





## Landslide Hazard Assessment Models at Regional Scale – (SciNet NatHazPrev Project)

Democritus University of Thrace (P1) Department of Civil Engineering *Geotechnical Division* 







### Scientific Staff:

- Dr Nikolaos Klimis, Associate Professor, Civil Engineering Dept. DUTh
- Dr Ioannis Markou, Associate Professor, Civil Engineering Dept. DUTh
- Dr Stylianos Skias, Associate Professor, Civil Engineering Dept. DUTh

### Collaborating Scientific Staff:

- Dr Konstantia Makra, Senior Researcher ITSAK-EPPO
- Dr Manos Rovithis, Researcher ITSAK-EPPO
- Dr Theologos Lazaridis, external collaborator of DUTh
- Mrs Eleni Petala, MSc Civil Engineer DUTh, PhD candidate
- Mr Manos Psaroudakis, MSc Civil Engineer, DUTh







## Activity 3.1:

Landslide Hazard Assessment (LHA) at a regional scale based on the adopted/ adapted methodology

### Activity 3.4:

Slope stability analyses on natural and cut slopes in order to propose preventive measures.

### Scales:

Regional (1:250,000 to 1:25,000)

Local (1:25,000 to 1:5,000)

Site – Specific ( < 1:5,000)

As defined in SafeLand project (Corominas et al, 2013)







**Susceptibility and Hazard Maps** are often based on the following assumptions:

- homogeneous geological conditions
- all slopes have the same probability of failure
- exact location of slope failure NOT required
- all landslides are of similar size
- runout distance is NOT calculated; NOR spatial distribution and intensity

This could be improved! HOW??

**By introducing STRUCTURAL information** 







## 1. Landslide Susceptibility (static conditions) according to FEMA method

- 1. Geology (lithology per geologic group)
- 2. Slope angle (slope inclination)
- 3. Underground Water Table







## Table 1. Landslide susceptibility of geologic groups under static conditions

#### (HazUS MH, Chapter 4 – PESH.) – FEMA method

Geologic Group		Slope Angle, degrees							
		0-10	10-15	15-20	20-30	30-40	>40		
	(a) DRY (groundwater below level of sliding)								
А	Strongly Cemented Rocks (crystalline rocks and well-cemented sandstone, c' =300 psf, \$\overline\$ j = 35°)	None	None	Ι	п	IV	VI		
в	Weakly Cemented Rocks and Soils (sandy soils and poorly cemented sandstone, $c' = 0$ , $\phi' = 35^{\circ}$ )	None	Ш	IV	v	VI	VII		
с	Argillaceous Rocks (shales, clayey soil, existing landslides, poorly compacted fills, c' =0 $\phi' = 20^{\circ}$ )	v	VI	VII	IX	IX	IX		
(b) WET (groundwater level at ground surface)									
A	Strongly Cemented Rocks (crystalline rocks and well-cemented sandstone, $c' = 300 \text{ psf}$ , $\phi' = 35^{\circ}$ )	None	Ш	VI	VII	VШ	VIII		
в	Weakly Cemented Rocks and Soils (sandy soils and poorly cemented sandstone, $c' = 0$ , $\phi' = 35^{\circ}$ )	v	VШ	IX	IX	IX	х		
с	Argillaceous Rocks (shales, clayey soil, existing landslides, poorly compacted fills, c' =0 $\phi' = 20^{\circ}$ )	VII	IX	х	х	х	х		

#### ✓ Steps to realize

- 1. classification of geologic group
- 2. slope angle
- 3. hydraulic conditions (dry / wet)

#### **Arbitrary scale**

- ✓ scale I: less susceptible
- ✓ scale X: most susceptible







## 2. Landslide Susceptibility (seismic conditions) according to FEMA method

- 1. Geology (lithology per geologic group)
- 2. Slope angle
- 3. Water table

Already considered for static conditions !

