.5				
25 - 0.5 1000 7.2 1012 0.09790 0.00206 0.0010 40 1855 0.5 1000 7.2 159 0.00092 0.00002 0.0010 41 - 0.5 1000 7.2 1012 0.09790 0.00206 0.0010 42 - 0.5 1000 7.2 1012 0.09790 0.00206 0.0010 43 1737 0.5 1000 7.2 277 0.01010 0.00020 0.0010 44 - 0.5 1000 7.2 1012 0.09790 0.00206 0.0010 45 1953 0.5 1000 7.2 61 - - 0.0010 BCK - - - 5.0 - 6.9 1.2078 1.767 -	21	1999						0.00009	
25 - 0.5 1000 7.2 1012 0.09790 0.00206 0.0010 40 1855 0.5 1000 7.2 159 0.00092 0.00002 0.0010 41 - 0.5 1000 7.2 1012 0.09790 0.00206 0.0010 42 - 0.5 1000 7.2 1012 0.09790 0.00206 0.0010 43 1737 0.5 1000 7.2 277 0.01010 0.00020 0.0010 44 - 0.5 1000 7.2 1012 0.09790 0.00206 0.0010 45 1953 0.5 1000 7.2 61 - - 0.0010 Mmin - Mmax Alpha Beta BCK - - - 5.0 - 6.9 1.2078 1.767 -	22	1957	0.5	250	7.2	57	0.05750	0.00118	0.0040
40 1855 0.5 1000 7.2 159 0.00092 0.00002 0.0010 41 - 0.5 1000 7.2 1012 0.09790 0.00206 0.0010 42 - 0.5 1000 7.2 1012 0.09790 0.00206 0.0010 43 1737 0.5 1000 7.2 277 0.01010 0.00020 0.0010 44 - 0.5 1000 7.2 1012 0.09790 0.00206 0.0010 45 1953 0.5 1000 7.2 61 - - 0.0010 BCK - - - 5.0 - 6.9 1.2078 1.767 - Z16 - - - 5.0 - 6.9 1.2078 1.767 -	25	-		1000	7.2				
41 - 0.5 1000 7.2 1012 0.09790 0.00206 0.0010 42 - 0.5 1000 7.2 1012 0.09790 0.00206 0.0010 43 1737 0.5 1000 7.2 277 0.01010 0.00020 0.0010 44 - 0.5 1000 7.2 1012 0.09790 0.00206 0.0010 45 1953 0.5 1000 7.2 61 - - 0.0010 Mmin - Mmax alpha Beta BCK - - - 5.0 - 6.9 1.2078 1.767 -	-	1855							
42 - 0.5 1000 7.2 1012 0.09790 0.00206 0.0010 43 1737 0.5 1000 7.2 277 0.01010 0.00020 0.0010 44 - 0.5 1000 7.2 1012 0.09790 0.00206 0.0010 45 1953 0.5 1000 7.2 61 - - 0.0010 Mmin - Mmax Beta BCK - - - 5.0 - 6.9 1.2078 1.767 - Z16 - - - 1.2078 1.767 -	-								
43 1737 0.5 1000 7.2 277 0.01010 0.00020 0.0010 44 - 0.5 1000 7.2 1012 0.09790 0.00206 0.0010 45 1953 0.5 1000 7.2 61 - - 0.0010 Mmin - Mmax alpha Beta BCK 5.0 - 6.9 1.2078 1.767 -	-	_							
44 - 0.5 1000 7.2 1012 0.09790 0.00206 0.0010 45 1953 0.5 1000 7.2 61 - - 0.0010 Mmin - Mmax alpha Beta BCK 5.0 - 6.9 1.2078 1.767 -	-	1737							
Mmin - Mmax alpha Beta BCK - - 5.0 - 6.9 1.2078 1.767 -		-	1						
Mmin - Mmax alpha Beta BCK - - 5.0 - 6.9 1.2078 1.767 -	-	1953					-	-	
Mmax alpha Beta	1.5	1755	0.0	1000	,.2	01			0.0010
Z16						alpha	Beta		
		-	-	-	5.0 - 6.9	1.2078	1.767	_	
	\vdash	-	-	_	5.0-6.6	1.5136	2.0954	-	

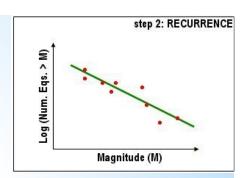
Time dependent

* ESTIMATION OF THE SOURCE SEISMICITY PARAMETERS AND PROBABILISTIC MODEL for time-independent model (Turkey)

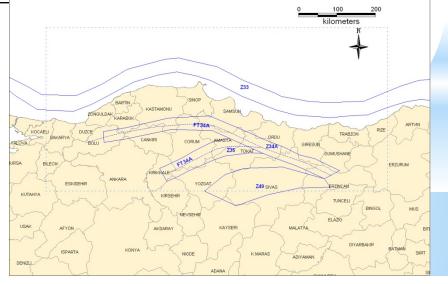
SAMSUN REGION

N is the number of the earthquakes above the magnitude \boldsymbol{M} in a given region and within a given period

"a" and "b" are regression constants.



				_	
	Source Zone No	Associated Fault	a	b	M _{min} - M _{max}
	Z33	Black Sea Fault	3.8	0.9	5.0 - 7.3
	Z34 Outside Zone	North Anatolian Fault	5	0.8	5.0 - 6.7
	Z34 Inside Zone	Zone (NAF)	5		6.8 - 7.9
	Z35 Outside Zone	Alaca Ezine Pazari	3.2	0.8	5.0 - 6.7
	Z35 Inside Zone	Fault			6.8 - 7.9
	Z49	Deliler Fault Zone	4.4	1	5.0 - 7.3
	ZBK1	Background	5.13	1	5.0-6.5



GROUND MOTION PREDICTION EQUATIONS

- * The GMPEs used in the hazard analysis are listed:
 - Akkar and Bommer (2009, rev:2010)
 - Boore and Atkinson (2008)
 - Chiou and Youngs (2008)
 - Campbell and Bozorgnia (2008)
 - Abrahamson and Silva (2008)

Ground Motion Parameters:

- **❖** PGA
- **❖** Sa(T=0.2sn)
- **❖** Sa(T=1.0sn)

Return Periods:

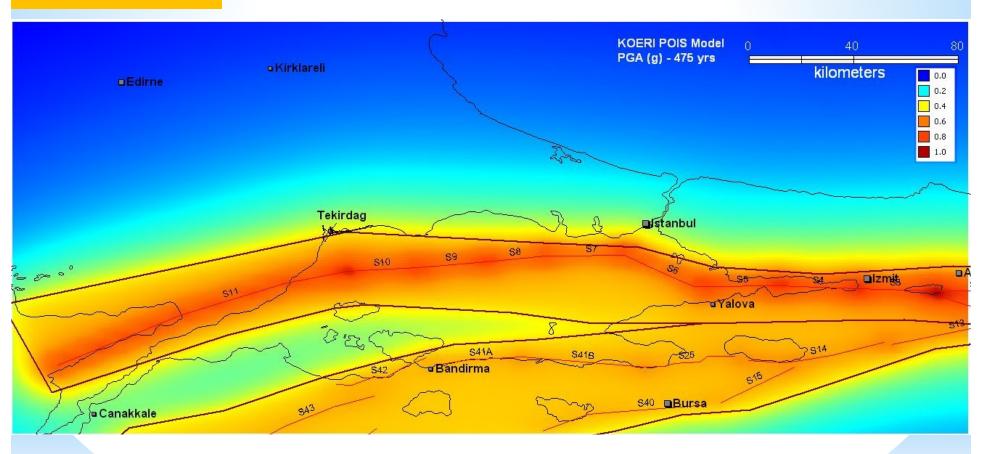
72, 475, 2475 years

Model	Area	Magnitud	Distanc	Period	Site	Mechanis	Compon
		e Range	e Range	Range (s)		m	ent
			(km)				
Abrahamso	California	Mw=5.0-	Rrup =	0.01 - 10.0,	Function	N, R/T, S	GMRot1
n and Silva	, Taiwan	8.0	0 - 200		of Vs30		50
(2008)	and other			PGA,			
	regions			2011			
				PGV			
Boore and	California	Mw=4.27	Rjb = 0	0.01 - 10.0,	Function	N, R, S, U	GMRot1
Atkinson	, Taiwan	– 7.9	- 280	DC A	of Vs30		50
(2008)	and other			PGA,			
	regions			PGV			
Chiou and	California	Mw=4.27	Rrup =	0.01 - 10.0,	Function	N, R, S	GMRot1
Youns	, Taiwan	-7.9	0.2 –	0.01 - 10.0,	of Vs30	N, K, S	50
(2008)	and other	- 7.9	70	PGA,	01 V 830		30
(2008)			70	1 0/1,			
	regions			PGV			
Campbell	California	Mw=4.27	Rrup =	0.01 - 10.0,	Function	N, R, S	GMRot1
and	, Taiwan	- 7.9	0.07 -		of Vs30		50
Bozorgnia	and other		199.27	PGA,			
(2008)	regions						
` ′				PGV			
Akkar and	European	Mw=5.0-	Rrup =	0.05-3.0,	3 classes	N,R/T,S	GMEA
Bommer	and	7.6	0 – 99	PGA,PGV			N
(2010)	Middle						
	East						

ISTANBUL - TEKIRDAG

MARMARA REGION

Time Independent Model NEHRP B/C Based PGA Distribution for %10 Probability of Exceedence in 50 years (475 years return period)



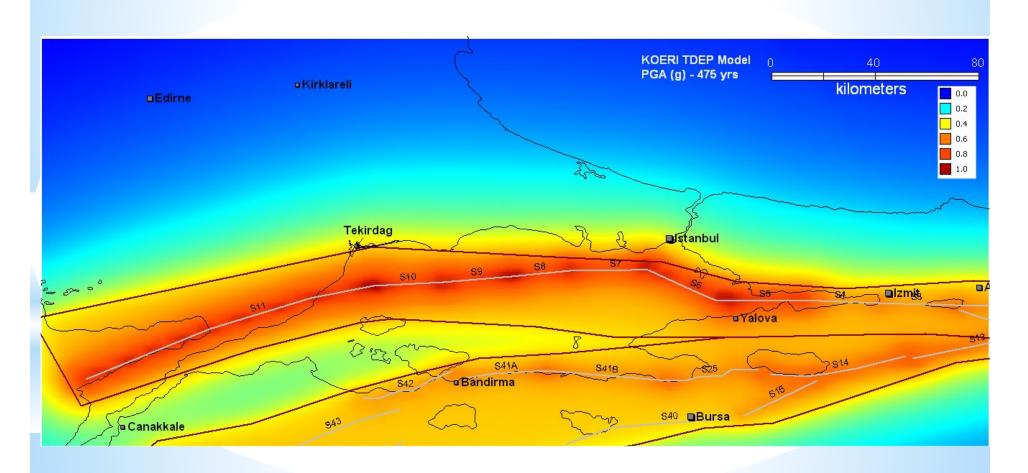








Time Dependent Model NEHRP B/C Based PGA Distribution for %10 Probability of Exceedence in 50 years (475 years return period)