Based on the principal of a Limit Equilibrium Method, an earthquake is considered as an horizontal force (seismic coefficient x weight of the potentially sliding mass of a slope)

4. Critical Acceleration  $(A_c)$  defined as the horizontal acceleration that produces a FoS = 1.0

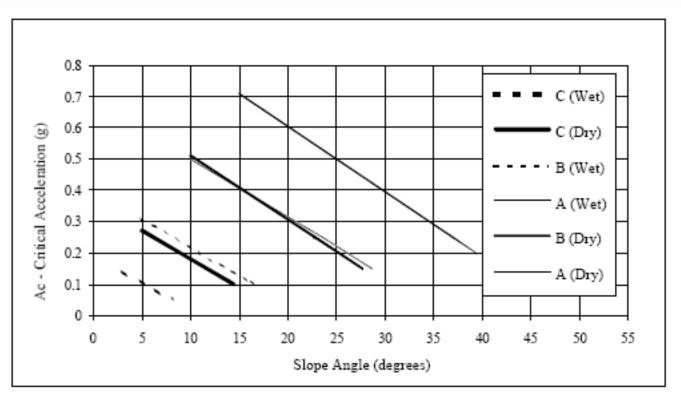






Critical acceleration (A<sub>c</sub>) is a complex function of slope, geology, steepness, groundwater table, type of landsliding & history of previous slope performance.

The Wilson and Keefer (1985) relationship is utilized in the method adopted herein.



Critical Acceleration as a Function of Geologic Group and Slope Angle (Wilson and Keefer, 1985).







#### Lower Bounds for Slope Angles and Critical Accelerations for Landsliding Susceptibility

	Slope Ang	le, degrees	Critical Acceleration (g)			
Group	Dry Conditions	Wet Conditions	Dry Conditions	Wet Conditions		
Α	15	10	0.20	0.15		
В	10	5	0.15	0.10		
С	5	3	0.10	0.05		

Critical Accelerations (ac) for Susceptibility Categories

Susceptibility Category	None	Ι	П	Ш	IV	V	VI	VII	VIII	IX	х
Critical Accelerations (g)	None	0.60	0.50	0.40	0.35	0.30	0.25	0.20	0.15	0.10	0.05







#### "Shallow" landslides susceptibility under seismic conditions

"Shallow" landslide susceptibility to earthquake-induced displacements, as specified by the index Ac/PGA

**Based on what criterion?** 

Index A<sub>c</sub>/PGA and a "subjective" categorization

- □ Very high: < 0.3
- □ High: 0.3 0.6
  - □ Moderate: 0.6 0.8
- Low: 0.8 1.0
- □ Very Low: 1.0 3.0
- **None:** > 3.0







# Landslide Hazard Assessment (regional scale)







#### •**Physically based landslide hazard** assessment methods are based on *modeling of slope failure processes*

- Applicable over large areas if geological & geomorphological conditions are fairly homogeneous and landslide types relatively simple
- Applicable to areas with incomplete or even non existing landslide inventories
- Most of them apply the **infinite slope model**, therefore they are applicable in the case of **shallow landslides**
- Also, a deterministic model for plane or circular landslides can be applied
- They account for different triggering parameters: rainfall and transcient groundwater response or to the effects of earthquake excitation







## Major advantages:

- They can be easily implemented in a GIS framework
- Results are more concrete & consistent compared to other approaches
- Higher predictive capability and most suitable to quantify the influence of individual parameters contributing to shallow landslide initiation
- Based on slope stability models, they allow the calculation of quantitative values of stability (safety factor, probability of failure)

### Some drawbacks:

• Parameterization can be a difficult task; access to critical parameters (soil depths, transient slope hydrological processes & temporal changes in hydraulic properties)

• Degree of simplification encountered / need for considerable amounts of reliable input data







## **3. Landslide Hazard Assessment** (under static & seismic conditions)

Two (2) approaches for landslide hazard assessment are implemented: HazUS method proposed by FEMA adapted to Hellenic data (triggering: earthquake),

□ the factor of safety F<sub>s</sub> computation method (triggering: static/hydraulic conditions).