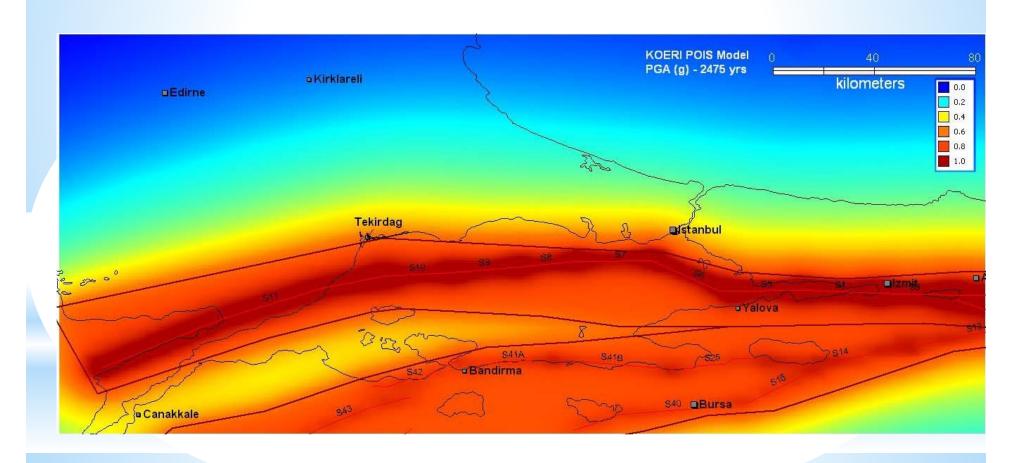








Time Independent Model NEHRP B/C Based PGA Distribution for %2 Probability of Exceedence in 50 years (2475 years return period)



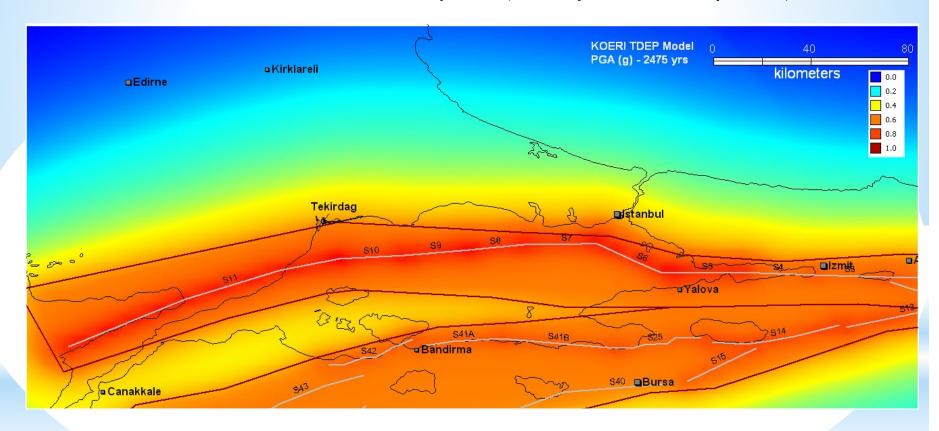








Time Dendent Model NEHRP B/C Based PGA Distribution for %2 Probability of Exceedence in 50 years (2475 years return period)



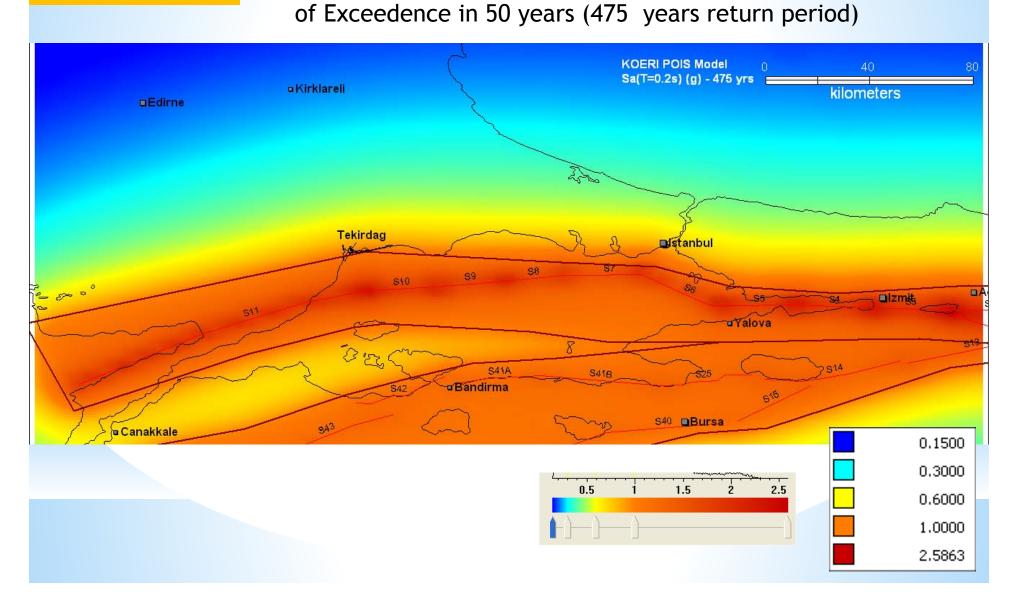








Time Independent Model NEHRP B/C Based Sa(T=0.2s) Distribution for %10 Probability





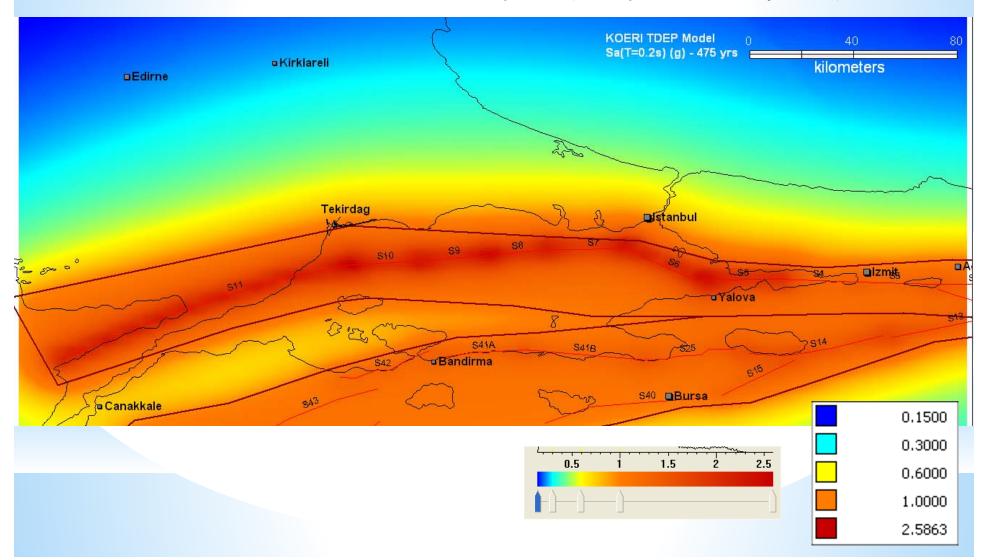






Time Dependent Model NEHRP B/C Based Sa(T=0.2s) Distribution for %10 Probability

of Exceedence in 50 years (475 years return period)



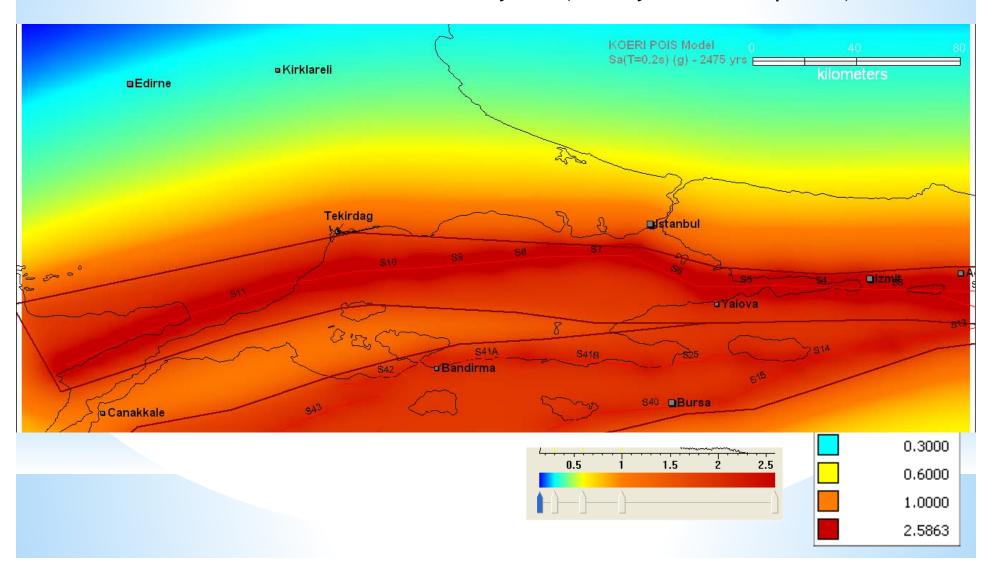








Time Independent Model NEHRP B/C Based Sa(T=0.2s) Distribution for %2 Probability of Exceedence in 50 years (2475 years return period)



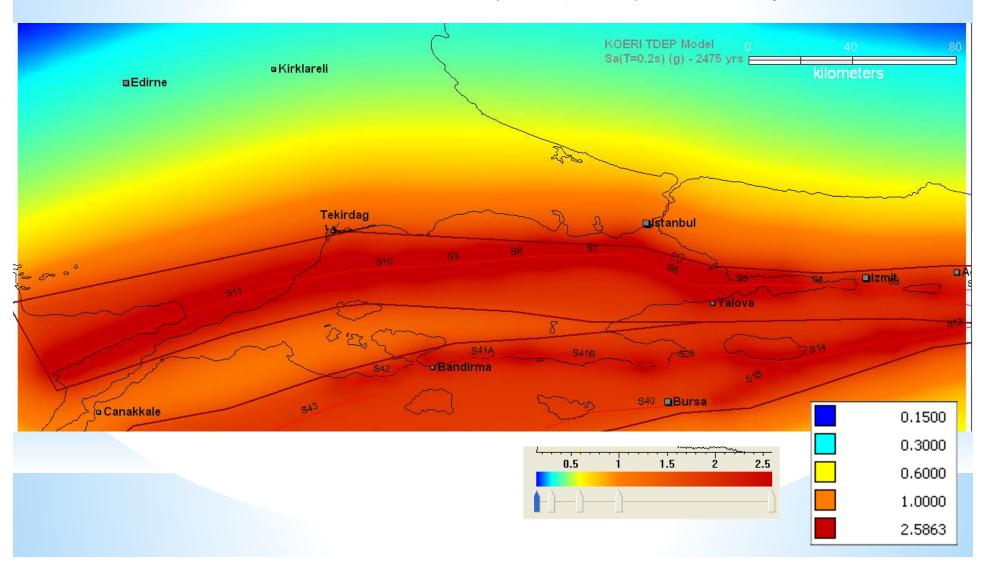








Time Dependent Model NEHRP B/C Based Sa(T=0.2s) Distribution for %2 Probability of Exceedence in 50 years (2475 years return period)