#### 3. Landslide Hazard (static / hydraulic conditions) according to the safety factor method (a)

3.1 Infinite Slope Model

**Factor of Safety Assessment:**  $FS = \frac{c'}{\gamma t \sin \alpha} + \frac{\tan \varphi'}{\tan \alpha} - \frac{m\gamma_w \tan \varphi'}{\gamma \tan \alpha}$ 

 $\phi$ ': effective angle of friction of geomaterial (<sup>0</sup>)

c': effective cohesion of geomaterial (kPa),

γ: specific weight (kN/m<sup>3</sup>),

a: slope angle (Deg),

 $\gamma_w$ : specific weight of the water (kN/m<sup>3</sup>),

t: normal thickness of the failure slab (m)

m: percentage of the water saturated failure slab (%)







Infinite Slope Model

$$FS = \frac{c'}{\gamma t \sin \alpha} + \frac{\tan \varphi'}{\tan \alpha} - \frac{m\gamma_w \tan \varphi}{\gamma \tan \alpha}$$

#### **Absolutely Necessary Data:**

- 1. Geological maps of relevant scale (lithology per geologic group)
- 2. Topographic maps of relevant scale to define slope angle (a)

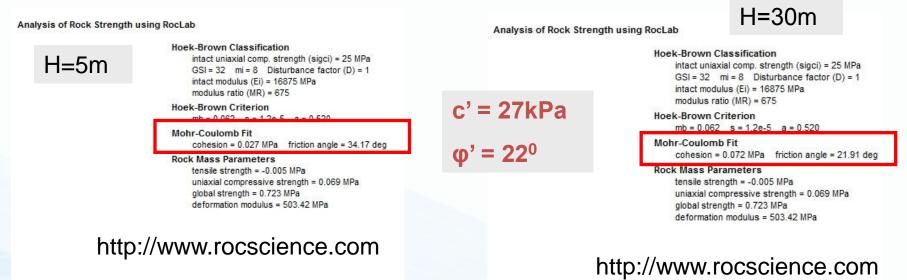
#### **Necessary Data calculated or estimated:**

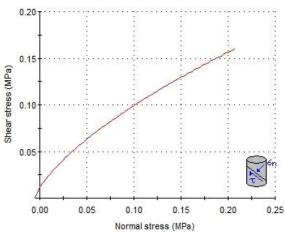
- 3. Geotechnical parameters per geological formation/group (φ', c', γ)
- IF geological formation is a ROCKMASS, then Hoek and Brown failure criterion is used in order to establish two pairs of (φ' & c') for low and high normal stress (small slope and high slope). GSI (Geological Strength Index) and uniaxial compressive strength must be estimated according to rockmass lithology and the condition of the rockmass.



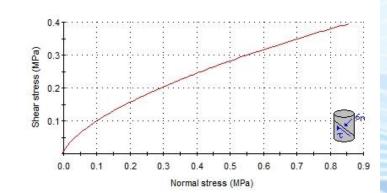








## A reliable freeware software **"RocLab"**









- 3. Geotechnical parameters per geological formation/group (φ', c', γ)
- IF geological formation is a SOIL, then according to the geological description (see geological maps) values of φ', c' and γ can be attributed according to international bibliography and our experiece.

No matter if **SOIL** or **ROCKMASS** is encountered, geotechnical parameters should be estimated or calculated in a relatively conservative way.







Data estimated : deterministic or parametric way

4. Level of ground water table (if possible)

#### Most difficult parameters to estimate ?

t: normal thickness of the failure slab (meters) m: percentage of saturation of the failure slab (%)

Normal thickness of failure slab (t) is determined as a function of slope angle, in order to calculate the factor of safety.

More effort is needed on this issue!







#### **3. Landslide Hazard (static / hydraulic conditions)** according to the safety factor method (b)

3.2 Deterministic Model for Circular Landslides

Factor of Safety  
Assessment: 
$$F_s = 4.32 * \left[ \frac{c'}{\gamma * H * \sin\beta} \right] + 1.22 * (1 - r_u) * \frac{\tan \phi'}{\tan\beta} + 0.005$$

 $\phi$ ': effective angle of friction of geomaterial (<sup>0</sup>)

c': effective cohesion of geomaterial (kPa),

 $\gamma$ : specific weight of geomaterial (kN/m<sup>3</sup>),

β: slope angle (Deg),

 $\gamma_w$ : specific weight of the water (kN/m<sup>3</sup>)

H : height of the slope (m)

 $r_u$ : pore pressure ratio ( $\gamma_w / \gamma$ )

Ferentinou et al., 2006







Upper Bound

Common borders. Common solutions.