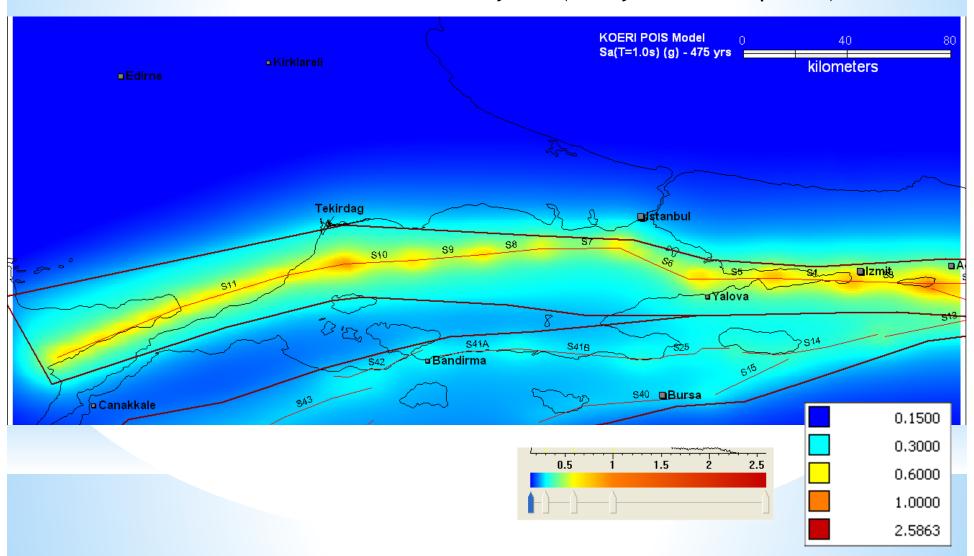






Time Independent Model

NEHRP B/C Based Sa(T=1.0s) Distribution for %10 Probability of Exceedence in 50 years (475 years return period)





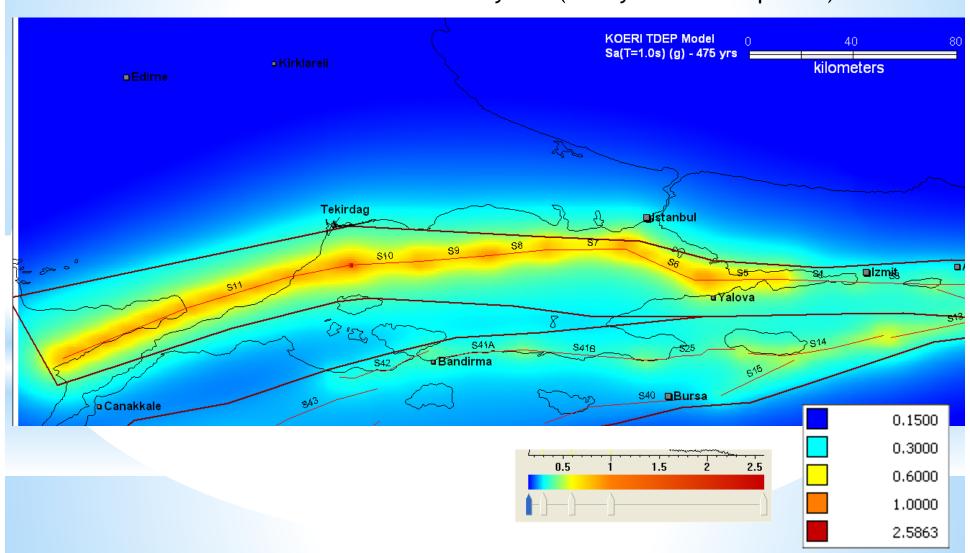






Time Dependent Model NEHRP B/C Based Sa(T=1.0s) Distribution for %10 Probability

of Exceedence in 50 years (475 years return period)





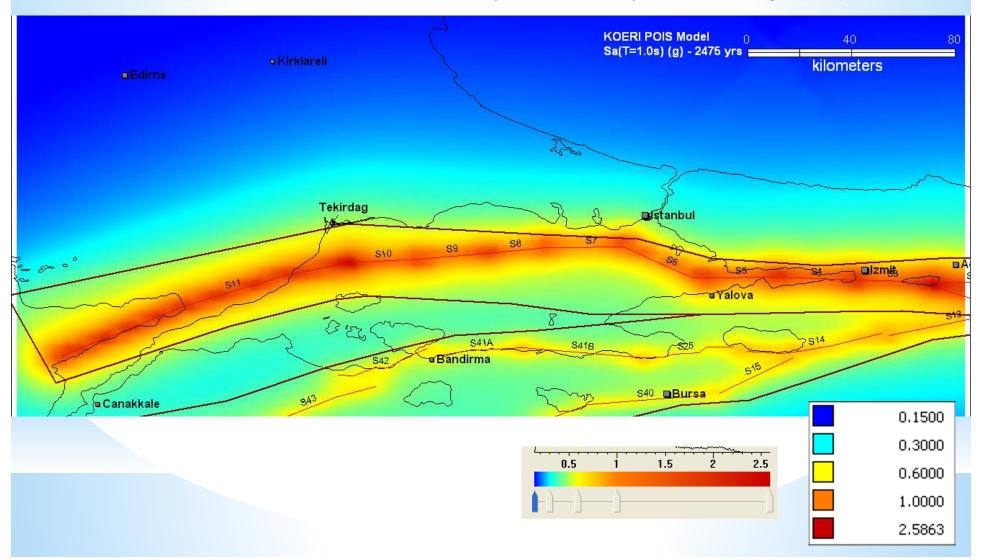






Time Independent Model NEHRP B/C Based Sa(T=1.0s) Distribution for %2 Probability

of Exceedence in 50 years (2475 years return period)





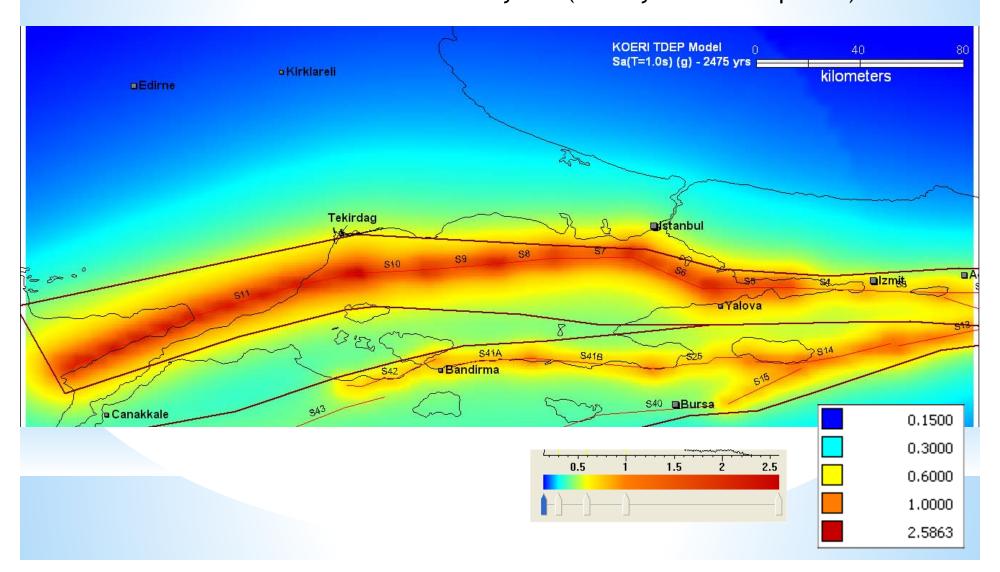






Time Dependent Model ed Sa(T=1.0s) Distribution for %2 Probab

NEHRP B/C Based Sa(T=1.0s) Distribution for %2 Probability of Exceedence in 50 years (2475 years return period)



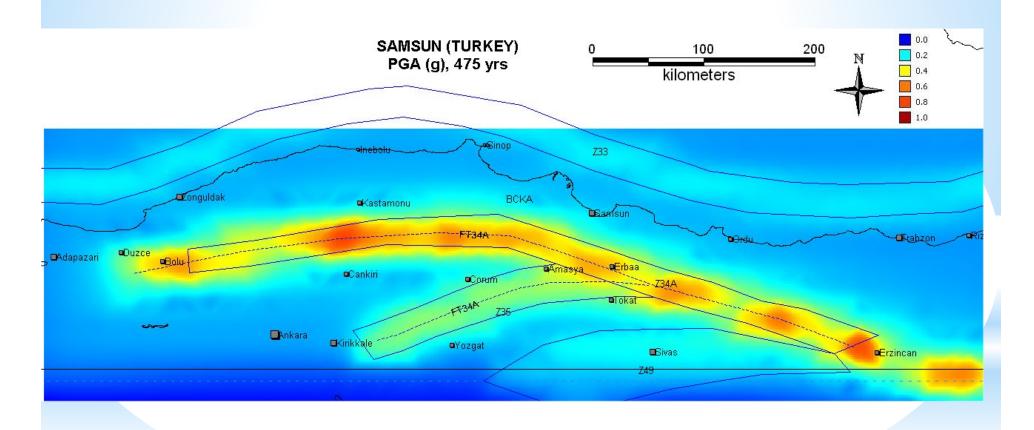








Time Independent Model NEHRP B/C Based PGA Distribution for %10 Probability of Exceedence in 50 years (475 years return period)



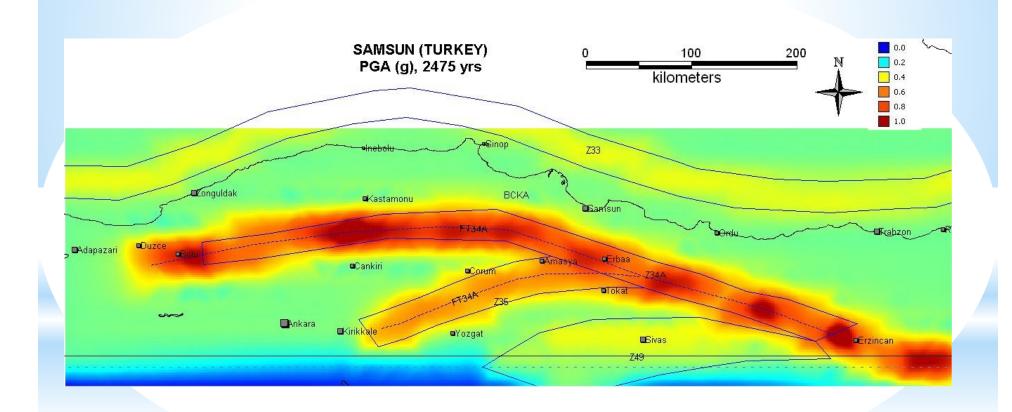








Time Independent Model NEHRP B/C Based PGA Distribution for %2 Probability of Exceedence in 50 years (2475 years return period)



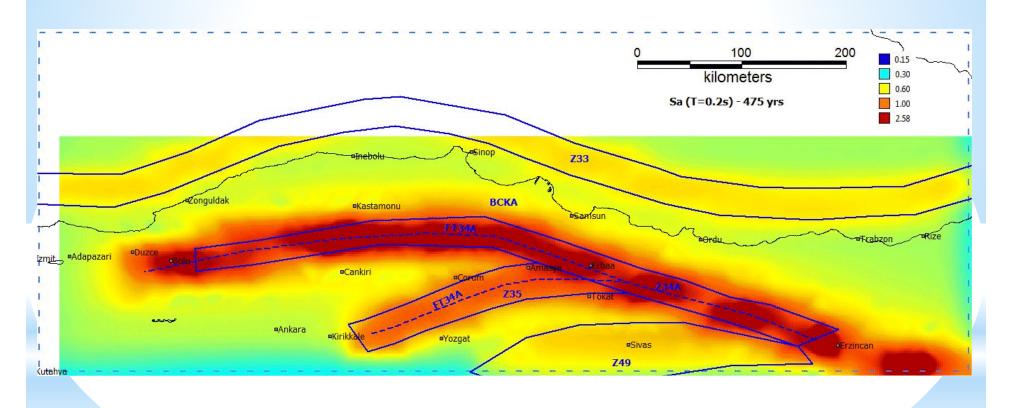








Time Independent Model NEHRP B/C Based Sa(T=0.2s) Distribution for %10 Probability of Exceedence in 50 years (475 years return period)