## 3. Landslide Hazard (seismic conditions) according to FEMA method (c)

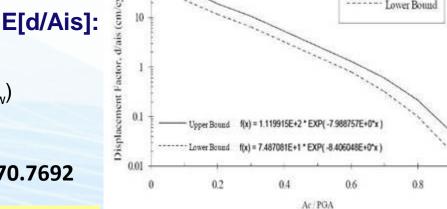
Assessment of Permanent Ground Displacements (PGD) of

"shallow" landslides

 $E[PGD] = E[d/A_{is}]*A_{is}*n$ 

 $A_{is}$ : induced acceleration (g) –  $A_{is}$  = PGA **n**: number of cycles (function of earthquake  $M_w$ ) **E[d/A<sub>is</sub>]:** expected displacement factor

 $n = 0.3419M_w^3 - 5.5214M_w^2 + 33.6154M_w - 70.7692$ 



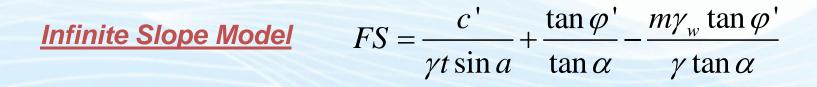
Local GMPEs (Skarlatoudis et al., 2003)  $h_c / PGA$   $\log PGA = 1.07 + 0.45M - 1.35 \times \ln(R + 6) + 0.09F + 0.06S \pm 0.286$  $\log PGA = 0.86 + 0.45M - 1.27 \times \ln(R^2 + h^2)^{\frac{1}{2}} + 0.10F + 0.06S \pm 0.286$ 







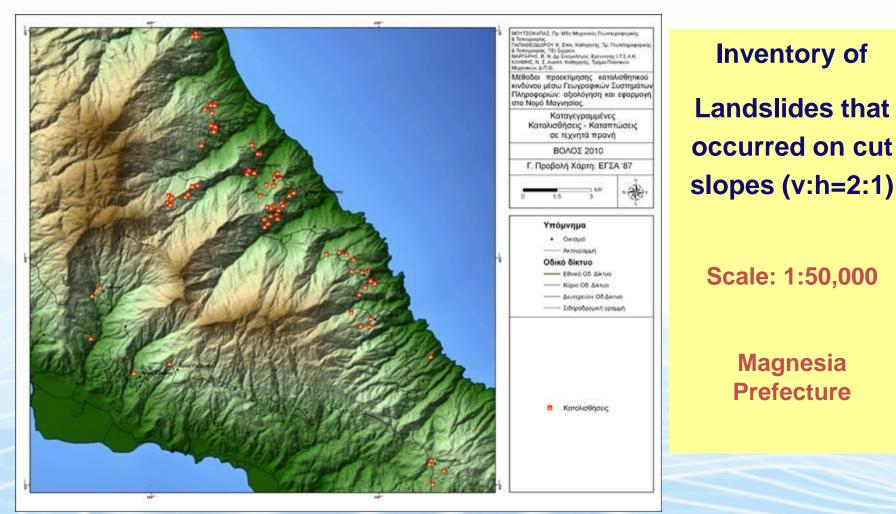
## An implementation (regional scale)