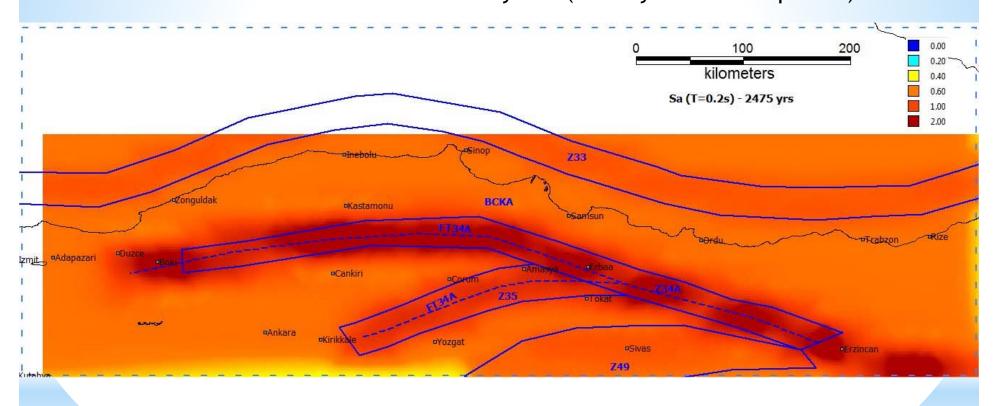








Time Independent Model NEHRP B/C Based Sa(T=0.2s) Distribution for %2 Probability of Exceedence in 50 years (2475 years return period)



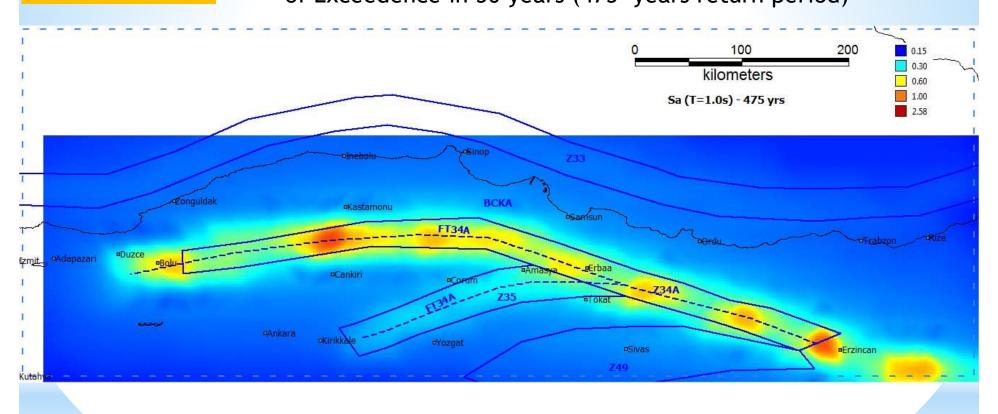








Time Independent Model NEHRP B/C Based Sa(T=1.0s) Distribution for %10 Probability of Exceedence in 50 years (475 years return period)



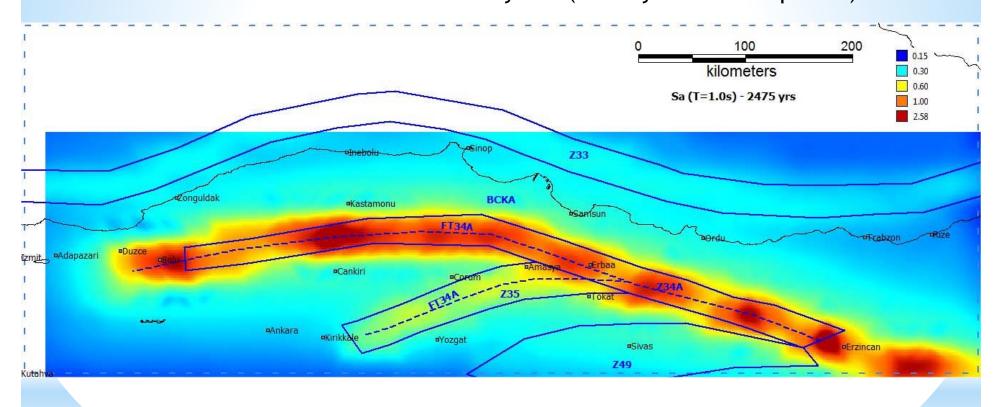








Time Independent Model NEHRP B/C Based Sa(T=1.0s) Distribution for %2 Probability of Exceedence in 50 years (2475 years return period)



Senario Based Study for SAMSUN region Senario 1 - 26 November 1943 LADİK EQ. Ms =7.2; Mw7.6 Sinop KARA DENIZ Inebolu SAMSUN REGION 26 Kasım 1943 LADIK DEPREMI o Daday VI Tosya ϕ_{corum} Cankiri llgaz VI \mathbf{V} 41°50'-Sivas Yozgat .1000 20 40 60 Km V ..500 MAIN SHOCK MAIN SHOCK VII (NOAA) **AFTER SHOCKS** I-VII limit **AMASRA** 41°45'-VIII KAMAN GÜZELCEHISAR

Senario 2: 3 September 1968 BARTIN EQ. Ms=6.6

Senario Based Study for SAMSUN region

SAMSUN REGION

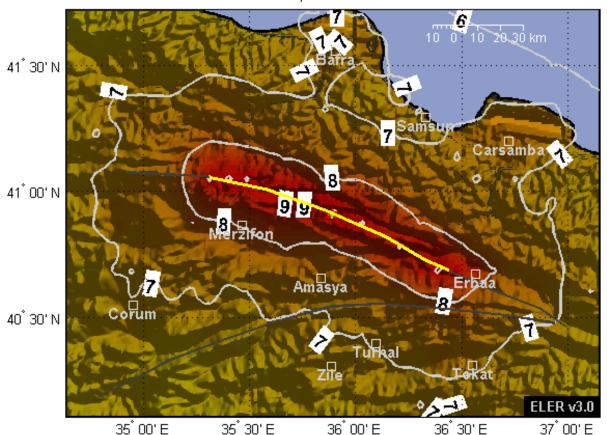
Senario 1 Southern Samsun - Ladik Eq.