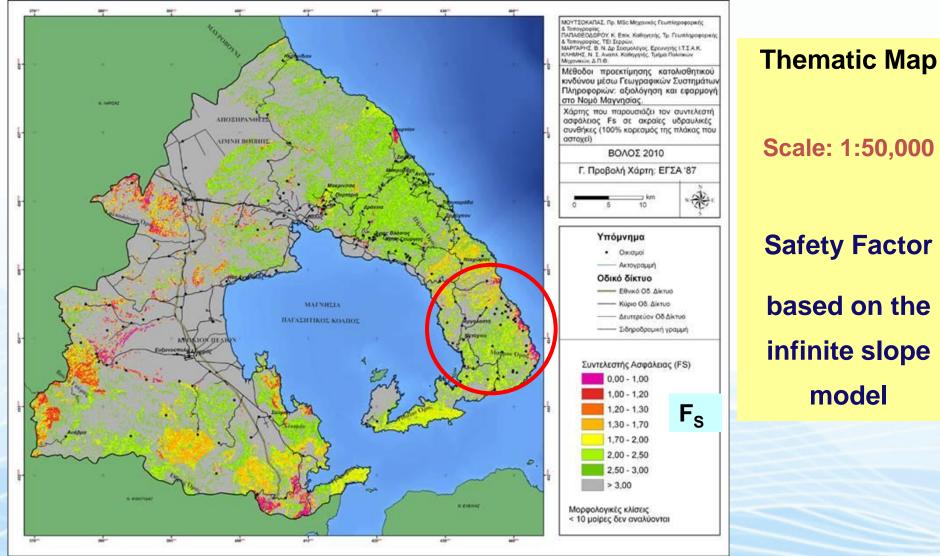












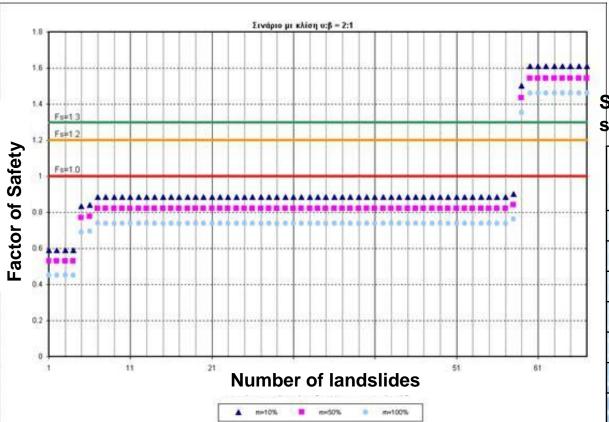






Landslide Hazard (static / hydraulic conditions) according to the safety factor method in 67 locations where landslides occurred in cut slopes (vertical:horizontal = 2:1)

#### The above method, albeit crude, reached a percentage of almost 85% success.



Parametric investigation regarding saturation (m, %) of the sliding slab.

Slope-normal thickness of the failure slab (t) correlated to the slope angle (°).

Slope angle (°)	Slab normal thickness (t)
90° - 80°	t=0.0m
80° - 70°	t=1.0m
70° - 60°	t=1.5m
60° - 50°	t=2.0m
50° - 40°	t=2,5m
40° - 30°	t=4,0m
30° - 0°	t=10m







## So, in order to CONCLUDE !!!

## Landslide Susceptibility Regional Scale 1:250,000 to 1:25,000 (static & seismic conditions)

FEMA method (for static conditions: geologic maps + topography maps + hydraulic conditions) BUT needs improvement (introducing structure of soils/rocks: dip & dip direction of bedding, schistosity, interface of weathered zone and rockmass or soil over rockmass)

FEMA method (for seismic conditions: geologic maps + topography maps + hydraulic conditions) + Critical Acceleration: index A<sub>C</sub> / PGA seems to work fine with local GMPEs and "shallow" landslides







Landslide Hazard Assessment Regional Scale 1:250,000 to 1:25,000 (static & seismic conditions):

- 1. Factor of Safety method (for static conditions: geologic maps + topography maps + hydraulic conditions (% of sliding slab saturation) + geotechnical parameters ( $\varphi$ ', c') + sliding slab normal thickness) seems to work fine for "shallow" landslides, BUT needs some improvement (regarding assessment of sliding slab thickness)
- 2. FEMA method (for seismic conditions: geologic maps + topography maps + hydraulic conditions) + Critical Acceleration: index A<sub>C</sub> / PGA resulting in assessment of Permanent Ground Displacements seems to work fine with local GMPEs and for "shallow type" landslides







## Activity 3.4:

Slope stability analyses on natural and cut slopes in order to propose preventive measures.

Need for site - specific scale on a scale < 1:5,000 (static & seismic conditions):

Need for a user friendly software for slope analysis:

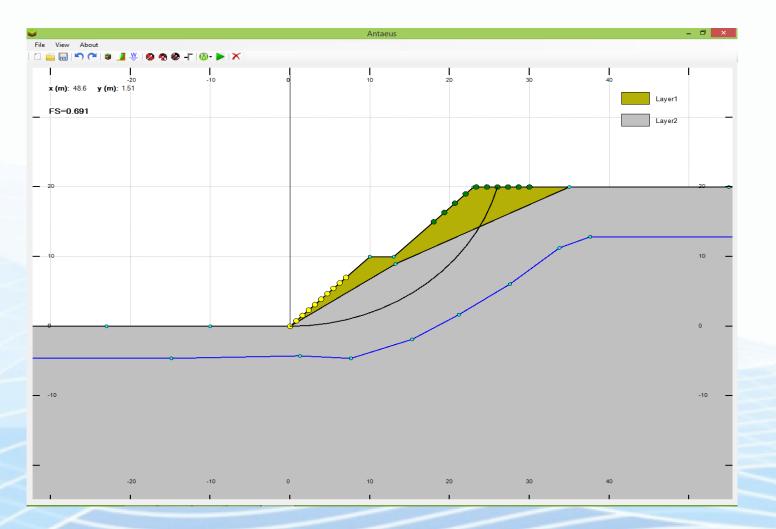
- freeware (if possible)
- easy to use and understand
- reliable

There is something like that under preparation





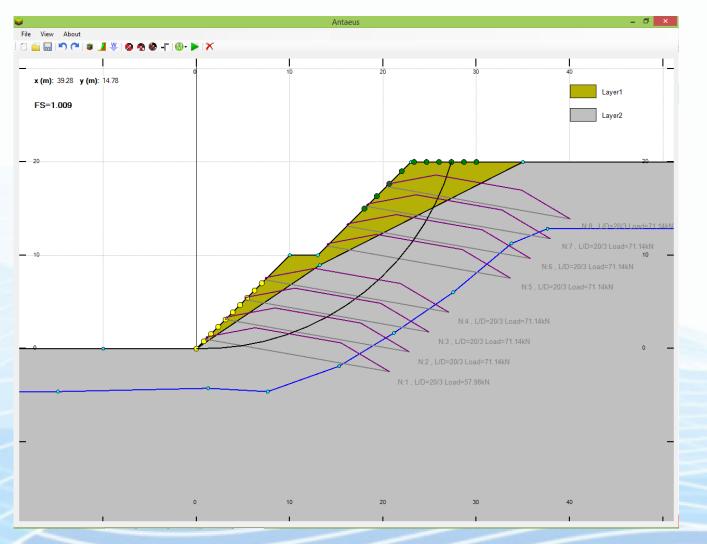








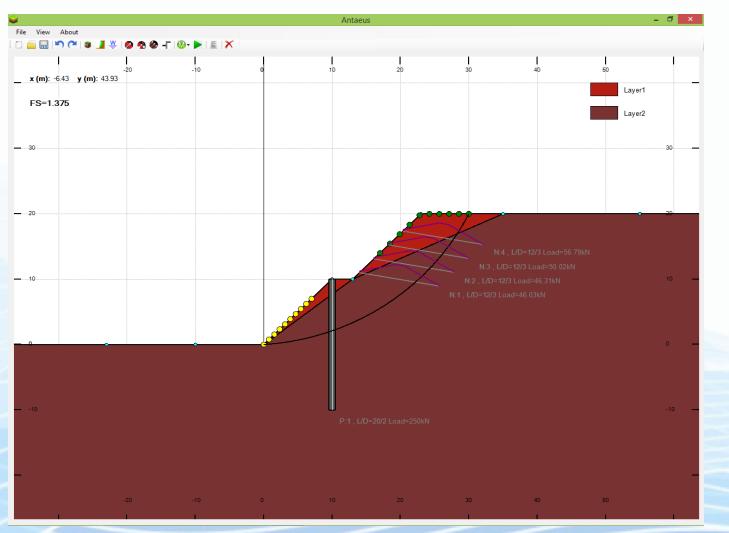


















## Thank you !