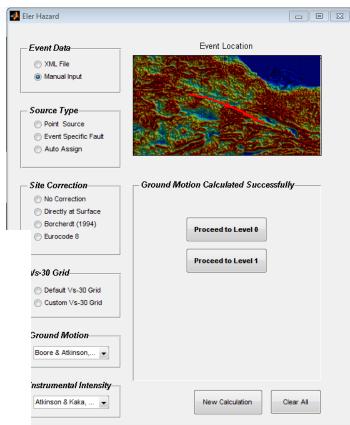
M7.6 - depth 10.0km - Rupture Length = 105

Lat: 40.91

Lon: 35.89

M7.6 Depth= 10 Lat= 40.91 Lon= 35.89 Map of: INTENS

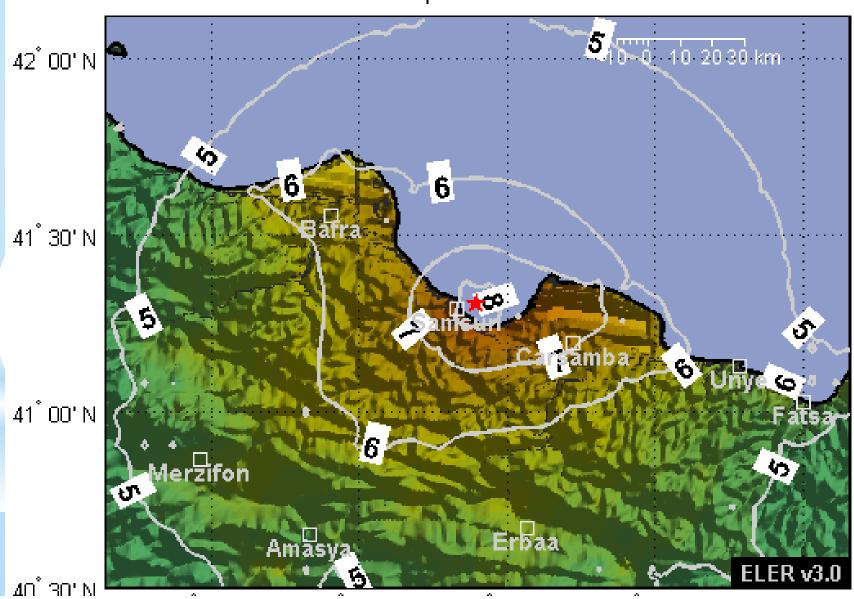




Senario 2 -Bartin Eq. M6.6

Intensity Distribution

M6.6 Depth= 5 Lat= 41.3086 Lon= 36.3998 Map of: INTENS









✓ The grid based PGA result for the return period of 475 years obtained from PSHA analysis was shared in the other work package to use as an input to landslide analysis

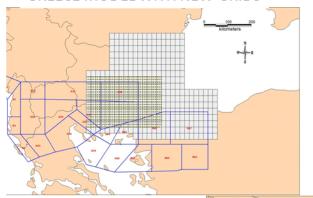
We were generated the grid with 0.25 x 0.25 degree covering all region.

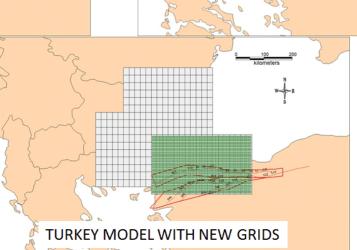
And then, we tried to combine all results for PGA, 475 yrs obtained from PSHA analysis from Greece, Bulgaria, Moldovia, Romania, Ukrain, and Turkey. The PGA for 475 years values obtained from PSHA for Bulgaria, Greece and Turkey were assigned in the middle of the grid.

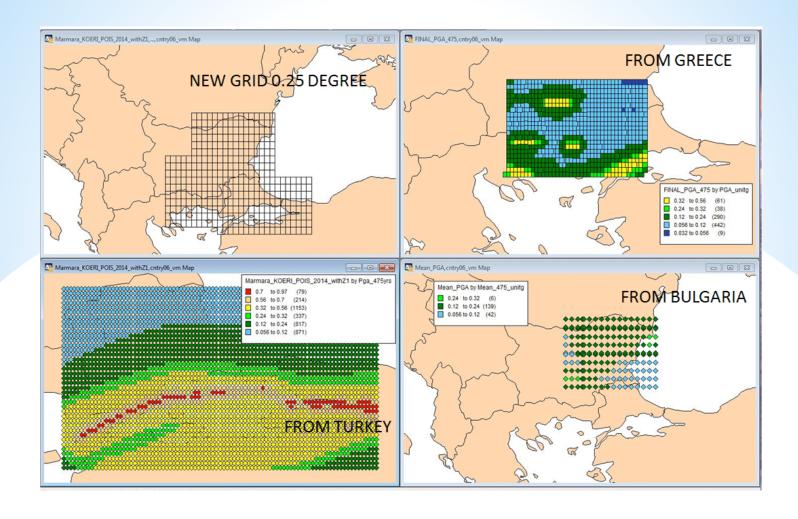
0.25*0.25 DEGREE GRID POINTS

GREECE MODEL WITH NEW GRIDS









PGA - the return period of 475 years







A Scientific Network for Earthquake, Landslide & Flood Hazard Prevention



SciNetNatHazPrev — STAKEHOLDERS MEETING
NOVEMBER 12-13, 2015, ISTANBUL, TURKEY

VENUE: MAÇKA SOCIAL CENTER, ISTANBUL TECHNICAL UNIVERSITY FOUNDATION

THANK YOU FOR YOUR ATTENTION